



September 11, 2024

ADDENDUM #1
BL107-24, Construction of Beaver Ruin Wetland Park

****The question deadline for BL107-24 has been extended until Friday, September 13, 2024 at 3:00 PM. All questions regarding bids shall be directed to Jake Scarpone, Purchasing Associate II, via email at jake.scarpone@gwinnettcounty.com or via phone at 770-822-8722.****

CLARIFICATIONS:

- C1. **Revise the Table of Contents to add Division 11, Section 11 6813 Playground Equipment and to revise Section 02 3000 Subsurface Investigation to add Appendix A.**
- C2. **Revise Gwinnett County's front-end page 3 SCOPE OF WORK the 5TH bullet to delete the word "future."**
- C3. **Add Section 11 6813 Playground Equipment.**
- C4. **Add Playground Site Plan as prepared by KOMPAN sheets K1.0 dated 09/11/24.**
- C5. **Revise Section 02 3000 Subsurface Investigation to add Appendix A.**
- C6. **Include Geotechnical Investigation as Appendix A.**

QUESTIONS & ANSWERS:

- Q1. **After a site visit of the Beaver Ruin Wetland area, I saw that there was an additional construction entrance that was being utilized by Clean Water Consultants at BP gas station (4450 Satellite Blvd, Duluth, GA 30096). Will this be a possible point of access for the project?**
 - A1. No, this location will not be available as an access point to the property.
- Q2. **I could not find anything within the contract specifications pertaining to who will be responsible for submitting the Sustainable SITE certification information and paying the associated fees with this. Is this something that Gwinnett County will handle?**
 - A2. The County has paid all associated fees for SITES certification. The contractor will need to participate in the process and provide the required documentation and comply with all other requirements of the Contract Documents.
- Q3. **Under the section titled "Special Provisions" number 22. GEOTECHNICAL on page 8, the paragraph calls out that the geotechnical report is attached in Appendix A, however Appendix A cannot be located.**
 - A3. Revise Section 02 3000 Subsurface Investigation to add Appendix A. Please see Attachment 6 for the geotechnical report.
- Q4. **Is there a CAD file for this project and if so, will it be made available?**
 - A4. CAD files will be provided to the awarded contractor.
- Q5. **Sheet 101 of 169 (sheet PT-09 Precast Concrete Specs) of the plan drawings states in section 1.3F states that "all precast shall consist of integrally colored concrete". Please confirm that**

color is in fact required since it does explicitly state this in the Precast Structural Concrete specification, Section 03-4100.

- A5. Yes, all precast shall consist of integrally colored concrete from one of PermaTrak's "standard colors". The owner selected standard color will be Adelaide Gray.
- Q6. Sheet 101 of 169 (sheet PT-09 Precast Concrete Specs) of the plan drawings states in section 1.3D states "walking surface of top surface of treads shall have a formliner finish". Please confirm that a hand or broom troweled top surface of treads is not acceptable.**
- A6. Permatrak treads walking surface will have the standard Permatrak finish PermaGrip. Hand or broom troweled top surface of treads is not acceptable.
- Q7. Does the Precast Concrete Specifications noted above supersede the Precast Structural Specification, Section 03-4100?**
- A7. No.
- Q8. Are you able to share the Geotechnical report for this project?**
- A8. Revise Section 02 3000 Subsurface Investigation to add Appendix A. Please see Attachment 6 for the geotechnical report.
- Q9. Can the question deadline be extended?**
- A9. The question deadline has been extended until Friday, September 13, 2024 at 3:00 PM. All questions shall be directed to Jake Scarpone, Purchasing Associate II, via email at jake.scarpone@gwinnettcounty.com or via phone at 770-822-8722.

This addendum should be acknowledged in the space provided on page 15 of the bid documents and returned with your bid. Failure to do so may result in your bid being deemed non-responsive.

Thank you,

Jake Scarpone

Jake Scarpone
Purchasing Associate II

Attachments:

1. Pre-Bid Conference Sign In Sheet
2. Revised Table of Contents
3. Section 11 6813 – Playground Equipment
4. Playground Plan
5. Section 02 3000 - Subsurface Investigation
6. Geotechnical Report

PRE-BID CONFERENCE

BL107-24

	<u>Representative Name</u>	<u>Company Name</u>	<u>Phone #</u>	<u>E-Mail Address</u>
	(DEPARTMENT REPRESENTATIVES SIGN-IN AT BOTTOM)			
1.	Brad Williams	Crowder	404-938-7012	bwilliams@crowderusa.com
2.	Latrice Land	Diversified Constr ^{of}	(678) 705-4373	lids@dcoggeorgia.com
3.	Andrew Dial	Gunnison	478 550 3858	Adial@woodmontree.com
4.	Neil Blasingame	Strack Inc	678-591-9594	neilb@strackinc.com
5.	Luce Miller	Strack, Inc	412-951-2477	lucem@strackinc.com
6.	Madeline Layson	Multiplex LLC	1078-317-2040	madeline@multiplexllc.com
7.	JASON PHILBIN	PERMATRAK CONCRETE	930-229-3036	JPHILBIN@PERMATRAK.COM
8.	Liz Camacho	Tri Scaper	678 939 8424	liz@triscaper.com
9.	Aaron Steele	Tailor trails	678-614-8300	AaronSteele@tailoredtrails.net
10.	Jeremy Vanoy	DOCS	770-653-0054	Jeremy.Vanoy@Gwinnettcounty.com
11.	Joseph Powell	CPL	770-831-9000	jpowell@cplteam.com
12.				
13.				

<u>Department Representative Name</u>	<u>Department</u>	<u>Department Representative Name</u>	<u>Department</u>
Jake Scarpone	DOFS		
DANIEL DAPT	DOCS		

SECTION 00 0010 – TABLE OF CONTENTS

REVISION DATE

DIVISION 00 – PROCUREMENT AND CONTRACTING REQUIREMENTS

00 0010	Table of Contents
00 0011	List of Drawings
00 0012	Gwinnett County Purchasing Front End Index
00 0013	Gwinnett County Purchasing Front End

DIVISION 01 - GENERAL REQUIREMENTS

01 1000	Summary
01 2000	General Requirements
01 2200	Unit Prices
01 2600	Contract Modification Procedures
01 2700	Project Management and Coordination
01 2900	Payment Procedures
01 3000	Submittals
01 3100	Construction Schedules
01 3120	Project Meetings
01 3329.02	Sustainable Design Reporting – SITES
01 3566.05	Project Sustainability Goal Credit Summary - SITES
01 3566.12	Sustainable Certification Project Procedures –SITES
01 3900	Electronic Deliverables Release
01 4000	Quality Requirements
01 4200	References
01 4300	Testing Laboratory Services
01 5000	Temporary Facilities
01 6000	Product Requirements
01 6300	Substitutions
01 7300	Execution
01 7419	Construction Waste Management and Disposal
01 7800	Contract Closeout
01 7839	Project Record Documents
01 7900	Demonstration and Training

DIVISION 02 – EXISTING CONDITIONS

02 3000	Subsurface Investigation	09-11-24
---------	--------------------------	----------

DIVISION 03 – CONCRETE

03 1000	Concrete Forming and Accessories
03 2000	Concrete Reinforcing
03 3000	Cast-in-Place Concrete
03 4100	Precast Structural Concrete

DIVISION 04 – MASONRY

04 2000	Unit Masonry
04 4313	Stone Masonry Veneer

DIVISION 05 – METALS

05 1200	Structural Steel Framing
---------	--------------------------

REVISION DATE

05 1213	Architecturally-Exposed Structural Steel Framing
05 3100	Steel Decking
05 5000	Metal Fabrications
05 5100	Metal Stairs
05 5213	Pipe and Tube Railings
05 5305	Metal Gratings
05 7316	Cable Railing

DIVISION 06 – WOOD, PLASTIC, AND COMPOSITES

06 1053	Miscellaneous Rough Carpentry
06 1326	Heavy Timber Trusses
06 1753	Shop-Fabricated Wood Trusses
06 4023	Architectural Woodwork

DIVISION 07 - THERMAL AND MOISTURE PROTECTION

07 2100	Thermal Insulation
07 2123	Loose-Fill Insulation
07 2726	Fluid-Applied Membrane Air Barriers
07 4113	Metal Roof Panels
07 4646	Fiber-Cement Siding
07 6200	Sheet Metal Flashing and Trim
07 7100	Roof Specialties
07 9200	Joint Sealants

DIVISION 08 – OPENINGS

08 1113	Hollow Metal Doors and Frames
08 3323	Overhead Coiling Doors
08 4500	Translucent Wall Panels

DIVISION 09 - FINISHES

09 6700	Fluid-Applied Flooring
09 9113	Exterior Painting
09 9123	Interior Painting
09 9300	Staining and Transparent Finishing

DIVISION 10 – SPECIALTIES

10 1400	Signage
10 2113.17	Phenolic Toilet Compartments
10 2800	Toilet Accessories
10 4400	Fire Protection Specialties

DIVISION 11 - EQUIPMENT

11 6813	Playground Equipment
---------	----------------------

09-11-2024

DIVISION 22 – PLUMBING

22 0500	Common Work Results for Plumbing
22 0517	Sleeves and Sleeve Seals for Plumbing Piping

REVISION DATE

22 0519	Meters and Gauges for Plumbing Piping
22 0523	General-Duty Valves for Plumbing Piping
22 0529	Hangers and Supports for Plumbing Piping and Equipment
22 0553	Identification for Plumbing Piping and Equipment
22 0719	Plumbing Piping Insulation
22 1005	Plumbing Piping
22 1006	Plumbing Piping Specialties
22 3000	Plumbing Equipment
22 4000	Plumbing Fixtures

DIVISION 23 – HEATING VENTILATING AND AIR CONDITIONING

23 0000	General Provisions for Mechanical Work
23 0002	Mechanical and Electrical Coordination
23 0529	Hangers and Supports for HVAC Piping & Equipment
23 0553	Identification for HVAC Piping and Equipment
23 0593	Testing, Adjusting and Balancing for HVAC
23 0713	Duct Insulation
23 3100	HVAC Ducts and Casings
23 3300	Air Duct Accessories
23 3423	HVAC Power Ventilators
23 3700	Air Outlets and Inlets

DIVISION 26 – ELECTRICAL

26 0010	General Provisions for Electrical Work
26 0519	Low-Voltage Electrical Power Conductors and Cables
26 0526	Grounding and Bonding for Electrical Systems
26 0529	Hangers and Supports for Electrical Systems
26 0533.13	Conduit for Electrical Systems
26 0533.16	Boxes for Electrical Systems
26 0553	Identification for Electrical Systems
26 0923	Lighting Control Devices
26 2416	Panelboards
26 2726	Wiring Devices
26 2816.16	Enclosed Switches
26 5100	Interior Lighting
26 5600	Exterior Lighting

DIVISION 31 – EARTHWORK

31 1000	Site Clearing
31 2200	Grading
31 2316.13	Trenching
31 2316	Excavation
31 2323	Fill
31 3116	Termite Control
31 6615	Helical Foundation Piles

DIVISION 32 – EXTERIOR IMPROVEMENTS

32 1313	Concrete Paving
32 1723	Pavement Markings

REVISION DATE

32 1726 Tactile Warning Surfacing
32 1816.13 Playground Protective Surface

DIVISION 33 – UTILITIES

33 0561 Concrete Manholes
33 1416 Site Water Utility Distribution Piping
33 3113 Site Sanitary Sewerage Gravity Piping
33 4211 Stormwater Gravity Piping

END OF SECTION 00 0010

**SECTION 11 6813
PLAYGROUND EQUIPMENT**

PART 1 GENERAL

1.01 SECTION INCLUDES

- A. Concrete footings for playground equipment.
- B. Playground equipment.
- C. Location of each item of playground equipment is indicated on drawings.

1.02 RELATED REQUIREMENTS

- A. Section 03 3000 - Cast-in-Place Concrete: Footings for playground equipment.

1.03 REFERENCE STANDARDS

- A. ASTM A123/A123M - Standard Specification for Zinc (Hot-Dip Galvanized) Coatings on Iron and Steel Products; 2017.
- B. ASTM A135/A135M - Standard Specification for Electric-Resistance-Welded Steel Pipe; 2021.
- C. ASTM A500/A500M - Standard Specification for Cold-Formed Welded and Seamless Carbon Steel Structural Tubing in Rounds and Shapes; 2020.
- D. ASTM A513/A513M - Standard Specification for Electric-Resistance-Welded Carbon and Alloy Steel Mechanical Tubing; 2020a.
- E. ASTM B26/B26M - Standard Specification for Aluminum-Alloy Sand Castings; 2018, with Editorial Revision.
- F. ASTM B108/B108M - Standard Specification for Aluminum-Alloy Permanent Mold Castings; 2019.
- G. ASTM B179 - Standard Specification for Aluminum Alloys in Ingot and Molten Forms for Castings from All Casting Processes; 2018.
- H. ASTM D3363 - Standard Test Method for Film Hardness by Pencil Test; 2022.
- I. ASTM F1292 - Standard Specification for Impact Attenuation of Surfacing Materials Within the Use Zone of Playground Equipment; 2022.
- J. ASTM F1487 - Standard Consumer Safety Performance Specification for Playground Equipment for Public Use; 2021.
- K. CPSC Pub. No. 325 - Public Playground Safety Handbook; 2015.

1.04 SUBMITTALS

- A. See Section 01 3000 - Administrative Requirements, for submittal procedures.
- B. Product Data: For manufactured equipment, provide manufacturer's product data showing materials of construction, compliance with specified standards, installation procedures, safety limitations, and the number of users permitted.

- C. Shop Drawings: Detailed scale drawings showing play event layout, Use Zone perimeters, and fall height for each play event.
 - 1. Show locations and dimensions of footings and anchorage points.
 - 2. Clearly identify mounting elevations in relation to a fixed survey point on site and to subgrade elevation and depth of protective surfacing.
- D. Letter from manufacturer certifying that the installer is approved.

1.05 QUALITY ASSURANCE

- A. Maintain one copy of the latest edition of ASTM F1487 and CPSC Pub. No. 325 at project site.
- B. Installer Qualifications: Company certified by manufacturer for training and experience installing playground equipment.

1.06 DELIVERY, STORAGE, AND HANDLING

- A. Deliver, handle, and store equipment to project site in accordance with manufacturer's recommendations.
- B. Store materials in a dry, covered area, elevated above grade.

1.07 WARRANTY

- A. See Section 01 7800 - Closeout Submittals, for additional warranty requirements.
- B. Provide manufacturer's standard warranty.

PART 2 PRODUCTS

2.01 NOTE:

- A. Where manufacturers are listed, add "Or approved equal".
- B. All references to manufacturer(s) and "approved equal" are included for description of quality and content of the designated equipment/materials. Equivalent items may be accepted if they meet all standards of quality and purpose for the intended use, as determined by Gwinnett County.
- C. Substitutions request requirements: Refer to Section 01 6300 – Substitutions.

2.02 MANUFACTURERS

- A. Playground Equipment:
 - 1. KOMPAN, INC.

2.03 PLAYGROUND EQUIPMENT - GENERAL

- A. Design Assumptions: Because the safety of the playground depends on strict compliance with design criteria, this information is provided for Contractor's information.
 - 1. Playground has been designed for children ages 2-5 and 5-12.
 - 2. If deviations from specified dimensions, especially fall heights, is required, obtain approval prior to proceeding; follow approval request procedure as specified for substitutions.
- B. Mount equipment on concrete footings, unless otherwise indicated.

1. Protective Surfacing Depth: As indicated on drawings.
 2. Provide supports as required to mount equipment at proper height above finish and sub-grades to allow installation of sufficient depth of protective surfacing; portion of support below top of surfacing must comply with specified requirements for equipment.
 3. Paint portion of support that is intended to be installed below top surface of protective surfacing a different color, or mark in other permanent way, so that installers and maintainers of protective surfacing can easily determine whether sufficient depth has been installed.
- C. Provide permanent label for each equipment item stating age group that equipment was designed for, manufacturer identification, and warning labels in accordance with ASTM F1487.

2.04 PLAYGROUND EQUIPMENT

- A. Comply with ASTM F1487 and CPSC Pub. No. 325; provide equipment complying with specified requirements for relevant age group(s).
1. Provide components having factory-drilled holes; do not use components with extra holes that will not be filled by hardware or covered by other components.
- B. Equipment Schedule:
1. Refer to Civil drawings.
- C. Equipment Locations:
1. Refer to Civil drawings.

2.05 MATERIALS

- A. Steel Pipe and Tube: Comply with ASTM A135/A135M, ASTM A500/A500M, or ASTM A513/A513M; hot-dipped galvanized and free of excess weld and spatter.
1. Tensile Strength: 45,000 psi, minimum.
 2. Yield Point: 33,000 psi, minimum.
 3. Galvanizing: Hot-dip metal components in zinc after fabrication, in accordance with ASTM A123/A123M; remove tailings and sharp protrusions and burnish edges.
- B. 513/A513M; hot-dipped galvanized and free of excess weld and spatter. Metal
- C. Fireman's poles, handles, spacers, chains and bars are made from stainless steel.
- D. Brackets, support legs and chains are hot dip galvanized steel tested for compliance with US CPSIA requirements regarding lead content as well as the European Standard EN 71-3 regarding migration of unwanted substances.
- E. Springs are made of steel qualities that meet DIN 17221. The springs are subjected to shot peening to prevent crack formation and fatigue fracture. Spring durability and expected life in use are tested on a sampling basis to ascertain that the spring will function after more than 5 years of normal use. Springs are fitted with patented anti-pinch clamps of cast nylon.
- F. Extruded Aluminum: ASTM B221 or ASTM B221M, Alloy 6061, 6062, or 6063.

1. Tensile Strength: 39,000 psi, minimum.
 2. Yield Point: 36,500 psi, minimum.
- G. Cast Aluminum: ASTM B26/B26M, ASTM B108/B108M, or ASTM B179.
- H. Chain: Corrosion resistant zinc plated steel; minimum size 4/0; polyvinyl chloride (PVC) coating.
- I. Rope Cable: Strands of steel cable with UV-stabilized polypropylene synthetic covering; ends capped to prevent fraying.
1. Nets and ropes:
 - a. Nets and ropes are made of UV-stabilized PP (polypropylene) with inner steel cable reinforcement. Ultimate tensile strength of the rope is at least 2,500 kg. The net connectors are KOMPAN-designed and made from a specially formulated injection-molded PA (polyamide) in order to perform the maximum strength and UV stability. Nets and ropes are equipped with stainless steel chains in the end for adjustment due to variation in Robinia dimensions.
- J. Plastic: Panels for decoration and attachment of slides are made of 19MM Ecocoretm.
- K. Hardware: Provide without hazardous protrusions, corners, or finishes, and that require tools for removal after installation; countersunk fasteners are preferred.
1. Use stainless steel for metal-to-metal connections; select type to minimize galvanic corrosion of materials connected by hardware.
 2. Use stainless steel for wood-to-wood and wood-to-metal connections.
 3. Use stainless steel with plastic components.
 4. Bearings: Self lubricating.
 5. Hooks, Including S-Hooks: Closed loop; maximum gap 0.04 inches, less than the thickness of a dime.
 6. Rails, Loops, and Hand Bars: Same metal as item is mounted on or aluminum; with powder coating.
 7. Anchors: In accordance with manufacturer's recommendations.
- L. Wood posts, crossbars and other un-fabricated parts:
1. Species: Robinia (Black Locust)
 - a. De-barked and sap free Robinia trunks.
 - b. Cut to meet safety requirements of ASTM F1487.
 - c. From FSC-certified sources.
- M. Polyvinyl Chloride (PVC) Coating: Ultraviolet (UV) stabilized and mold-resistant; slip-resistant finish; prime parts to be coated with clear acrylic thermosetting solution, and preheat prior to dipping in liquid PVC.
1. Thickness: 0.08 inch, minimum, plus/minus 0.02 inch.
 2. Hardness: 85 durometer, when tested in accordance with ASTM D3363.
- N. Concrete: As specified in Section 03 3000.

PART 3 EXECUTION

3.01 VERIFICATION OF CONDITIONS

- A. Verify that playground area has been graded to subgrade elevations required and that excess soil, rocks, and debris have been removed.
- B. Verify that playground equipment footings have been installed in proper locations and at proper elevations.
- C. Verify location of underground utilities and facilities in playground area; damage to underground utilities and facilities will be repaired at Contractor's expense.

3.02 INSTALLATION

- A. Coordinate work with preparation for and installation of protective surfacing specified in Section 32 1816.13; install protective surfacing after playground equipment installation.
- B. Install in accordance with CPSC Pub. No. 325, ASTM F1487, manufacturer's instructions, and requirements of authorities having jurisdiction (AHJ).
- C. Anchor equipment securely below bottom elevation of resilient surfacing layer.
- D. Install without sharp points, edges or protrusions, entanglement hazards, pinch, crush, or shear points.
- E. Do not modify play events on site without written approval of manufacturer.
- F. Install required signage if not factory-installed.

3.03 FIELD QUALITY CONTROL

- A. Obtain the services of the equipment manufacturer's field representative to review the finished installation for compliance with specified requirements and with design criteria to the extent known to the Contractor; submit report of field review.
- B. Owner or Owner's representative will inspect playground equipment after installation to verify that playground meets specified design safety and accessibility requirements.
- C. Repair or replace rejected work until compliance is achieved.

3.04 CLEANING

- A. Restore adjacent existing areas that have been damaged from the construction.
- B. Clean playground equipment of construction materials, dirt, stains, filings, and blemishes due to shipment or installation; clean in accordance with manufacturer's instructions, using cleaning agents as recommended by manufacturer.
- C. Clean playground area of excess construction materials, debris, and waste.
- D. Remove excess and waste material and dispose of off-site in accordance with requirements of authorities having jurisdiction (AHJ).

3.05 PROTECTION

- A. Protect installed products until Date of Substantial Completion.

MAZE AREA
 50/50 BEIGE PIP SAFETY SURFACING
 AREA: 1,630 SF
 PERIMETER: 171 LF

5-12 FLAT AREA
 50/50 BEIGE PIP SAFETY SURFACING
 AREA: 4,713 SF

2-5 AREA
 50/50 BEIGE PIP SAFETY SURFACING
 AREA: 1,576 SF
 PERIMETER: 158 LF

SWING AREA
 50/50 BEIGE PIP SAFETY SURFACING
 AREA: 1,534 SF

5-12 MOUND AREA
 50/50 BEIGE PIP SAFETY SURFACING
 AREA: 2,827 SF

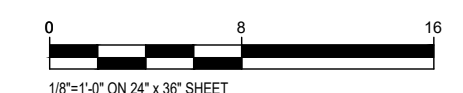
50/50 GREEN PIP SAFETY SURFACING AREA: 2,385 SF

TOTAL PIP AREA: 14,665 SF
 50/50 BEIGE PIP FLAT AREA: 9,453 SF
 50/50 BEIGE PIP MOUND AREA: 2,827 SF
 50/50 GREEN PIP AREA: 2,385 SF

#	Product Number	Product Name	M.F.H.	Count	#	Product Number	Product Name	M.F.H.	Count
A	NR025-CUSTOM-FSC_3058308	5 Seats Rotating Swing 2 Adults, 2 Bch, 1 ADA	71"	1	J	KR0152195	woodchip mulch	3"	1
B	NR099206	Double Encircling Slide		1	L	CRP43031-CUSTOM_2029977	HD Climber Rope with EPDM Top & Tip Carousal	0"	1
C	COR08266	Climbing Net	5'2"	1	M	EL04005-30175C		3"	1
D	NR08021-CUST-FSC_3058044	Triple Wooden Play Panel	0"	1	N	KR0201006	Robbie tree with ramp and bridge	5'10"	1
E	NR0154-041F5C	Spring Board	18"	1	O	KR0200489	2.5 Robina Tree	3'2"	1
F	NR0115-041F5C	Shed Springer	18"	1	P	KR0200683	rotary play	2'2"	1
G	NR0115-041F5C	Forest Bag Springer	18"	1	D	KR0200112	Robbie maze	0"	2
H	EL040158-041F0T	Junior Slides	0"	1					
I	GK199014-0217	Supernova	24"	1					

Beaver Ruin Wetlands Park

Gwinnett County, GA
 Site Plan



REVIEW BY	DATE	REVISION
DESIGN		
REV. NO.	REV. BY	REV. DATE

SALES REPRESENTATIVE: K1.0
 SHEET: K1.0
 REVISION NOTES

MANUFACTURER'S SHOP DRAWING
 FOR USE BY CONTRACTOR, ENGINEER, OR DESIGN PROFESSIONAL. IF REQUIRED, SEE BIDDING/SALES
 PROPOSAL FOR COMPLETE DETAILS TO BE PROVIDED BY SUPPLIER OR MANUFACTURER. COMPANY
 SHALL MAINTAIN AND STORE WITH COMPANY SALES REP OR PROJECT MANAGER PRIOR TO USE FOR REVIEW,
 REVISIONS, OR CONSTRUCTION.
 TO BE READ CONJUNCTIVELY WITH COMPANY'S STANDARDS FOR SITE PREPARATION, MATERIALS AND
 INSTALLATION PROCESSES. PROCEED AT THE CONTRACTOR'S RISK. COMPANY IS NOT RESPONSIBLE FOR
 ANY DAMAGE TO OR LOSS OF EQUIPMENT OR PERSONNEL. COMPANY'S PRODUCT IS NOT A
 SUBSTITUTE FOR ANY OTHER PRODUCT. ALL DIMENSIONS AND LOCATIONS OF ALL STRUCTURES SHOWN REQUIRE A SITE OFFICE
 OF THE MANUFACTURER TO VERIFY. SPECIFICATIONS FOR EACH COMPANY STRUCTURE MAY BE FOUND AT
 COMPANY.COM/PARTS/STANDARDS
 DIMENSIONS OF PLAY AREA, SEE THE OBSERVATION LOCATIONS OF ALL EXISTING UTILITIES EQUIPMENT
 AND SITE FURNISHINGS TO BE FIELD VERIFIED PRIOR TO CONSTRUCTION.
 PRINTED AND PLOTTED IN US BY KOMPAN © 2024 KOMPAN, INC. ALL RIGHTS RESERVED.

**SECTION 02 3000
SUBSURFACE INVESTIGATION**

PART 1 GENERAL

1.01 SECTION INCLUDES

- A. Attached subsurface evaluation report - Appendix A.

1.02 DESCRIPTION

- A. A soils investigation report titled Report of Geotechnical Exploration Beaver ruin Wetlands Park, dated January 7th, 2021, has been prepared for the site of this work by UNITED CONSULTING and is attached.
- B. *A soils investigation report titled Report of Geotechnical Exploration Beaver ruin Wetlands Park, dated December 21, 2020, has been prepared for the site of this work by UNITED CONSULTING and is attached.*
- C. *A Boardwalk Foundation Recommendations letter from Tetra Tech dated December 31, 2020.*
- D. Such information is not a warranty of subsurface conditions and may not reflect subsurface conditions over the entire proposed construction area. The Contractor shall be responsible for their interpretations and use of the information.
- E. The availability or use of the soils investigation report and logs of test borings shall not be construed as a waiver of the Contractor's duty to examine the site and the conditions affecting the work, and does not relieve the Contractor from the risk of soil or subsurface conditions which could reasonably be anticipated.

PART 2 PRODUCTS (NOT USED)

PART 3 EXECUTION (NOT USED)

END OF SECTION 02 3000

This page intentionally left blank



UNITED
CONSULTING

REPORT

**For Gwinnett County
Department of Water
Resources**

Geotechnical Exploration
Beaver Ruin Wetlands Park
Duluth, Gwinnett County, Georgia

Project No.: GCDWR-20-GA-04273-01
December 21, 2020





September 21, 2020

Hales O'Connell
to Attention: Manager
Gwinnet County Department of Water Resources
4 Independence Way
Lawrenceville, GA 30046

Re: [Hales O'Connell Gwinnet County](#)

Report of Geotechnical Investigation
Beaver Ruin Wetlands Park
in Gwinnet County, Georgia
October 20, 2020 - 04273-01


Dear Sirs:

We are pleased to submit this report of geotechnical investigation for the above-mentioned project. The work was completed in general accordance with the proposal of 2020-40-01 effective 07/20/20. The Technical Report is attached for your review. The report has a reference to 2000-7121-1 issued on 4/27/20.

We appreciate the opportunity to assist you with this project and look forward to continuing participation should you have any questions or if we can be of further assistance.

Sincerely,

UNITED CONSULTING


Rafael I. Ospina, P.E.
Consultant Geotechnical Engineer




Chris L. Roberds, P.G.
Senior Geotechnical Engineer

T L g



TABLE OF CONTENTS

10	T	4
20	T T	
0		
40		7
0	B T T T	
0	L B T T T	10
70	T	11
71	isting ill	11
72	ite epa ation	11
7	iffi lt a ation	12
74	on ate onsi e ations	12
7	a ing onsi e ations	12
7	on ation esign an onst tion	1
77	on loo labs	14
7	a th o k	1
7	lopes	1
710	ill la e ent	1
711	etaining alls	1
0	L T T	1

TABLES

- Table 1 □ Boa alk ie ea tion Loa s
- Table 2 □ a y of bs fa e on itions
- Table □ oil o osi ity Test es lts
- Table 4 □ a y of eli ina y eli al ie esign e o en ations
- Table □ Late al a th ess es

APPENDIX

- ene al otes a ati e of illing pe ations
- ig e 1 □ Bo ing Lo ation lan
- plo ation o e es
- Labo ato y o e es
- T Bo ing Logs 12
- eli al ile esign Calculations Summary 1
- Lab a y heet 4
- Li i an lasti Test epo t 2
- oist e ontent es lts 4
- ain i□e ist ib tion es 1
- n onfine o p ession Test epo t
- o pa tion epo t 2
- T ia ial Test es lts 2
- nalyti al Lab Test es lts 1
- Ben hing etail



1.0 EXECUTIVE SUMMARY

United Consulting has completed a geotechnical investigation for the Beaumont Industrial Park to be located to the south of Atlanta Boulevard in the Chattahoochee County Georgia lease area to the east of the airport for a proposed installation of the site services area below.

The geotechnical investigation program included 12 Test Borings and limited laboratory testing.

1. Below the ground surface boring B-1 encountered 2 feet of fill soils. The fill encountered consists of loose sand with traces of silt and clay and generally appeared to be free of debris and organic content with a tan to brown coloration. Test results indicate a bearing capacity of approximately 1000 psf.
2. Partially weathered rock was encountered in borings B-2 through B-4 at depths ranging from 1 foot to 2 feet. The general condition of borings B-1, B-2, and B-4 at depths ranging from 1 foot to 2 feet indicated a condition of weathering associated with the rock. It is noted that shallow rock may be present between and around the areas plotted.

Recommendations as encountered in each of the borings at depths ranging from 1 foot to 2 feet at the time of drilling on 24 hours after drilling. Recommendations should be made for this project. The contractor should be prepared to excavate and remove material as needed. Recommendations should be anticipated to fluctuate with the change of seasons during periods of heavy to high precipitation or to changes in the flood plain or water table for the area.

4. It is noted that the site is prepared as shown and it is the opinion that the proposed buildings can be supported on helical pier footings. Details and recommendations for foundations are included in the report.



2.0 PROJECT INFORMATION

The project site is located south of Atlantic Boulevard in Lithia Springs, Georgia. The project site is located in a residential neighborhood with streets and an association easement. The project site is adjacent to Atlantic Boulevard. The site is bounded by Atlantic Boulevard to the north and by residential easements to the east. The general location of the project site is shown on the attached site location map.

The topographic site plan was provided by the client dated 11/22/2019. The elevations at the site range from about 10 feet in the north to 7 feet along the creek running in the southeast portion of the site.

It is noted that the project will consist of street, station and development of a park which will include boardwalks, on-site trails, storage areas, and other amenities. The scope of this project is limited to the trail and the street station areas.

Based on an aerial and associated attachment for John Wiley at the date 11/2/2020, it is noted that the boardwalk elevations will be as follows:

Table 1: Boardwalk Pier Reaction Loads

Direction	Service Loads (kips)	Factored Loads (kips)
Vertical	2.4 LL	4 LL
Lateral	1.0	2

If the actual plans and site grading information vary significantly from the above anticipated estimates, consulting should be contacted to determine if other considerations should be evaluated and revised.



3.0 PURPOSE

The purpose of this geotechnical exploration was to assess the general type and condition of the subsurface materials at the project site and to provide foundation recommendations for bored piles retaining walls gaining earth ock stability on the other geotechnical related issues see pertinent to this project.



4.0 SCOPE

The scope of geotechnical exploration includes the following items:

1. Boring layout and logging negotiations

2. Visual reconnaissance of the site for a geotechnical standpoint

3. Logging of 12 standard penetration tests (SPT) borings to assess the quality and consistency of the subsurface soils

4. Visual evaluation of the soil samples obtained using field-testing program for the identification and classification

5. Laboratory testing consisting of fifteen (15) grain size analysis with hydrometer and fifteen (15) Atterberg Limits (liquid limit, plasticity index, and shrinkage limit) tests, two (2) standard penetration tests, five (5) cone penetration tests, and one (1) triaxial test on representative soil samples as well as shear strength and consolidation tests at representative locations

6. Analyzing the existing soil conditions with respect to the proposed construction and

7. Reporting this report to document the results of field-testing program and engineering analysis and to provide findings and general recommendations



5.0 SUBSURFACE CONDITIONS

The geotechnical exploration for the project consists of twelve Test Borings designated B-1 to B-12 along the tail race to the dam along the stream restoration area.

Initially each of the borings encountered a thin surficial layer. Beneath the surficial materials below the ground surface boring B-1 encountered 2 feet of fill soils. The fill encountered consists of loose and highly compressible silty sand. The Standard Penetration Test (SPT) values in the fill range from 2 to 4 blows per foot (bpf).

Below the fill in boring B-1 and the ground surface in the remaining borings typical residual soils of the local hydrogeology were encountered in the borings. The residual soils generally consist of very loose to very dense and highly compressible silty sand and clayey sand to fine silt with varying amounts of sand, silt, and clayey sand. The SPT values within the residual soils range from 2 to 4 bpf and those within the residual silts range from 2 to 4 bpf.

Typically the clayey sand was encountered in borings B-2 through B-12 at depths ranging from 1 foot to 2 feet. This is a test for soil that can be penetrated with a soil boring auger but has SPT values in excess of 100 bpf. The encountered clayey sand is highly compressible and highly plastic.

The groundwater table in borings B-1, B-2, and B-12 at depths ranging from 1 foot to 2 feet below ground surface in the borings is the depth that the boring cannot be advanced with a soil boring auger. The groundwater table generally represents a seasonal water table less than 2 feet above the base of the borehole.

Groundwater was encountered in each of the borings at depths ranging from 1 foot to 2 feet at the time of drilling. 24 hours after drilling, groundwater levels should be anticipated to fluctuate with the changes in seasonal precipitation of the local high precipitation area to changes in the flood plain or the watershed of the site.

The borings were backfilled with soil cuttings.

For a more detailed description of the subsurface conditions encountered please refer to the boring logs. The typical boring log data table is presented below.



Table 2: Summary of Subsurface Conditions

Location	Boring No.	Ground Surface Elevation ¹ (ft-msl)	Bottom of Fill Depth (ft)	24-hr GW Depth (ft.)	Depth to PWR (ft.)	Depth to Refusal (ft.)	Termination Depth (ft)
Tail	B-1	1					0
	B-2				1	1	1
	B-3	7		1	1	1	1
	B-4	7			2		0
	B-5		2		1	2	2
	B-6	2			2		0
Treatment Area	-1	0					1
	-2	2					1
	-3			4			1
	-4						1
	-5	0		4			1
	-6	0					1
Notes: 1. Ground surface elevations were estimated for site topography appropriate by the client at file date 11/22/201							



6.0 LABORATORY TESTING PROGRAM

Laboratory testing for this project includes fifteen (15) grain size analysis with hydrometer and fifteen (15) sieve analysis for total suspended solids (TSS) and total dissolved solids (TDS) tests. In addition, there are fifteen (15) soil moisture content tests, fifteen (15) soil specific gravity tests, and fifteen (15) soil density tests. The results of the moisture content tests are shown on the boring logs next to the respective soil samples tested. A detailed description of the laboratory tests and the laboratory test results are included in the Appendix.

In addition, there are fifteen (15) sulfate tests performed on representative soil samples and the results tabulated below.

Table 3: Soil Corrosivity Test Results

Boring	Depth (ft.)	Soil pH (S.U.)	Soil Resistivity (ohm-cm)	Chloride (mg/kg)	Sulfate (mg/kg)
B-1	2 - 4	7.4	740	44	4
B-2	2 - 4	7.4	400	4	40
B-3	2 - 4	4.4	1400	42	1
B-4	2 - 4	7.4	1400	40	0
B-5	2 - 4	7.0	100	4	1



7.0 DISCUSSION AND RECOMMENDATIONS

The following observations are based on the existing of the proposed construction the data obtained in the soil test borings at the site. The observations are in accordance with the best practices like those mentioned at the project site.

The observations indicate that the construction should be completed with the proposed materials early in the preparation of final construction drawings to determine if the observations are still applicable. It should be re-evaluated as needed.

7.1 Existing Fill

Below the ground surface being B- is approximately 2 feet of fill soils. The fill mentioned consists of loose and with traces of silt and clay. Generally, it appears to be free of debris and organic content. It has a tan to light brown color. Test results are as follows: blow count of 10 to 15 blows per foot.

Since any site containing non-existing fill materials it is not known to find deep areas of fill, soft soils, trash pits, or debris topsoil. Below the construction blast or other suitable materials within existing fill materials. The quality of the fill should be the final state at the time of construction by proofrolling and possibly the excavation of test pits and soft or other suitable soils if mentioned should be done for the area of the planned construction. The observations indicate that the project budget in the construction of the area that areas containing loose consistency soils that cannot be densified in place or other suitable materials during the overall construction within the fill.

7.2 Site Preparation

In order to develop a plan for the existing vegetation and trees in the site, the following should be done for the area of the proposed construction. The overall of trees should include the overall of the site. The height of trees should be at least 10 feet below the ground surface.

Any existing underground utilities should be located to at least 10 feet outside the perimeter of proposed building footprints. Any utility lines should be located and any abandoned utility pipes should be left in place within the non-structural areas of the site. They should be filled-in with concrete with a depth of 2 feet. A minimum depth of at least 100 psi.

In order to place any concrete fill or construction areas to be filled, shallow foundations, slabs, and piers should be proofrolled with a fully loaded trailer. The proofrolling should be performed in the observation of the geotechnical engineer or his representative so that areas where the proofrolling is a type of proofrolling may be treated by a method or by the geotechnical engineer. This method may consist of nailing and backfilling with suitable concrete fill replacing with aggregate and a layer of sheet piling or other method that is deemed suitable.



Due to the presence of non-competent existing fill soils, a easement requiring stabilization and other special approval with engineering fill shall be anticipated and budgeted for during site preparation.

7.3 Difficult Excavation

Initially, the contractor shall assess and note the conditions in borings B-2 through B-4 at depths ranging from 1 foot to 2 feet. Geotechnical logs in borings B-1, B-2, and B-4 at depths ranging from 1 foot to 2 feet indicate conditions requiring and/or blasting associated with the rock. It is noted that generally expected for the mass grading of the site, the note that shallow rock may be present between areas for the easement plot.

It is also important to note that depths to and/or an average shall be noted in the geotechnical log and an average shall be noted in the geotechnical log at shallow depths between and/or the borings for this study.

Typically, the contractor shall loosen by ripping with large rippers or single tooth rippers in mass excavation. The use of specialized excavation equipment such as backhoes or possibly blasting is typically required for excavation in confined trench excavations. Relatively soft and loose rock typically requires blasting for overall mass excavation.

Notions relating to the following definitions for rock are included in the definitions and help a contractor to interpret the rock excavation requirements.

1. General excavation by material copying an original volume of more than 1 cubic yard which cannot be excavated with a single-tooth ripper and by a bucket or a loader having a minimum capacity of not less than 4000 lbs. single wheel loader.
2. Trench excavation by material copying an original volume of more than 12 cubic yards which cannot be excavated with a backhoe having a bucket capacity of not less than 4000 lbs. single wheel loader and rock teeth.

7.4 Groundwater Considerations

Groundwater conditions in each of the borings at depths ranging from 1 foot to 2 feet at the time of drilling 24 hours after drilling. Groundwater is not expected to significantly impact construction. Groundwater levels shall be anticipated to fluctuate with the change of seasons during periods of dry or high precipitation or other changes in the flood plain or water table for the area.

7.5 Caving Considerations

All excavations shall be conducted in accordance with the occupational safety and health regulations regarding the flattening of the excavation site and the use of shoring may be needed to maintain stability during construction.

7.6 Foundation Design and Construction

Shallow spread footings were initially considered for this project however due to the presence of soft loose soils within the upper five to ten feet below ground surface and the presence of shallow ground water shallow spread footings are not considered a viable foundation option for the boardwalk project. Helical piles were then considered as a cost-effective deep foundation system for the boardwalk project.

Helical piles are installed by rotating helical anchor shafts through the upper oblique bearing strata opening on the anchor and the specific pile type helical piles may be designed for a working compressive capacity of 10 tons. The helical piles may have an uplift capacity similar to the compression capacity provided by the efficient bearing of the helical pile lead section. Lateral resistance is typically provided by installing piles at a batter of 1h 4 1/4" to 1h 1 1/4". The helical pile anchor is installed typically provides detailed design and installation details. Helical pile leads are typically provided with three helices with helices spaced typically at 12 inches the helical lead section of the total anchor helices are arranged in series typically for 10, 12 and 14 inches in diameter helical pile shafts come in different types and sizes ranging from 2 7/8" to 4 1/2" the helical pile configurations and sizes are also available by different helical pile suppliers. The capacity of the helical piles is controlled by the anchor that can be applied to the helical pile anchor assembly during installation. The nominal ultimate helical pile compression tension capacity is related to the total ease of installation.

During installation of the helical piles detailed records should be maintained by a representative of the contractor to verify pile type, location, length, installation conditions and estimate capacity. It is estimated that the allowable capacity of the anchor to be proposed dependent on installation procedure prior to mobilization and construction.

Depending on material availability and other factors it is possible that other deep foundation alternatives may be economically feasible for this project. It would be glad to evaluate other deep foundation options and provide recommendations for such if needed. Additional subsurface exploration will be required depending on the type of alternative deep foundation option considered.

Based on the load specifications noting the preliminary helical pile design calculations to determine helical pile size and configuration and estimate installation depths. The preliminary helical pile foundation system consists of two batter piles at 1h 4 1/4" installation angle with three helices 10", 12" and 14" diameter installed to depths between helical angles of 14 to 2 feet opening on the subsurface conditions encountered in the site borings complete along the boardwalk for this project. The batter helical piles are designed to provide 0 kips of effective compression load 24 kips of axial load and 2 kips of axial load for the lateral load 1 kips pile on the effective compression load. Note that helical pile installation contractor will develop their own design for the project and that the pile recommendations are for estimating foundation quantities and engineer's cost estimates. The preliminary helical pile foundation recommendations are summarized in Table 4 and the helical pile design calculations summary is included in the Appendix.



Table 4: Summary of Preliminary Helical Pier Design Recommendations

Structure	Boring No.	Depth to Dense Soil (ft-bgs) ($N_{60} > 30$ bpf)	Pile Type	Battered Pile Design Compression Service Load ¹ (kips)	Battered Pile Minimum Installation Torque (Ft-lb) ($K_t = 10 \text{ ft}^{-1}$)	Minimum Depth to Bottom Helix (ft-bgs)
Boatalk Tail	B-1	0	17 - dia 1- \square shaft 14 12 10 elies 2 Battered Piles at 1h 4 14° ft To e ating 10 00 t-lb	0	10	2
	B-2	1				1
	B-3	1				17
	B-4	1				17
	B-5	1				14
	B-6	2				24

Notes

- Battered piles are designed to handle the seismic lateral load 24.4 kips and lateral load 11 kips. The 11 kips seismic lateral load in each pile total of 22 kips per bent is transferred to pile axial compression and tension load respectively when the load is applied along the bent.
- At least one vertical pile load test using the top large helix 14" shall be performed to check the factored ultimate lateral helical pile ultimate rotational length bearing capacity for the installation to be eased in the field. The estimate initial to be provided above is based on a $K_t = 10 \text{ ft}^{-1}$.

7.7 Ground Floor Slabs

Ground floor slabs are designed as beams with a width of 120 inches. It is important to note that the floor slabs are often subjected to lateral loads due to the installation and other construction activities between completion of grading and slab construction. Therefore, the geotechnical engineer should evaluate the stability of the slabs during the construction phase. The geotechnical engineer to be consulted should be responsible for the design of the slabs with the engineer's fill to be at least 10% of its standard unit weight.



7.8 Earthwork

The onsite soils if free of organic and other deleterious materials shall generally be suitable for use as engineering fill with proper moistening of a locally available soil. It may be necessary to use other soils if it breaks progressively to meet a gradation requirement. It may also be necessary to use soil to meet a gradation requirement.

Due to the presence of high silt contents, some of the onsite soil may be sensitive to moisture variations during rainy seasons. These soils will be difficult to compact. A partial consolidation during the placement of wet earth on-site soils may need to be considered. The soils should be placed within a narrow range of their optimum moisture content, typically within about 1 percent of optimum moisture to achieve proper compaction. Typical estimates on suitable fill are no organic plasticity index less than 2 and a liquid limit of 40 or less, with not more than 0 percent greater than 4-in. These estimates should also be applied to potential borrow soils if necessary.

Moisture content should always be maintained to prevent saturation of exposed soils in case of serious rainfall. The surface of moist soils will also improve and reduce the soil moisture content. The degree of soil stability problems will also be dependent upon the practices taken by the contractor to help protect the soils for saturation during construction.

Moisture-density relationships should be prepared for each soil type set to provide a net essay for quality assurance testing. Soil moisture contents at the time of compaction should be a guide so that they are within moisture content limits that will allow the required compaction to be obtained.

7.9 Slopes

It is recommended that the fill is to be placed on existing slopes of grades greater than 4:1. The slopes should be benched to prevent sliding of the fill mass along the existing surface. This can be achieved by notching the slope face by at least about 1 foot horizontally with the top to blade as each lift is compacted. Typical benching detail is provided in the appendix.

Permanent slopes should be constructed no steeper than 2:1. All slopes of up to 20 feet in total height constructed to 2:1 should be acceptable for this project assuming proper benching and placement and compaction of engineering fill. Slopes greater than 20 feet should be evaluated for global stability and should be designed by a licensed geotechnical engineer. Slopes higher than 20 feet should be benched if less than 2:1. For less than 2:1 slopes, the topsoil or subsoil should be placed on slopes only if an appropriate level of quality control and compaction testing. In the specification of the geotechnical engineer is not planned, 2:1 slopes will not likely be achieved and flatter slopes should be considered.

All slopes should be protected for erosion during construction and provided with appropriate permanent vegetation. Other measures after construction, slopes should be protected for erosion. Non-off flow by means of benches and drainage ditches to prevent runoff on slopes. Although on-site channels appropriate vegetation should consist of fast-growing grasses that will rapidly establish a dense cover.



at o e the enti e slope Lan s aping on sisting of isolate sh bs an pine sta ill not p o i e
a e ate slope p ote tion

ini b il ing o etaining all setba k fo the nea est e ge of fo n ations of at least 10 feet
fo the est of slopes is e o en e ini setba k of feet is e o en e fo pa e ent
an bs

7.10 Fill Placement

oist e- ensity ete inations sho l be pe fo e fo ea h soil type se to p o i e ata ne essa y
fo ality ass an e testing The nat al oist e ontent at the ti e of o pa tion sho l be ithin
oist e ontent li its hi h ill allo the e i e o pa tion to be obtaine This is gene ally ithin
th ee pe entage points of the opti oist e The ont a to sho l be p epa e to in ease o
e ease soil ate ontent as nee e to a hie e the e i e eg ees of o pa tion

The fill sho l be pla e in thin lifts not to e ee -in h loose thi kness an o pa te e
e o en the fill be o pa te to at least pe ent of tan a o to T ai y
ensity ithin top t o feet an at least pe ent of tan a o to ai y ensity else he e
on the site o t en h ba kfill alk-behin type o pa tion e ip ent is typi ally se fo o pa tion
so e e o en pla ing fill in thin lifts not to e ee 4 in hes spe ially ithin oa ays an pa e ent
a eas

eote hni al nginee on a f ll-ti e basis sho l obse e g a ing ope ations n-pla e ensity tests
taken by that in i i al ill assess the eg ee of o pa tion being obtaine The f e en y of the testing
sho l be ete ine by the eote hni al nginee

7.11 Retaining Walls

The follo ing etaining all e o en ations pe tain to ast-in-pla e b il ing an site etaining alls
ithin the a eas e plo e an a e not inten e fo o la blo ko alls fo la blo ko
all a e planne on the site nite ons lting sho l be notifie be a se a itional e al ation ill be
e i e to p o i e e o en ations spe ifi to the planne all types an lo ations

The esign of etaining alls st in l e the ete ination of the late al p ess e that ill a t on the
all The late al ea th p ess e is a f n tion of the soil p ope ties s ha ge loa s behin the all an
a o nt of efo ation that the all an n e go This efo ation is basi ally epen ent pon the
elati e igi ty of the all syste

The a ti e ea th p ess e on ition e elops hen the all o es a ay fo the soil o e a s ffi ent
istan e s h as fo a f eestan ing antile e all The at-est on ition e ists hen the e is no late al
st ain on the soil s h as alls hi h a e igi ly est aine like a base ent o s b-fo n ation all The
passi e on ition o s hen the all o es into the soil

The follo ing e i alent fl i p ess es a e e o en e fo th ee ea th p ess e on itions



Table 5 - Lateral Earth Pressures

Earth Pressure Condition	Earth Pressure Coefficient	Recommended Equivalent Fluid Pressure
Active	0.33	2 psf/ft
At-Rest	1.00	4 psf/ft
Passive	2.67	12 psf/ft

Note that the design shall consider the effects of the passive pressure the effects of the design shall consider a safety factor of 2 to the state ultimate passive earth pressure in design

The equivalent fluid pressures are based on an assumed soil density of 120 pcf and an internal friction angle of 28 degrees and cohesion of 0 coefficient of friction of 0.4 for silty clay

The parameters listed above are based on a level properly compacted backfill no friction at the soil interface and no surcharge effects on design of retaining walls shall be included the buoyant unit weight of the in-situ soil shall be used to determine the lateral earth pressure The hydrostatic pressure based on the water table elevation shall be included in the analysis

Every opening in the wall shall not be subjected to backfill within 10 feet laterally behind any retaining wall unless the wall is designed for the increased pressure to be applied back The effects of openings in the wall shall be considered in this case retaining wall backfill shall be applied to the top of the tank or to a minimum density per adjacent drainage system has a footing on a foundation has a minimum width is equal to the length of any retaining walls shall be more than 10 feet in height

The retaining walls shall be designed by a professional engineer familiar with retaining wall design and registered in Georgia The design shall consider sloping backfills shall have an other factors affecting all loadings The design shall also consider global stability



8.0 LIMITATIONS

This report is for the use of **Gwinnett County** and the designs of the project described herein may only be applied to this specific project. Conditions and observations have been prepared using generally accepted standards of professional engineering practice in the state of Georgia. Other liability is expressly disclaimed. The firm is not responsible for conditions or observations of others.

The right to rely upon this report and the data therein may not be assigned without the written permission of the firm.

The scope of this evaluation is limited to an evaluation of the load-carrying capabilities and stability of the soils. It does not include a determination of the presence of contaminants or other geologic substances. The presence and absence are not implied or suggested by this report and should not be inferred.

Conditions and observations are based upon information furnished to us and obtained from the previously described exploration and testing program and our personal observations. They do not reflect conditions in subsurface conditions that may exist between the surface and the subsurface of the site. Hidden conditions between the surface and the subsurface may be necessary to evaluate conditions and observations based upon on-site observations of the conditions.

If the design location of the project is changed, the conditions obtained herein should be considered in all cases unless otherwise stated. Changes and observations are either effective or ineffective in design is complete. We should be given the opportunity to review the foundation planning plan and applicable portions of the specifications to confirm that they are consistent with the intent of our observations.

UNITED CONSULTING



APPENDIX

General Notes/Narrative of Drilling Operations

Figure 1 – Boring Location Plan

Exploration Procedures

Laboratory Procedures

SPT Boring Logs (12)

Helical Pile Design Calculations Summary (1)

Lab Summary Sheet (4)

Liquid and Plastic Test Report (2)

Moisture Content Results (4)

Grain Size Distribution Curves (15)

Unconfined Compression Test Report (5)

Compaction Report (2)

Triaxial Test Results (2)

Analytical Lab Test Results (16)

Benching Detail

GENERAL NOTES

The soil classifications noted on the Boring Logs are visual classifications unless otherwise noted. Minor constituents of a soil sample are termed as follows:

Trace	0 - 10%
Some	11 - 35%
Suffix "y" or "ey"	36 - 49%

LEGEND



Split Spoon Sample obtained during Standard Penetration Testing



Relatively Undisturbed Shelby Tube Sample



Groundwater Level at Time of Boring Completion



Groundwater Level at 24 hours (or as noted) after Termination of Boring

w Natural Moisture Content

LL Liquid Limit

PL Plastic Limit Atterberg Limits

PI Plasticity Index

PF Percent Fines (Percent Passing #200 Sieve)

γ_d Dry Unit Weight (Pounds per Cubic Foot or PCF)

γ_m Moist or In-Situ Unit Weight (PCF)

γ_{sat} Saturated Unit Weight (PCF)

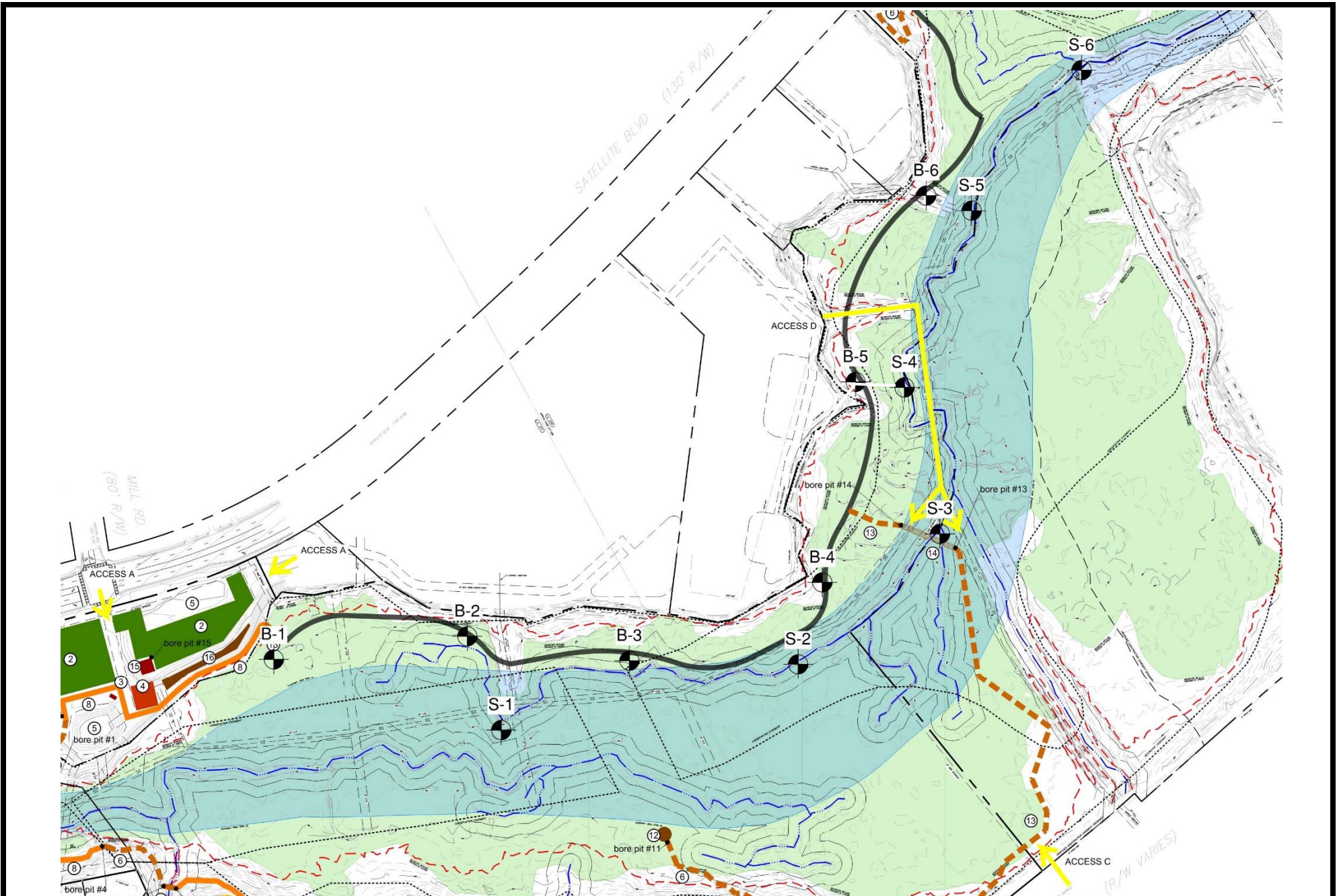
B L T T LL T

The test borings are made by mechanically advancing heli al hollow steel augers into the ground samples are collected at regular intervals in each of the borings following established procedures for performing the standard penetration Test in accordance with

Terzaghi's (1947) soil samples are obtained with a standard 140 mm diameter split barrel sampler. The sample is first seated into penetration any loose fittings and then driven an additional foot with the blow count of a 140-pounds hammer freely falling a distance of 30 inches. The number of blows required to drive the sampler the final foot is designated the standard penetration resistance. The driving resistance known as the blow count is related with the relative density of granular soils and the consistency of cohesive deposits.

The following table expresses soil consistency and relative densities based on standard penetration resistance values determined by the standard penetration Test.

	<u>SP</u>	<u>consistency</u>
	0-2	very soft
	3-4	soft
lay an	5-10	medium
ilt	11-20	stiff
	21-30	very stiff
	31-60	hard
	<u>SP</u>	<u>relative density</u>
	0-4	very loose
	5-10	loose
an	11-15	medium
	16-20	medium dense
	21-30	dense
	31-60	very dense



Scale:	NTS
Prepared:	SRT
Checked:	RIO
Project No.:	GCDWR-20-GA-04273-01

Notes

Client:	Gwinnett County Dept. of Water Resources
Site:	Beaver Ruin Wetlands Park South of Satellite Boulevard Duluth, Gwinnett County, Georgia
Title:	Boring Location Plan

FIG. 1



EXPLORATION PROCEDURES

Standard Penetration Test (SPT) borings

The 12 SPT borings designate B-1 through B-12 and are performed at the appropriate locations in site on the attached Boring Location map. The SPT borings are performed in general accordance with ASTM D 1586. Soil samples obtained during testing are analyzed by the project engineer and classified according to the Unified Soil Classification System. The nature of field operations is in line with the permit.

The test locations in the field are determined by the project engineer using a hand-held measuring instrument for existing site features. The test locations shall therefore be considered appropriate on surface elevations as obtained from topographic information by client dated 11/22/2017. Soils on surface elevations at the boring locations shall be considered appropriate.



LABORATORY PROCEDURES

Grain Size (Sieve) Analysis with or without Hydrometer

Grain size analysis tests are performed to determine the particle size distribution of selected samples tested. The grain size distribution of soils coarser than a number 200 sieve is determined by passing the samples through a standard set of nested sieves that are finer than the number 200 sieve. The percentage retained in each sieve and the grain size distribution curve for the percentage of settlement of the different size particles in the soil passes through a 200 sieve. The soil is soaked in a suitable liquid for a minimum of 24 hours. The soil is then placed in a glass jar with a hydrochloric acid solution taken at specific times. The graph is a function of the data. These tests are like those described by ASTM 421 and 422. The results are in Table 1. The procedure is

Liquid and Plastic Limits (Atterberg Limits)

Liquid Limit and Plastic Limit tests are used in the classification of the soils and provide an indication of the soil behavior with moisture change. The plasticity number is based on the Liquid Limit (LL) and the Plastic Limit (PL). The Liquid Limit is the moisture content at which the soil will flow as a heavy consistency and is the upper limit of the plastic range as determined in a standard test (ASTM 41). The Plastic Limit is the moisture content at which the soil begins to lose its plasticity as determined in a standard test (ASTM 41). The plasticity number is the difference between the Liquid Limit and Plastic Limit. The plasticity number is the ratio of the difference between the in-place moisture and the plastic limit to the plasticity limit. The data obtained are in Table 1. The procedure is

Moisture Content

The moisture content is determined for selected soil samples obtained in the split spoon sample representative portion of each sample as required and then placed in an oven and dried at 110 degrees Celsius for at least 1 to 2 hours. The weight of the soil is again weighed. The weight of the moisture lost during drying is determined. From this data the moisture content of the sample is then calculated as the weight of moisture divided by the weight of the soil expressed as a percentage. This test is done according to ASTM 221. The moisture content results are in Table 1. The procedure is

Moisture content is a self-indicator of a soil's compressibility. If the soil is to be used as fill, the moisture content may be compared to the range of moisture content for high plasticity soils. The moisture content may be a



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-1
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
890	Grass; 3" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=26; LL=34; PI=8 Shelby tube sample collected from 4'-6' bgs Groundwater encountered at 7 feet at the time of drilling and at 6 feet 24 hours after drilling	
	Sand - some clay and silt, trace mica; very loose; dark-tan (Residual) (SM)		1		1-1-2-2	3	6		30.9
	Clay - trace silt and sand; soft; orange-brown/gray		2		2-2-2	4	16		
		5	3		N/A	N/A	24		
885	- firm		4		2-3-3-3	6	1		26.4
	- soft		5		1-2-2-3	4	24		27.6
		10							
880									
	Sand - some silt, trace clay, trace mica, some rock; very loose; brown/dark gray	15	6		2-2-2	4	18		27.9
875									
	- trace rock; loose; tan-brown	20	7		3-4-5	9	18		
870									
	- firm	25	8		3-5-7	12	18		
865									
		30	9		4-6-7	13	18		
860	BORING TERMINATED AT 30 FEET								
		35							
855									
		40							
850									

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-2
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
890	Grass; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% Bulk sample collected from 0'-5' bgs: PL=22; LL=40; PI=18 NM=25.2% Shelby tube sample collected from 4'-6' bgs Groundwater encountered at 6 feet at the time of drilling and at 5 feet 24 hours after drilling
	Clay - silty, some sand; soft; orange-brown/gray (Residual) (CL) - firm; gray-tan	1		1-1-2-2	3	24	24.9	
		2		2-3-3	6	18		
885		3		N/A	N/A	24		
		4		2-3-2-2	5	24	26.0	
880	Sand - trace silt and clay, trace rock; loose; orange-brown/gray	5		2-4-5-4	9	24	21.8	
		10						
875	Partially weathered rock sampled as Sand - some silt, trace clay, some rock; very dense; brownish-gray	15		4-22-50/5	50/5	15	17.6	
870		19.5		50/0	50/0	0		
	AUGER REFUSAL AT 19.5 FEET	20						
		25						
		30						
		35						
		40						

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index
 NM=Natural Moisture



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-3
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
	Grass; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% Groundwater encountered at 3 feet at the time of drilling and at 1 feet 24 hours after drilling Shelby tube sample collected from 4'-6' bgs: 4'-4.5': PL=20; LL=38; PI=18; NM=22.7% 4.5'-5.5': PL=16; LL= 25; PI= 9; NM=20.8% 5.5'-6': Non-Plastic; NM=22.5%
	No Recovery	1	1	1-2-2-2	4	0		
885	Clay - some sand, trace silt; soft; orange-brown/gray (Residual) (CL)	2	2	2-2-2	4	10		
	- silty-sandy; gray-brown	5	3	N/A	N/A	24		
880	Sand - some silt and clay, trace rock; very loose; gray (SC)	4	4	1-1-1-1	2	24	34.9	
	- trace silt and clay (SP)	5	5	3-5-8-6	13	19	18.1	
	- firm; orange-brown/gray	10						
875								
	- some rock	15	6	7-9-9	18	18	19.1	
870								
	PWR sampled as Sand - trace silt and clay, some rock; very dense; gray	20	7	50/2	50/2	1	18.2	
865	AUGER REFUSAL AT 19 FEET							
		25						
860								
		30						
855								
		35						
850								
		40						

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index
 NM=Natural Moisture



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-4
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass & Pine Needles; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% Bulk sample collected from 0'-5' bgs: PL=35; LL=52; PI=17 NM=21.6% Shelby tube sample collected from 4'-6' bgs Groundwater encountered at 8 feet at the time of drilling and at 5 feet 24 hours after drilling	
885	Sand - some clay and silt, some mica; loose; orange-brown/tan-brown (Residual) (SM) - firm		1		2-4-5-6	9	24		25.7
			2		3-5-7	12	18		
			3		N/A	N/A	24		
880	- some silt, trace clay, some rock; loose; tan-brown/dark brown		4		3-3-4-4	7	24		20.2
			5		3-4-5-5	9	24		23.9
		10							
875	- firm		6		4-7-10	17	18		
		15							
870	- medium dense		7		7-10-16	26	18		19.0
		20							
865									
	Partially weathered rock sampled as Sand - some silt, trace clay, some rock; very dense; brownish-gray	25	8		7-10-50/5	50/5	15		
860									
			9		50/1	50/1	1		
		30							
855	BORING TERMINATED AT 30 FEET								
		35							
850									
		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index
 NM=Natural Moisture



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-5
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/21/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES				NOTES		
			NO.	TYPE	BLOWS/6"	N-VALUE		RECOV. (%)	W (%)
	Grass; 3" Topsoil	0						Automatic Hammer with Efficiency=94.7% Shelby tube sample collected from 4'-6' bgs Groundwater encountered at 8 feet at the time of drilling and at 6 feet 24 hours after drilling	
	Sand - trace silt and clay; loose; gray-brown (Fill)		1		2-2-4-5	6	24		13.9
885	Sand - some clay, trace silt; loose; orange brown/ gray-brown (Residual) - trace silt and clay		2		4-4-4	8	18		
		5	3		N/A	N/A	24		
	- firm		4		4-6-6-5	12	24		25.0
880	- loose		5		3-5-5-7	10	24		18.4
		10							
875									
	Partially weathered rock sampled as Sand - trace silt and clay, some rock; very dense; brownish-gray	15	6		50/5	50/5	4	15.4	
870									
		20	7		10-12-50/4	50/4	15		
865									
	- orange-brown/black/white		8		23-28-36	64	12		
		25							
	AUGER REFUSAL AT 26 FEET								
860									
		30							
855									
		35							
850									
		40							



BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: B-6
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/23/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
	Grass; 2" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=27; LL=46; PI=19 Bulk sample collected from 0'-5' bgs Shelby tube sample collected from 4'-6' bgs: 4'-4.5': PL=32; LL=57; PI=25; NM=27.9% 5'-6': PL=25; LL=35; PI=10; NM=40.8% Groundwater encountered at 8 feet at the time of drilling and at 6 feet 24 hours after drilling
890	Sand - some clay and silt, trace mica; very loose; orange-brown/red-brown (Residual) (SC)	1	1	1-1-2-2	3	12	23.6	
	- trace clay, some mica; red-brown/tan-brown	2	2	2-2-2	4	18		
	- some clay (SM)	5						
	Silt - sandy, some clay; soft; gray-brown (ML)	3	X	N/A	N/A	24		
885		4	1	2-1-2-2	3	12	19.9	
		5	1	1-2-2-1	4	9		
		10						
880								
	Sand - some silt, trace clay, some mica, trace rock; loose; orange-brown/gray-brown	15	6	1-3-2	5	18	40.0	
875								
		20	7	3-4-5	9	12	29.8	
870								
	- firm; orange-brown/gray-brown	25	8	6-6-11	17	18	22.8	
865								
	Partially weathered rock sampled as Sand - some silt, trace clay, trace mica, some rock; very dense; gray-brown	30	9	18-40-50/5	50/5	16		
860	BORING TERMINATED AT 30 FEET							
		35						
855								
		40						

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index
 NM=Natural Moisture



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-1
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
890	Grass; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=24; LL=39; PI=15 Groundwater encountered at 8 feet at the time of drilling and at 5 feet 24 hours after drilling	
	Sand - trace silt and clay, trace mica; very loose; red-brown/tan-brown (Residual)		1		2-1-2-2	3	4		20.7
	Clay - silty, some sand; firm; red-brown/gray (CL)		2		2-2-3-4	5	24		22.5
885	Sand - some clay, trace silt, trace rock; loose; gray-brown		3		2-4-3-2	7	19		18.0
	Clay - some sand, trace silt; firm; dark gray		4		3-2-3-2	5	24		38.1
	Sand - some clay, trace silt, some rock; very loose; dark gray		5		1-1-1-1	2	24		23.0
880		10							
	- trace clay; medium dense; gray-brown		6		5-10-11	21	18		
875	BORING TERMINATED AT 15 FEET	15							
870		20							
865		25							
860		30							
855		35							
850		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-2
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass; 3" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=25; LL=45; PI=20 Groundwater encountered at 5 feet at the time of drilling and at 3 feet 24 hours after drilling	
880	Sand - some clay, trace silt, trace rock; very loose; red-brown/orange-brown (Residual)		1		1-2-1-3	3	24		43.8
	Clay - some sand and silt; firm; orange-brown/gray (CL) - soft		2		2-2-4-4	6	24		29.6
			3		2-2-2-2	4	24		28.3
875	Silt - some sand, trace clay, trace mica; firm; gray-brown		4		4-4-4-4	8	24		34.0
	Sand - trace silt and clay, trace mica, some rock; very loose; orange-brown/gray		5		2-2-2-2	4	19		34.5
870		10							
	- some silt; loose		6		2-2-3	5	18		
	BORING TERMINATED AT 15 FEET	15							
865									
		20							
860									
		25							
855									
		30							
850									
		35							
845									
		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-3
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/22/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% Non-Plastic Groundwater encountered at 7 feet at the time of drilling and at 4 feet 24 hours after drilling	
	Sand - some clay, trace silt, trace mica; very loose; orange-brown/red-brown (Residual) (SM)		1		1-1-2-2	3	19		39.1
880	- some silt, trace gravel and clay; loose; dark tan		2		3-5-4-4	9	24		19.3
	Clay - some sand, trace silt; soft; brownish-gray	5	3		1-1-2-2	3	15		22.0
	Sand - trace silt and clay; loose; gray		4		2-3-4-4	7	24		23.4
875	Clay - trace silt and sand, trace mica; soft; brownish-gray	10	5		1-1-2-1	3	24		60.5
870									
	Sand - some silt, trace clay, some mica and rock; very loose; orange-brown/gray-brown	15	6		2-1-2	3	18		
	BORING TERMINATED AT 15 FEET								
865		20							
860		25							
855		30							
850		35							
845		40							



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-4
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/21/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES				NOTES		
			NO.	TYPE	BLOWS/6"	N-VALUE		RECOV. (%)	W (%)
885	Grass; 4" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=20; LL=26; PI=6 Groundwater encountered at 4 feet at the time of drilling and at 3 feet 24 hours after drilling	
	Sand - some clay, trace silt, trace mica; very loose; orange-brown/tan-brown (Residual)		1		1-1-2-3	3	24		19.9
	- orange-brown/gray (CL-ML)		2		2-2-2-2	4	24		23.4
	- trace clay; loose; dark gray		3		1-3-2-4	5	24		27.1
880	- firm; orange-brown/white/black		4		4-6-9-10	15	24		18.2
	- medium dense		5		8-9-12-17	21	24		13.8
875		10							
	- some rock; very dense		6		15-30-31	61	18		
870	BORING TERMINATED AT 15 FEET								
		20							
865									
		25							
860									
		30							
855									
		35							
850									
		40							
845									

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-5
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/23/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
880	Grass; 3" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=25; LL=34; PI=9 Groundwater encountered at 6 feet at the time of drilling and at 4 feet 24 hours after drilling	
	Sand - some clay, trace silt, trace mica; very loose; red-brown/tan-brown (Residual) (SM)		1		1-1-2-2	3	15		27.9
	- some silt, trace clay and rock; loose; gray-brown/dark tan		2		2-3-3-3	6	24		23.9
	- trace rock; very loose	5	3		2-1-2-2	3	19		21.5
875			4		1-2-1-1	3	24		20.8
	- some silt, trace clay; gray-brown/orange-brown		5		1-1-1-1	2	12		28.8
870		10							
	- loose		6		2-2-4	6	18		
865	BORING TERMINATED AT 15 FEET	15							
860		20							
855		25							
850		30							
845		35							
840		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Department of Water Resources BORING NO.: S-6
 PROJECT NAME: Beaver Ruin Wetlands Park DATE: 9/23/20
 JOB NO.: GCDWR-20-GA-04273-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
880	Grass; 3" Topsoil	0						Automatic Hammer with Efficiency=94.7% PL=22; LL=32; PI=10 Groundwater encountered at 4 feet at the time of drilling and at 3 feet 24 hours after drilling	
	Clay - trace silt and sand, trace mica; soft; orange-brown (Residual) (CL) - silty, some sand; stiff; dark brown		1		1-1-2-3	3	24		35.9
			2		3-5-4-4	9	24		32.1
	- trace silt; very soft; gray		5		1-1-1-1	2	24		
875			3		1-1-1-1	2	24		
	Sand - some clay, trace silt, trace rock; very loose; gray-brown - some rock; gray		4		1-1-2-1	3	24		34.1
			5		2-1-1-9	2	24	48.4	
870		10							
	- some silt, trace clay, some rock; medium dense		6		13-13-16	29	18		
865	BORING TERMINATED AT 15 FEET	15							
860		20							
855		25							
850		30							
845		35							
840		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index

Beaver Ruin Wetlands Park
Gwinnett County Department of Water Resources

Helical Pile Design Calculations Summary (Axial and Lateral Capacity)														
Structure	Boring ID	Ground Surface Elevation ¹ (ft-msl)	Depth to Dense Soil (ft-bgs) (N ₆₀ > 30 bpf)	Factored Axial Loads ² (Kips)	Service Level Axial Loads ² (Kips)	Factored Lateral Load ² (Kips)	Service Level Lateral Load ² (Kips)	Service Level Lateral Load Converted to Compression/Tension Load ³ (kips)	Pile Type ^{4,5}	Battered Pile Design Compression/Tension Service Load ³ (Kips)	Battered Piles Minimum Installation Torque ⁶ (Ft-lb) K _t = 10 ft ⁻¹	Minimum Depth to Top Helix (ft-bgs)	Minimum Depth to Bottom Helix Plate (Vertical Pile Length) (ft-bgs)	Estimated Helical Pile Tip Elevation ⁷ (ft-msl)
DWR Trail/ Boardwalk	B-1	891	>30	33.54	24.34	2.63	1.5	6.2	CHANCE SS175 - Square 1-3/4" Shaft 14", 12", 10" Helices (2 Battered Piles at 1h:4v (14°) @ ≥ 6 ft) Torque Rating 10,500 Ft-lb	30.5	6,108	18.5	25	866
	B-2	889	13.5									9.5	15	874
	B-3	887	18.5									10.5	17	870
	B-4	887	18.5									10.5	17	870
	B-5	888	13.5									7.5	14	874
	B-6	892	28.5									17.5	24	868

- Notes:
- (1) Ground Surface Elevations are interpolated from provided Topographic Plan provided by the client dated (file date) 11/22/2019 and should be considered approximate.
 - (2) Loads provided by John Pyle of PermaTrak in an E-Mail Attachment dated 11/23/2020
 - (3) Battered piles are designed to handle the axial and lateral Service Loads. The 1.5 kips Service Lateral Load in each pile (total of 3 kips per bent) is transferred to pile axial compression and tension load, respectively when the load is applied along the bent.
 - (4) Alternative pile sizes and helix size configurations may be used by the helical pile installer provided the minimum pile ultimate (Factored) capacities design loads specified for the project are met.
 - (5) We recommend a minimum FOS=2 for Compression and Tension Strength of helical piles.
 - (6) At least one vertical pile load test using the top large helix (14") should be performed to check the Kt factor used to calculate the ultimate helical pile ultimate (Nominal Strength) bearing capacity from the installation torque measured in the field.
 - (7) Final pile tip elevation to be determined in the field based on the minimum pile installation torque rating required to achieve the ultimate capacity of the pile.

**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Content %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)
Borehole Number	Sample ID					% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %	Moisture %	Dry (lb/cuft)								
													L.L.	P.L.			P.I.	L.I.		
B-1	1	Bag	0-2	SM	30.9	34	26	8	0.61	100.0	43.3	40.0	-	-	-	-	-	-	-	
B-1	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-1	4	Bag	6-8	-	26.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-1	5	Bag	8-10	-	27.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-1	6	Bag	13.5-15	-	27.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-1	4	Bag	6-8	-	26.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-2	1	Bag	0-2	-	24.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-2	1A	Bulk	0-5	CL	25.2	40	22	18	0.18	100.0	77.1	70	106.6	17.8	-	-	-	-	-	
B-2	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-2	4	Bag	6-8	-	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-2	5	Bag	8-10	-	21.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-2	6	Bag	13.5-15	-	17.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-3	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-3	3A	Shelby	4-4.5	CL	22.7	38	20	18	0.15	100.0	63.1	55	-	-	2.7	-	-	-	-	U
B-3	3B	Shelby	4.5-5.5	SC	20.8	25	16	9	0.53	100.0	45.8	40	-	-	2.7	-	-	-	-	U
B-3	3C	Shelby	5.5-6	SP	22.5	NV	NP	NP	NP	100.0	4.2	2	-	-	2.7	-	-	-	-	U
B-3	4	Bag	6-8	-	34.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-3	5	Bag	8-10	-	18.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-3	6	Bag	13.5-15	-	19.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-3	7	Bag	18.5-20	-	18.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-4	1	Bag	0-2	-	25.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 MOISTURE (Mc)
 NP - NO PLASTICITY
 NV - NO VALUE

United Consulting

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Content %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)
Borehole Number	Sample ID					% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %	Moisture %	Dry (lb/cuft)								
													L.L.	P.L.			P.I.	L.I.		
B-4	1A	Bulk (R)	0-5	SM	21.6	52	35	17	-0.79	100.0	45.6	42.0	101.3	20.6	2.7	-	26.7	97.9	-	T
B-4	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,R,C,S
B-4	4	Bag	6-8	-	20.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-4	5	Bag	8-10	-	23.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-4	7	Bag	18.5-20	-	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-5	1	Bag	0-2	-	13.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-5	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,R,C,S
B-5	4	Bag	6-8	-	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-5	5	Bag	8-10	-	18.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-5	6	Bag	13.5-15	-	15.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-6	1	Bag	0-2	SC	23.6	46	27	19	-0.18	100.0	47.5	45	-	-	-	-	-	-	-	
B-6	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,R,C,S
B-6	3A	Shelby	4-4.5	SM	27.9	57	32	25	-0.16	100.0	46.8	43	-	-	2.7	-	-	-	-	U
B-6	3B	Shelby	5-6	ML	40.8	35	25	10	1.58	100.0	65.3	60	-	-	2.7	-	-	-	-	U
B-6	4	Bag	6-8	-	19.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-6	6	Bag	13.5-15	-	40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-6	7	Bag	18.5-20	-	29.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-6	8	Bag	23.5-25	-	22.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
S-1	1	Bag	0-2	-	20.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
S-1	2	Bag	2-4	CL	22.5	39	24	15	-0.10	100.0	81	70	-	-	-	-	-	-	-	
S-1	3	Bag	4-6	-	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 REMOLDED (R)
 NP - NO PLASTICITY
 NV - NO VALUE

United Consulting

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Contant %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)
Borehole Number	Sample ID					% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %	Moisture %	Dry (lb/cuft)								
													L.L.	P.L.			P.I.	L.I.		
S-1	4	Bag	6-8	-	38.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-1	5	Bag	8-10	-	23.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-2	1	Bag	0-2	-	43.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-2	2	Bag	2-4	CL	29.6	45	25	20	0.23	100.0	71.6	65	-	-	-	-	-	-	-	-
S-2	3	Bag	4-6	-	28.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-2	4	Bag	6-8	-	34.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-2	5	Bag	8-10	-	34.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-3	1	Bag	0-2	-	39.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-3	2	Bag	2-4	SM	19.3	NV	NP	NP	NP	95.0	15.3	13	-	-	-	-	-	-	-	-
S-3	3	Bag	4-6	-	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-3	4	Bag	6-8	-	23.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-3	5	Bag	8-10	-	60.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-4	1	Bag	0-2	-	19.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-4	2	Bag	2-4	CL-ML	23.4	26	20	6	0.57	100.0	69.3	50	-	-	-	-	-	-	-	-
S-4	3	Bag	4-6	-	27.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-4	4	Bag	6-8	-	18.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-4	5	Bag	8-10	-	13.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-5	1	Bag	0-2	-	27.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-5	2	Bag	2-4	SM	23.9	34	25	9	-0.12	100.0	31.4	25	-	-	-	-	-	-	-	-
S-5	3	Bag	4-6	-	21.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
S-5	4	Bag	6-8	-	20.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 REMOLDED (R)
 NP - NO PLASTICITY
 NV - NO VALUE

United Consulting

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

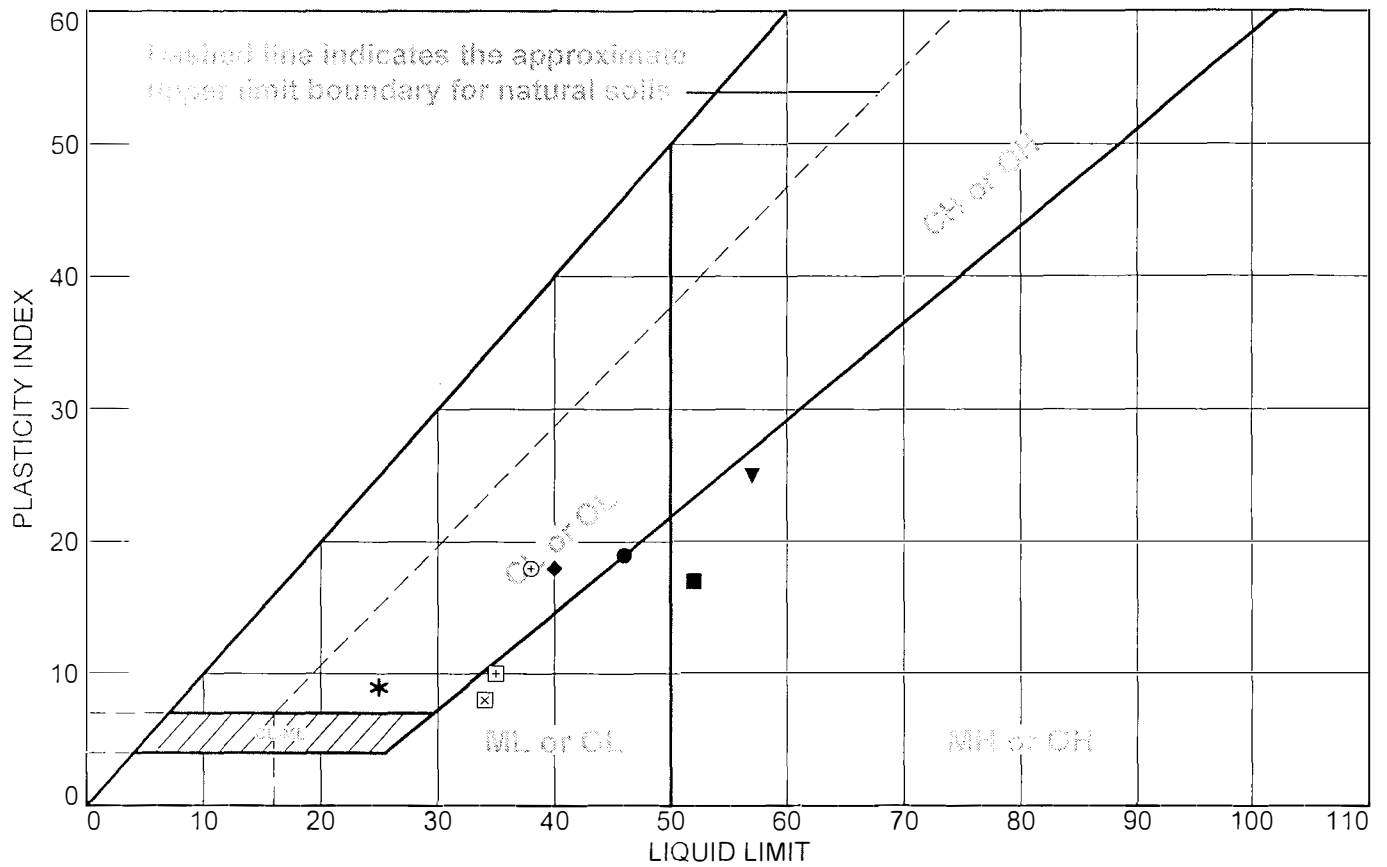
**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Content %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)	
										% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %			Moisture %	Dry (lb/cuft)			
Borehole Number	Sample ID					L.L.	P.L.	P.I.	L.I.												
S-5	5	Bag	8-10	-	28.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
S-6	1	Bag	0-2	-	35.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
S-6	2	Bag	2-4	CL	32.1	32	22	10	1.01	100.0	77.8	71	-	-	-	-	-	-	-		
S-6	4	Bag	6-8	-	34.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
S-6	5	Bag	8-10	-	48.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-		

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 REMOLDED (R)
 NP - NO PLASTICITY
 NV - NO VALUE

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

LIQUID AND PLASTIC LIMITS TEST REPORT



SOIL DATA								
	SOURCE	SAMPLE NO.	DEPTH	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
●		B-6	0-2 ft	23.6	27	46	19	SC
■		B-4(Bulk)	0-5.0'	21.6	35	52	17	SM
▲		B-3(Bottom)	5.5-6 ft	22.5	NP	NV	NP	SP
◆		B-2(Bulk)	0-5 ft	25.2	22	40	18	CL
▼		B-6 (Top)	4-4.5 ft	27.9	32	57	25	SM
*		B-3(Middle)	4.5-5.5 ft	20.8	16	25	9	SC
⊙		B-3(Top)	4-4.5 ft	22.7	20	38	18	CL
⊠		B-6 (Bottom)	5-6 ft	40.8	25	35	10	ML
●		S-3	2-4 ft	19.3	NP	NV	NP	SM
⊠		B-1	0-2 ft	30.9	26	34	8	SM

United Consulting

Norcross, Georgia

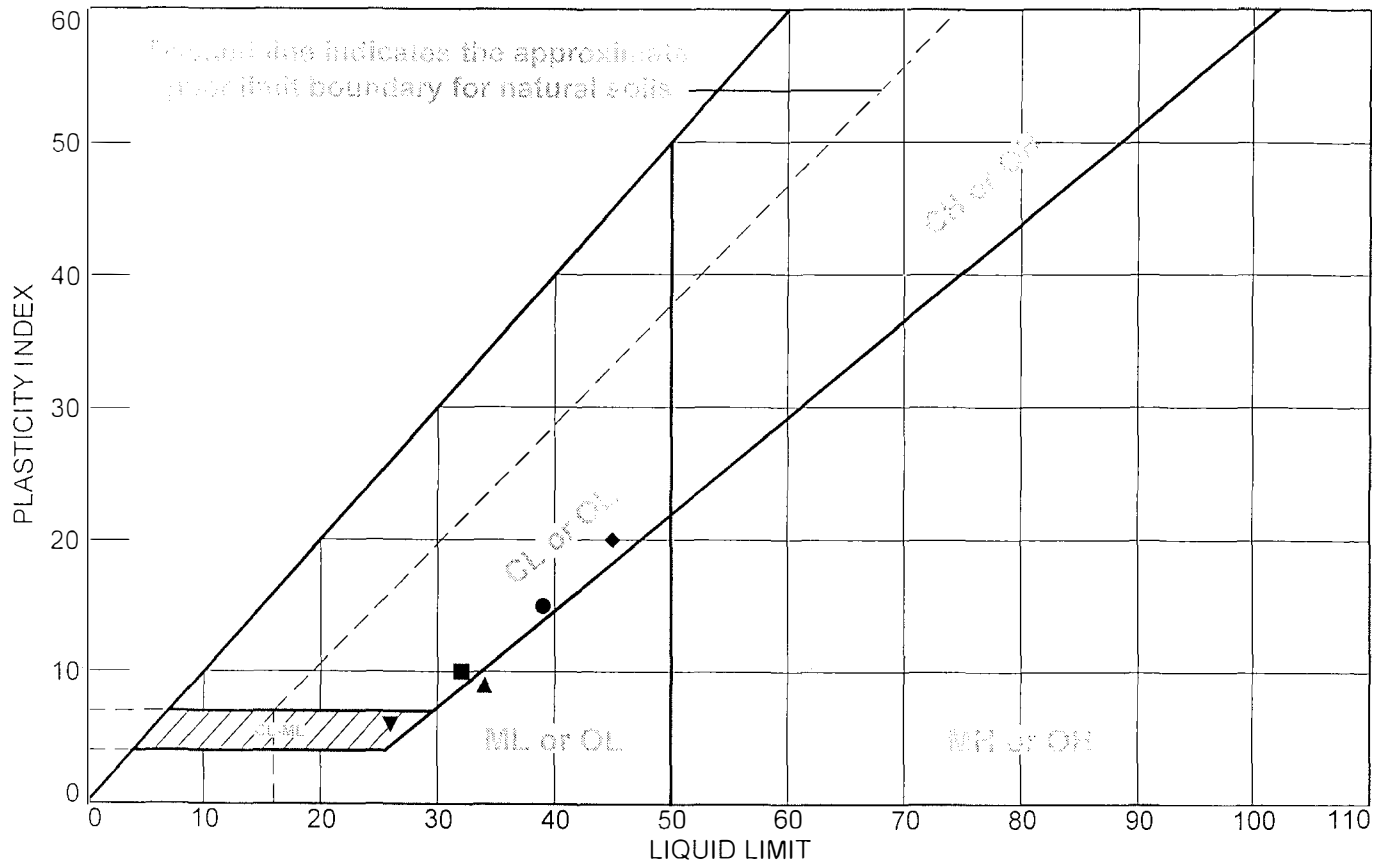
Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Project No.: GCDWR20GA0427301

Figure

LIQUID AND PLASTIC LIMITS TEST REPORT



SOIL DATA								
	SOURCE	SAMPLE NO.	DEPTH	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
●		S-1	2-4 ft	22.5	24	39	15	CL
■		S-6	2-4 ft	32.1	22	32	10	CL
▲		S-5	2-4 ft	23.9	25	34	9	SM
◆		S-2	2-4 ft	29.6	25	45	20	CL
▼		S-4	2-4 ft	23.4	20	26	6	CL-ML

United Consulting

Norcross, Georgia

Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Project No.: GCDWR20GA0427301

Figure

Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCDWR20GA0427301
 Project Name: Beaver Ruin Wetlands Park
 Received Date: 11/6/2020

Tested By: SH
 Date Tested: 11/6/2020
 Reviewed by: MS
 Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
B-6	6-8	37.65	174.74	152.00	19.9
S-1	6-8	32.94	165.60	128.99	38.1
B-3	18.5-20	37.63	158.21	139.63	18.2
B-5	13.5-15	33.06	143.91	129.14	15.4
S-5	4-6	37.85	196.42	168.33	21.5
B-6	18.5-20	37.48	193.91	157.97	29.8
S-5	6-8	33.00	244.70	208.27	20.8
B-2	8-10	33.07	235.05	198.87	21.8
S-4	8-10	33.17	176.09	158.79	13.8
B-5	8-10	32.92	195.64	170.41	18.4
B-4	6-8	27.11	198.00	169.27	20.2
B-4	18.5-20	27.07	172.80	149.58	19.0
B-2	6-8	32.81	201.74	166.86	26.0

Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCDWR20GA0427301
 Project Name: Beaver Ruin Wetlands Park
 Received Date: 11/6/2020

Tested By: SH
 Date Tested: 11/6/2020
 Reviewed by: MS
 Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
B-5	0-2	37.66	193.30	174.29	13.9
B-4	8-10	37.45	190.60	161.02	23.9
S-3	6-8	32.82	188.97	159.32	23.4
S-3	4-6	22.59	148.79	126.03	22.0
B-6	23.5-25	22.58	136.24	115.11	22.8
S-2	0-2	22.61	140.45	104.54	43.8
S-5	0-2	22.48	146.66	119.55	27.9
S-2	4-6	22.33	157.97	128.04	28.3
S-4	0-2	22.73	157.27	134.91	19.9
B-6	13.5-15	22.37	149.53	113.18	40.0
B-3	13.5-15	22.74	134.82	116.82	19.1
B-4	0-2	123.01	284.03	251.08	25.7
S-2	6-8	22.79	166.12	129.74	34.0

Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCDWR20GA0427301
 Project Name: Beaver Ruin Wetlands Park
 Received Date: 11/6/2020

Tested By: SH
 Date Tested: 11/6/2020
 Reviewed by: MS
 Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
S-2	8-10	33.05	226.05	176.59	34.5
S-1	8-10	32.81	170.66	144.85	23.0
B-2	13.5-15	33.29	206.69	180.79	17.6
B-2	0-2	32.71	180.77	151.24	24.9
B-7	18.5-20	37.56	176.88	143.84	31.1
B-1	13.5-15	33.03	187.36	153.73	27.9
B-1	8-10	33.03	190.46	156.37	27.6
B-1	6-8	32.95	197.84	163.45	26.4
S-1	0-2	33.14	69.19	63	20.7
B-3	8-10	33.16	211.25	183.98	18.1
B-3	6-8	32.85	182.16	143.53	34.9
B-5	6-8	37.48	199.51	167.13	25.0
S-1	4-6	37.58	190.37	167.1	18.0

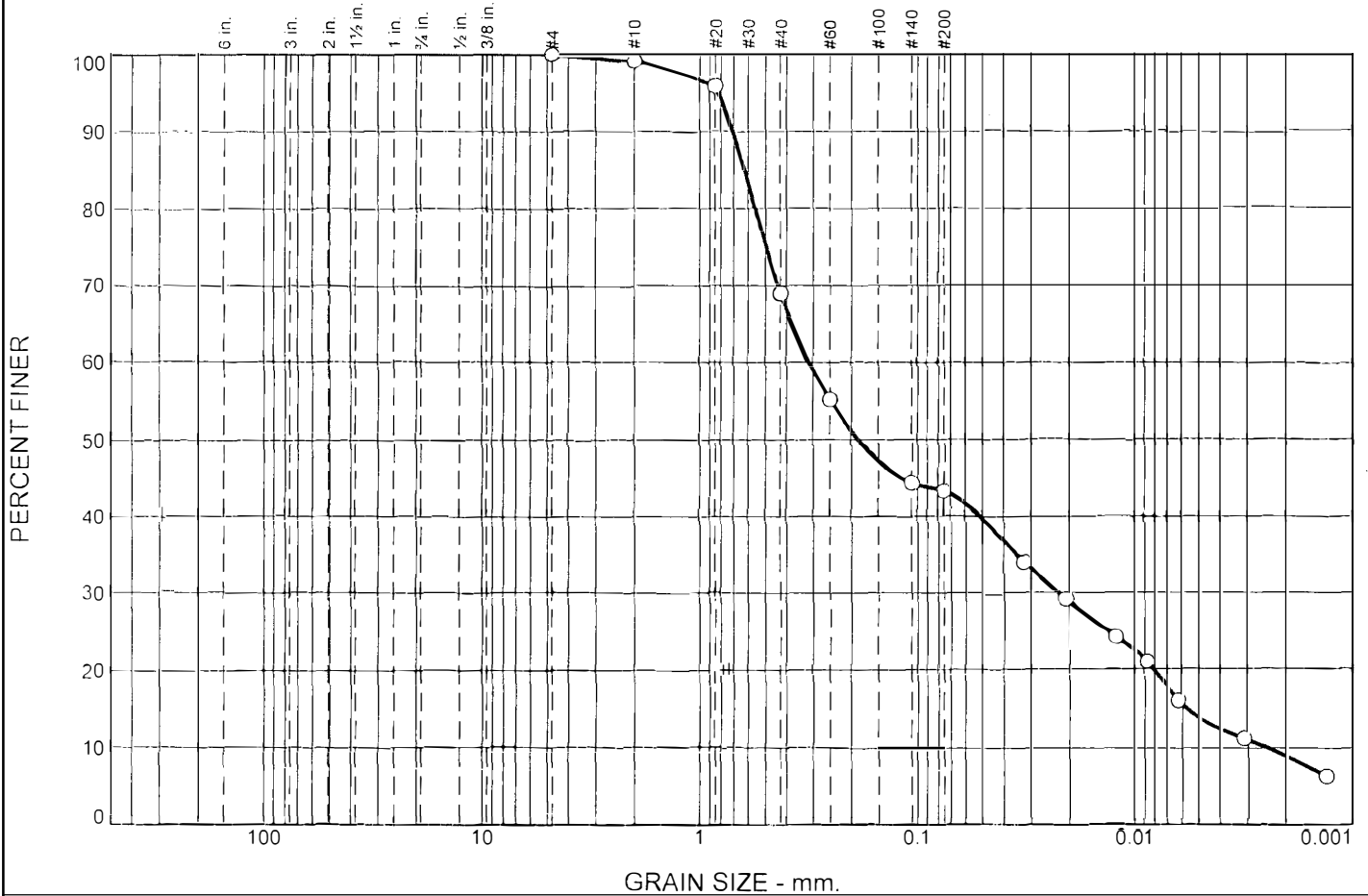
Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCDWR20GA0427301
 Project Name: Beaver Ruin Wetlands Park
 Received Date: 11/6/2020

Tested By: SH
 Date Tested: 11/6/2020
 Reviewed by: MS
 Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
S-5	8-10	22.50	161.73	130.58	28.8
S-6	6-8	14.92	124.14	96.37	34.1
S-3	0-2	15.00	123.29	92.86	39.1
S-6	8-10	14.96	122.06	87.13	48.4
S-4	6-8	14.73	105.35	91.41	18.2
S-3	8-10	14.94	113.87	76.57	60.5
S-4	4-6	14.70	127.67	103.56	27.1
S-6	0-2	14.41	106.02	81.82	35.9

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	56.7	29.6	13.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.1		
#20	96.0		
#40	69.0		
#60	55.2		
#140	44.3		
#200	43.3		

Material Description

Sand, some silt and clay, dark tan

Atterberg Limits

PL= 26 LL= 34 PI= 8

Coefficients

D₉₀= 0.7066 D₈₅= 0.6240 D₆₀= 0.3135
D₅₀= 0.1855 D₃₀= 0.0226 D₁₅= 0.0057
D₁₀= 0.0024 C_u= 128.08 C_c= 0.66

Classification

USCS= SM AASHTO= A-4(1)

Remarks

* (no specification provided)

Sample Number: B-1 Depth: 0-2 ft

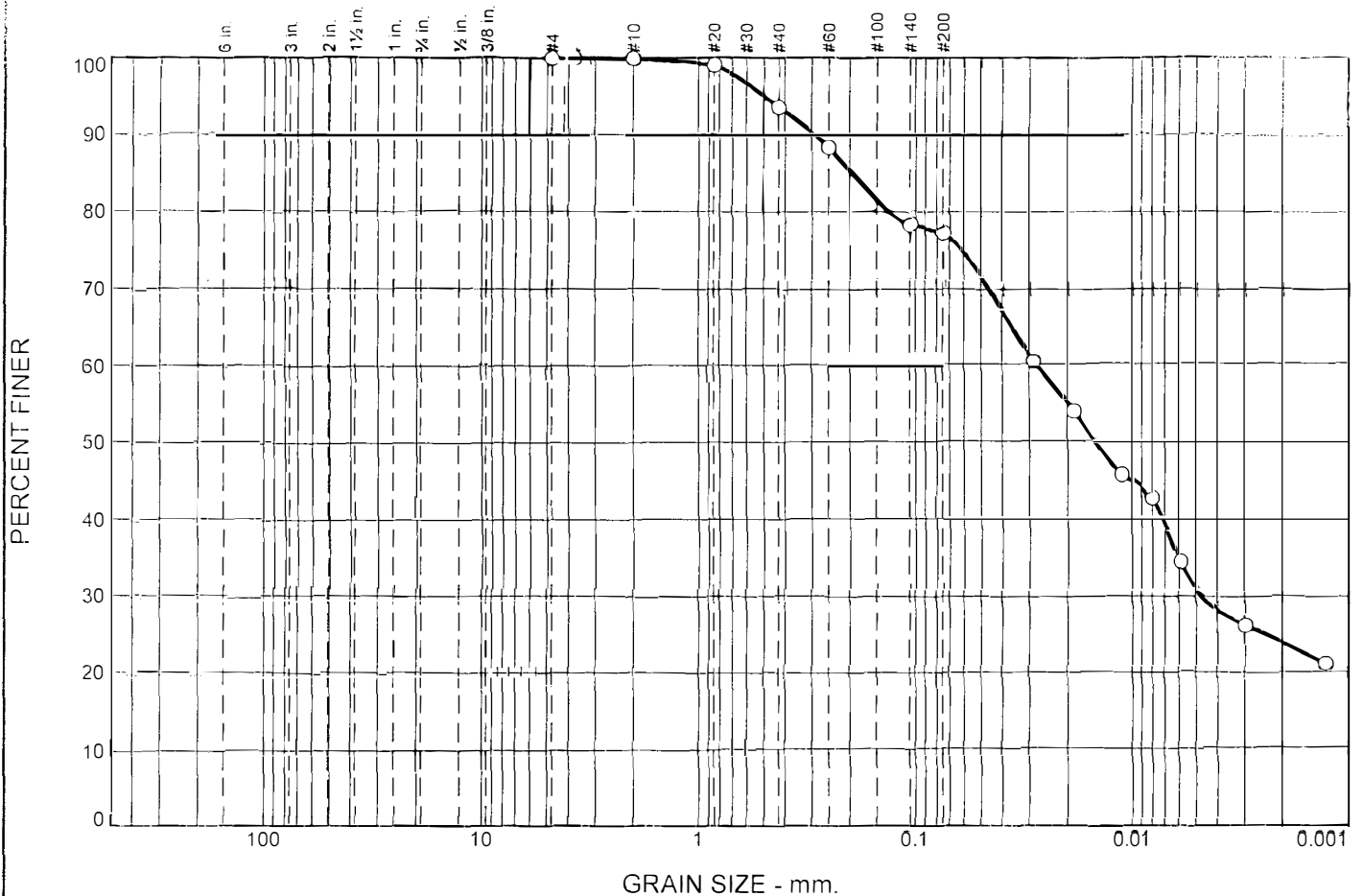
Date: 11/6/2020

United Consulting
Norcross, Georgia

Client: Gwinnett co dept of Water Resources
Project: Beaver Ruin Wetlands Park
Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	22.9	46.2	30.9

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	99.0		
#40	93.6		
#60	88.3		
#140	78.3		
#200	77.1		

Material Description

Clay-silty, some sand, gray tan

Atterberg Limits

PL= 22 LL= 40 PI= 18

Coefficients

D₉₀= 0.2913 D₈₅= 0.1959 D₆₀= 0.0276
D₅₀= 0.0149 D₃₀= 0.0047 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= CL AASHTO= A-6(13)

Remarks

* (no specification provided)

Sample Number: B-2(Bulk) Depth: 0-5 ft

Date: 11/6/2020

United Consulting

Norcross, Georgia

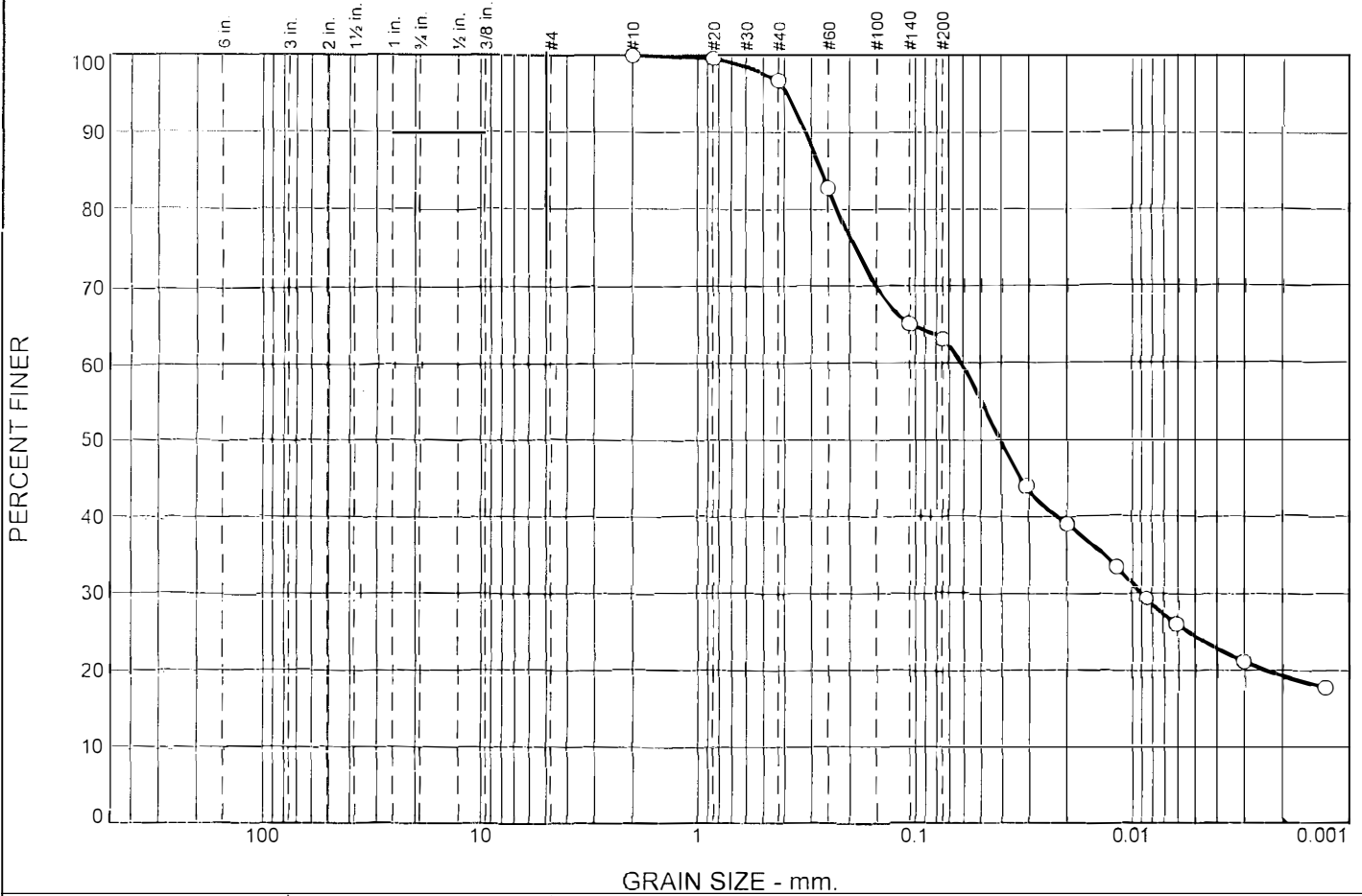
Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	36.9	38.7	24.4

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	99.6		
#40	96.8		
#60	82.8		
#140	65.1		
#200	63.1		

Material Description

Clay-silty-sandy, gray and brown

Atterberg Limits

PL= 20 LL= 38 PI= 18

Coefficients

D₉₀= 0.3184 D₈₅= 0.2689 D₆₀= 0.0613
D₅₀= 0.0406 D₃₀= 0.0090 D₁₅=
D₁₀= C_u= C_c=

Classification

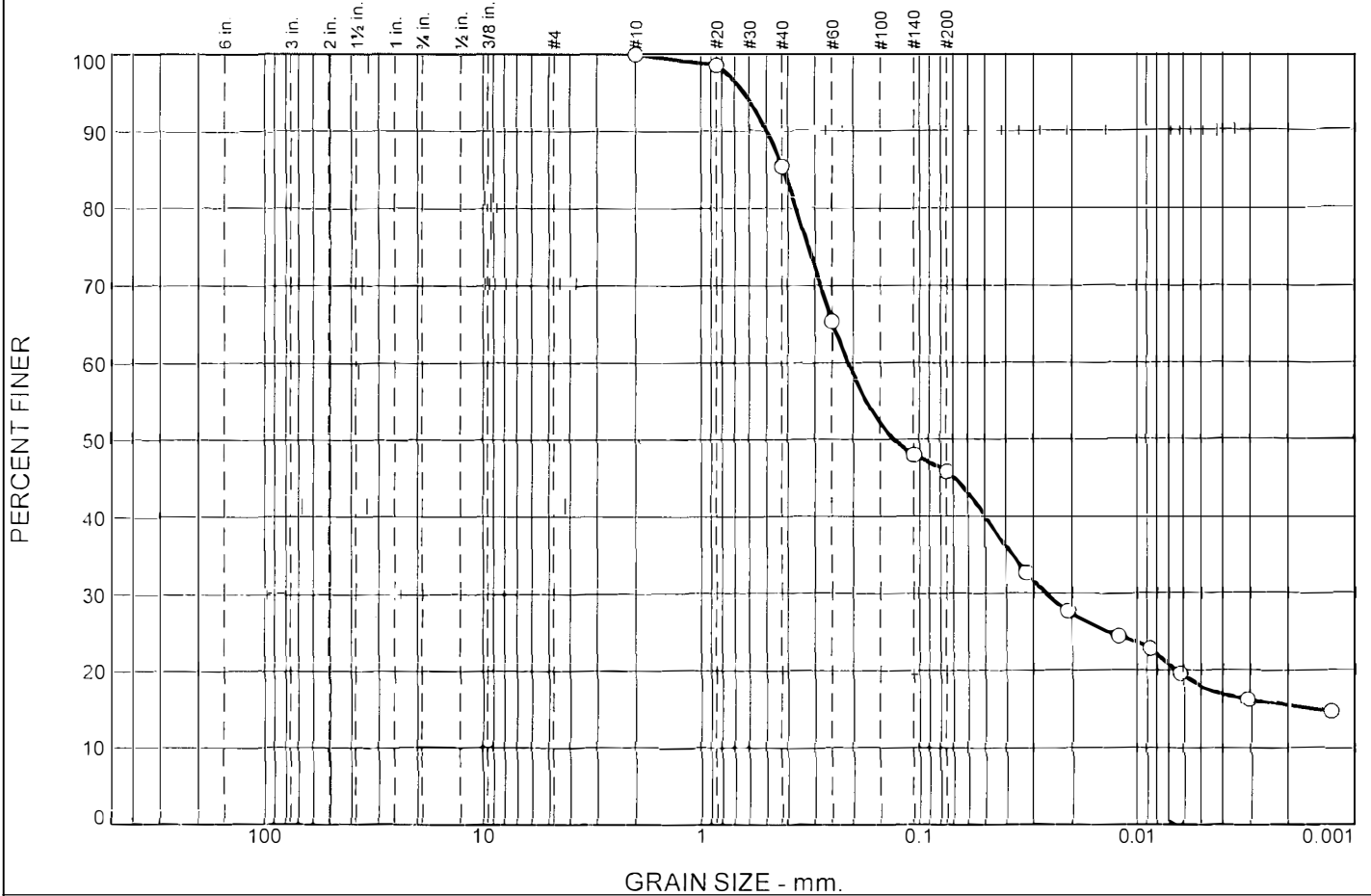
USCS= CL AASHTO= A-6(9)

Remarks

* (no specification provided)

Sample Number: B-3(Top) Depth: 4-4.5 ft Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	54.2	27.9	17.9

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	98.6		
#40	85.4		
#60	65.4		
#140	48.0		
#200	45.8		

Material Description

Sand, some silt and clay, gray

Atterberg Limits

PL= 16 LL= 25 PI= 9

Coefficients

D₉₀= 0.4978 D₈₅= 0.4198 D₆₀= 0.2111
D₅₀= 0.1298 D₃₀= 0.0265 D₁₅= 0.0016
D₁₀= C_u= C_c=

Classification

USCS= SC AASHTO= A-4(1)

Remarks

* (no specification provided)

Sample Number: B-3(Middle)

Depth: 4.5-5.5 ft

Date: 11/6/2020

United Consulting
Norcross, Georgia

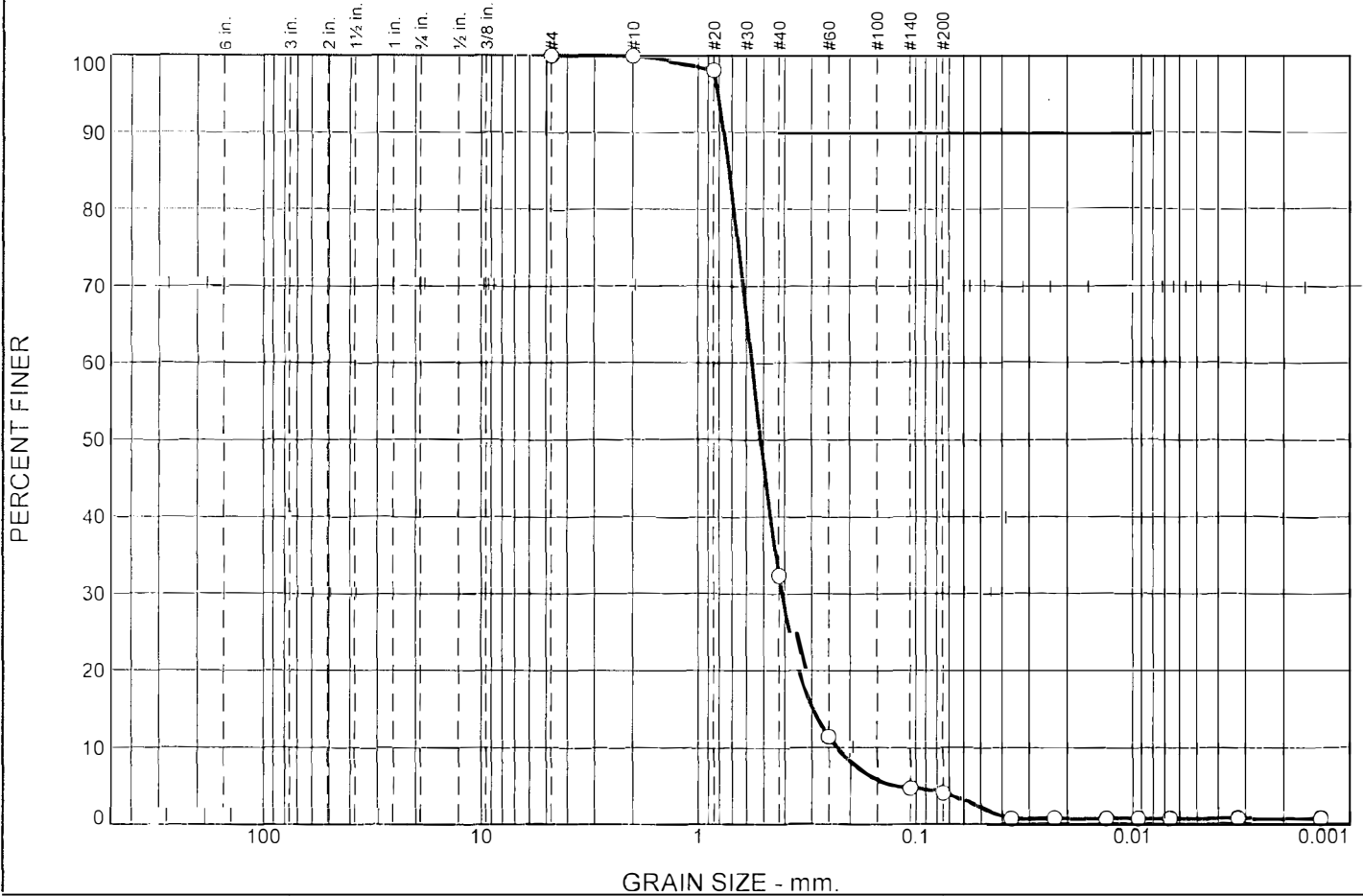
Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	95.8	3.5	0.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	100.0		
#20	98.1		
#40	32.3		
#60	11.4		
#140	4.8		
#200	4.2		

Material Description

Sand, trace silt and clay, gray

Atterberg Limits

PL= NP LL= NV PI= NP

Coefficients

D₉₀= 0.7625 D₈₅= 0.7208 D₆₀= 0.5660
D₅₀= 0.5150 D₃₀= 0.4117 D₁₅= 0.2971
D₁₀= 0.2294 C_u= 2.47 C_c= 1.31

Classification

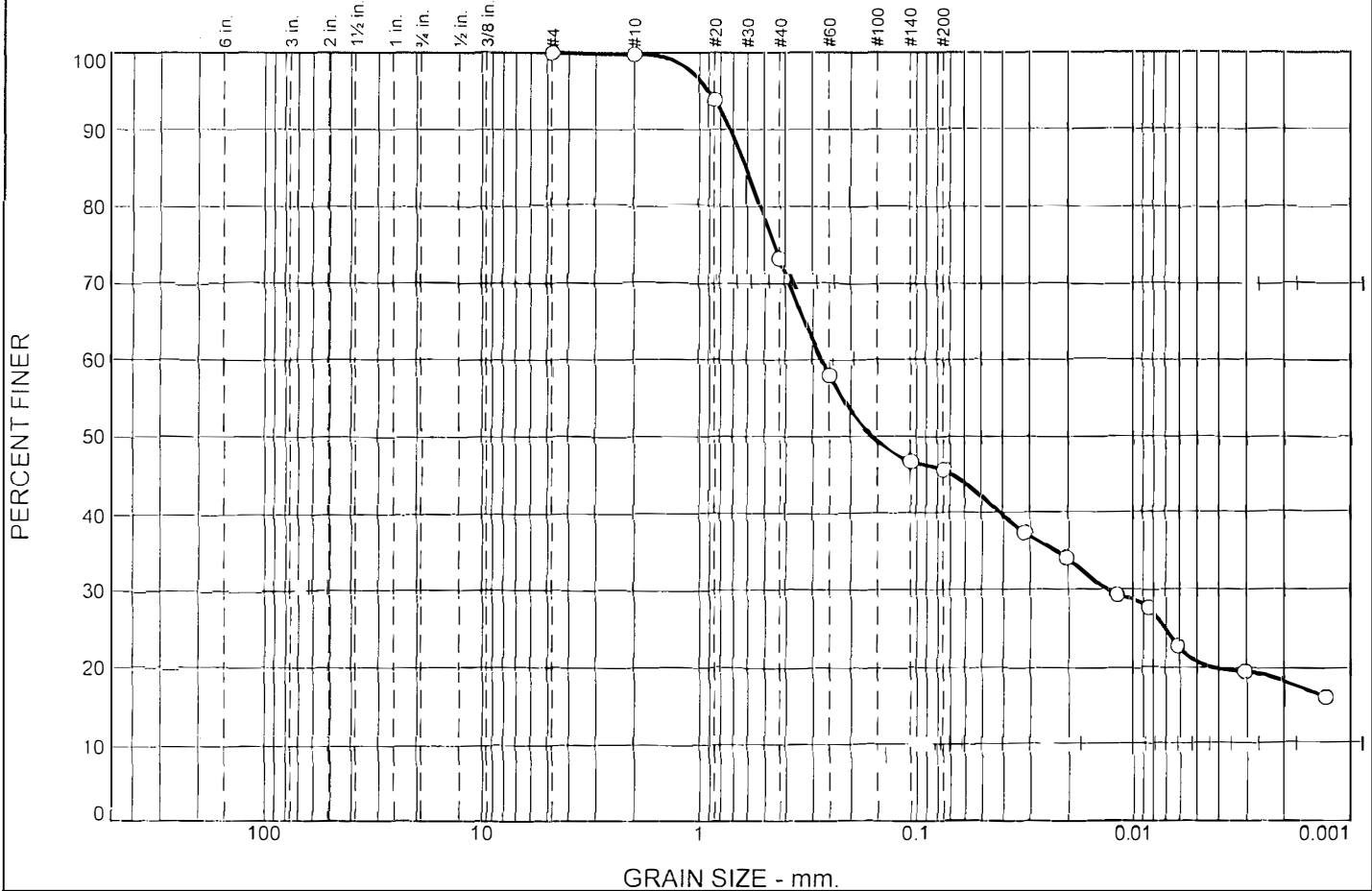
USCS= SP AASHTO= A-1-b

Remarks

* (no specification provided)

Sample Number: B-3(Bottom) Depth: 5.5-6 ft Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	54.4	24.9	20.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.8		
#20	93.8		
#40	73.2		
#60	58.0		
#140	46.7		
#200	45.6		

Material Description

Sand, some silt and clay, orange brown

Atterberg Limits

PL= 35 LL= 52 PI= 17

Coefficients

D₉₀= 0.7224 D₈₅= 0.6086 D₆₀= 0.2720
D₅₀= 0.1594 D₃₀= 0.0134 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= SM AASHTO= A-7-5(5)

Remarks

* (no specification provided)

Sample Number: B-4(Bulk)

Depth: 0-5.0'

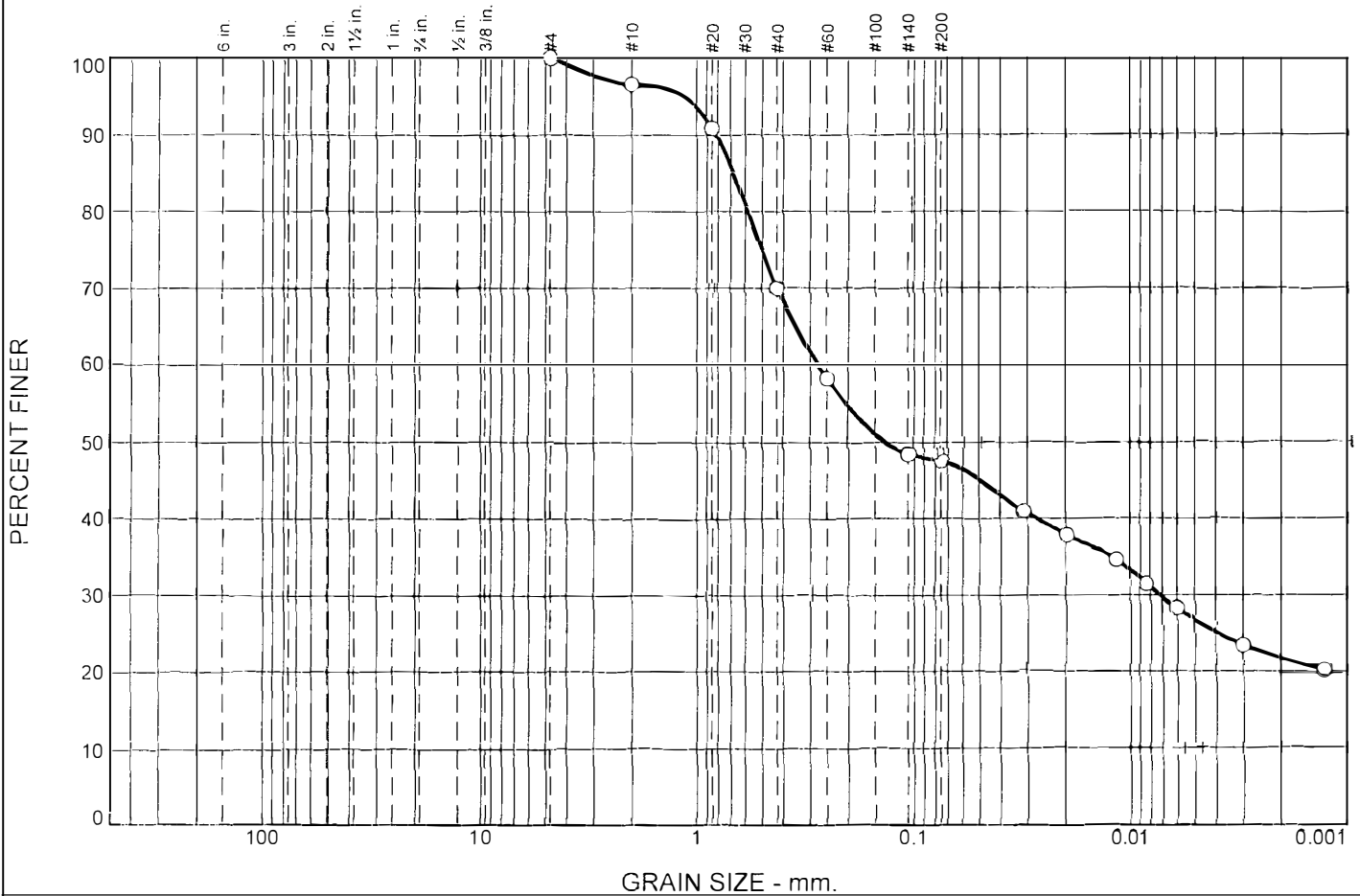
Date: 11/6/2020

United Consulting
Norcross, Georgia

Client: Gwinnett co dept of Water Resources
Project: Beaver Ruin Wetlands Park
Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	52.5	20.7	26.8

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	96.5		
#20	90.9		
#40	69.9		
#60	58.3		
#140	48.4		
#200	47.5		

Material Description

Sand, some clay and silt, brown

Atterberg Limits

PL= 27 LL= 46 PI= 19

Coefficients

D₉₀= 0.8171 D₈₅= 0.6803 D₆₀= 0.2748
D₅₀= 0.1348 D₃₀= 0.0072 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= SC AASHTO= A-7-6(6)

Remarks

* (no specification provided)

Sample Number: B-6 Depth: 0-2 ft

Date: 11/6/2020

United Consulting

Norcross, Georgia

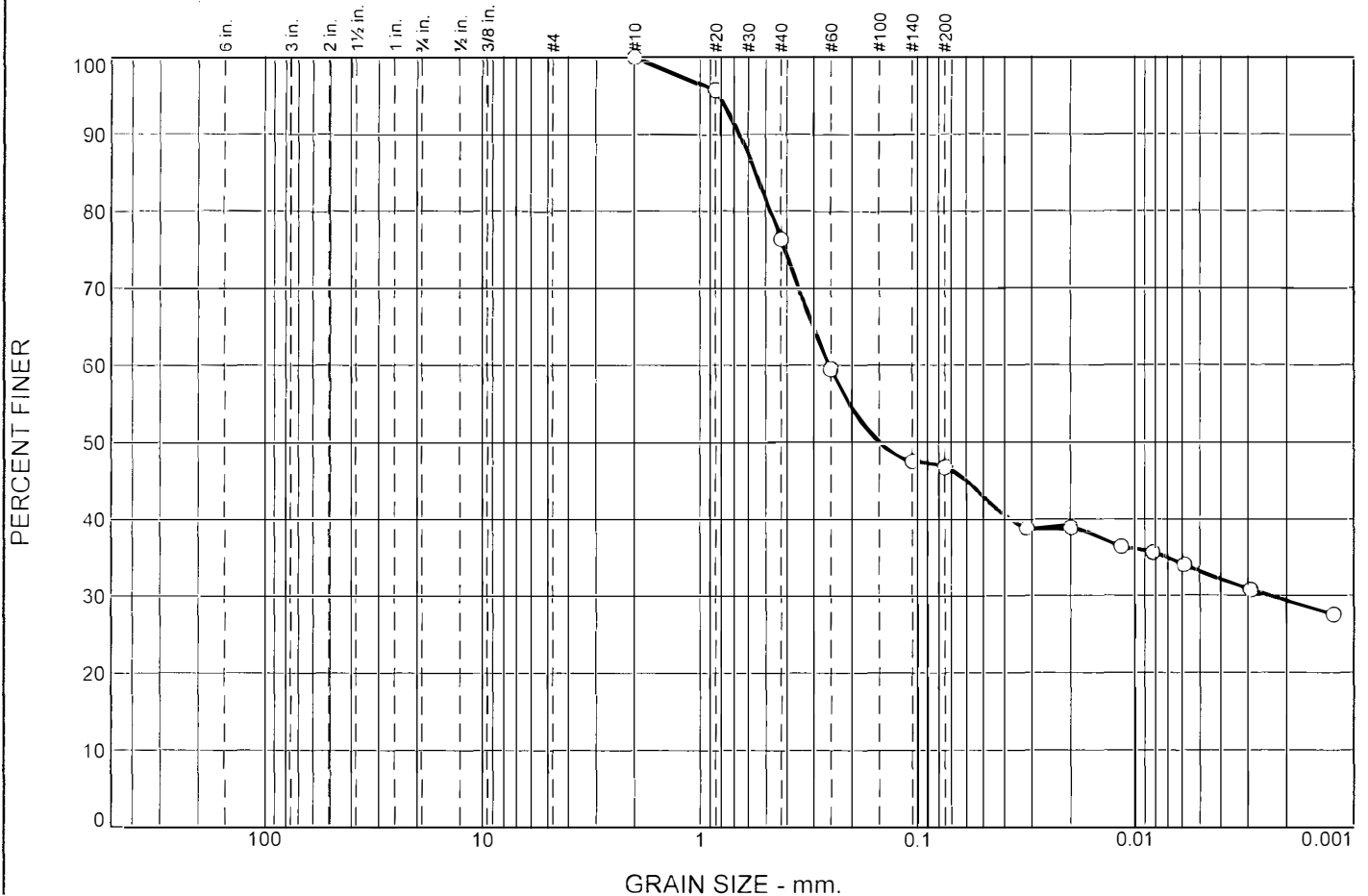
Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	53.2	13.6	33.2

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	95.8		
#40	76.3		
#60	59.5		
#140	47.6		
#200	46.8		

Material Description

Sand, some clay and silt, red brown

Atterberg Limits

PL= 32 LL= 57 PI= 25

Coefficients

D₉₀= 0.6580 D₈₅= 0.5541 D₆₀= 0.2543
 D₅₀= 0.1493 D₃₀= 0.0024 D₁₅=
 D₁₀= C_u= C_c=

Classification

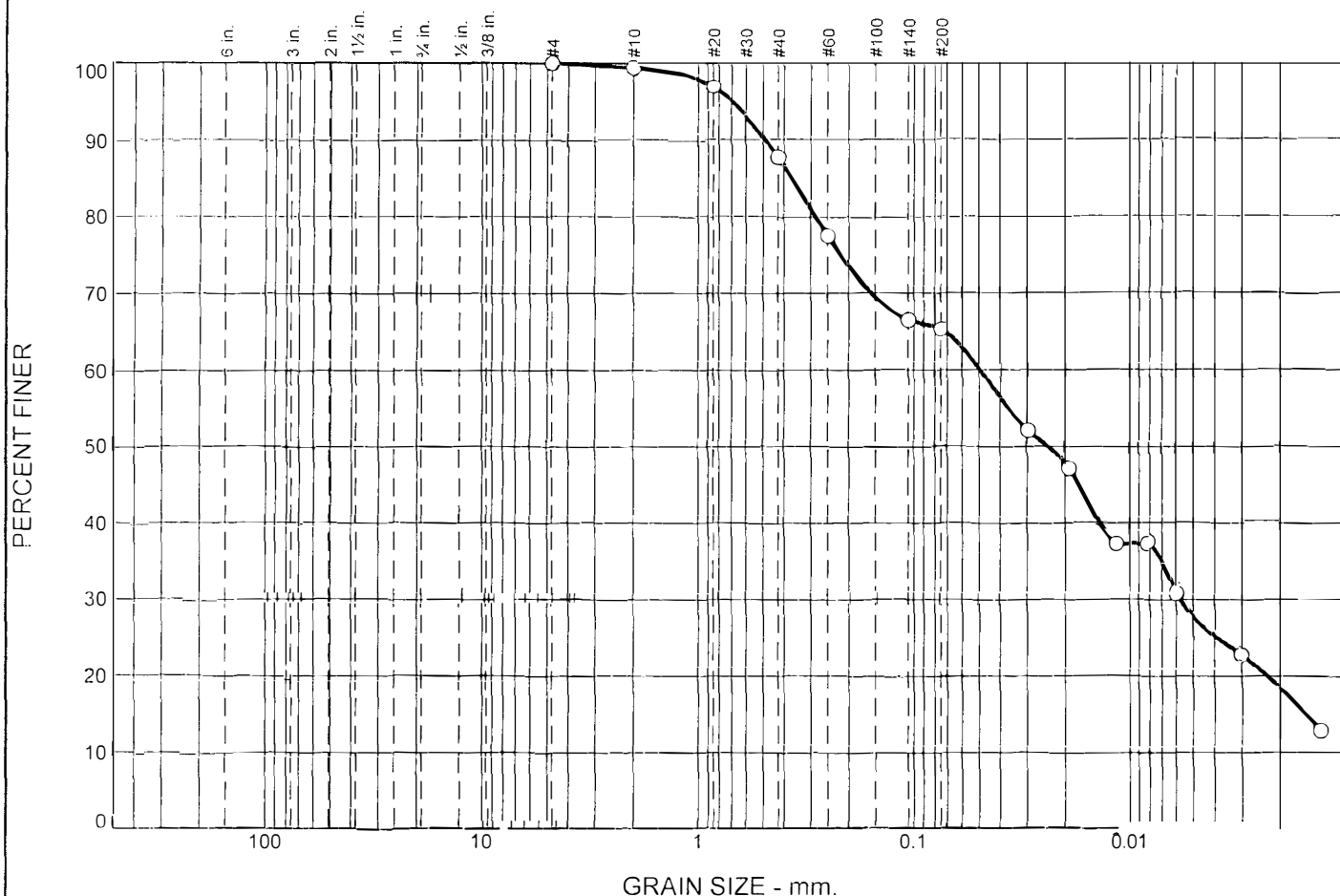
USCS= SM AASHTO= A-7-5(8)

Remarks

* (no specification provided)

Sample Number: B-6 (Top) Depth: 4-4.5 ft Date: 11/12/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	34.7	37.7	27.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.4		
#20	96.8		
#40	87.7		
#60	77.6		
#140	66.4		
#200	65.3		

Material Description

Silt-sandy, some clay, brown

Atterberg Limits

PL= 25 LL= 35 PI= 10

Coefficients

D₉₀= 0.4867 D₈₅= 0.3668 D₆₀= 0.0494
D₅₀= 0.0239 D₃₀= 0.0057 D₁₅= 0.0015
D₁₀= C_u= C_c=

Classification

USCS= ML AASHTO= A-4(5)

Remarks

* (no specification provided)

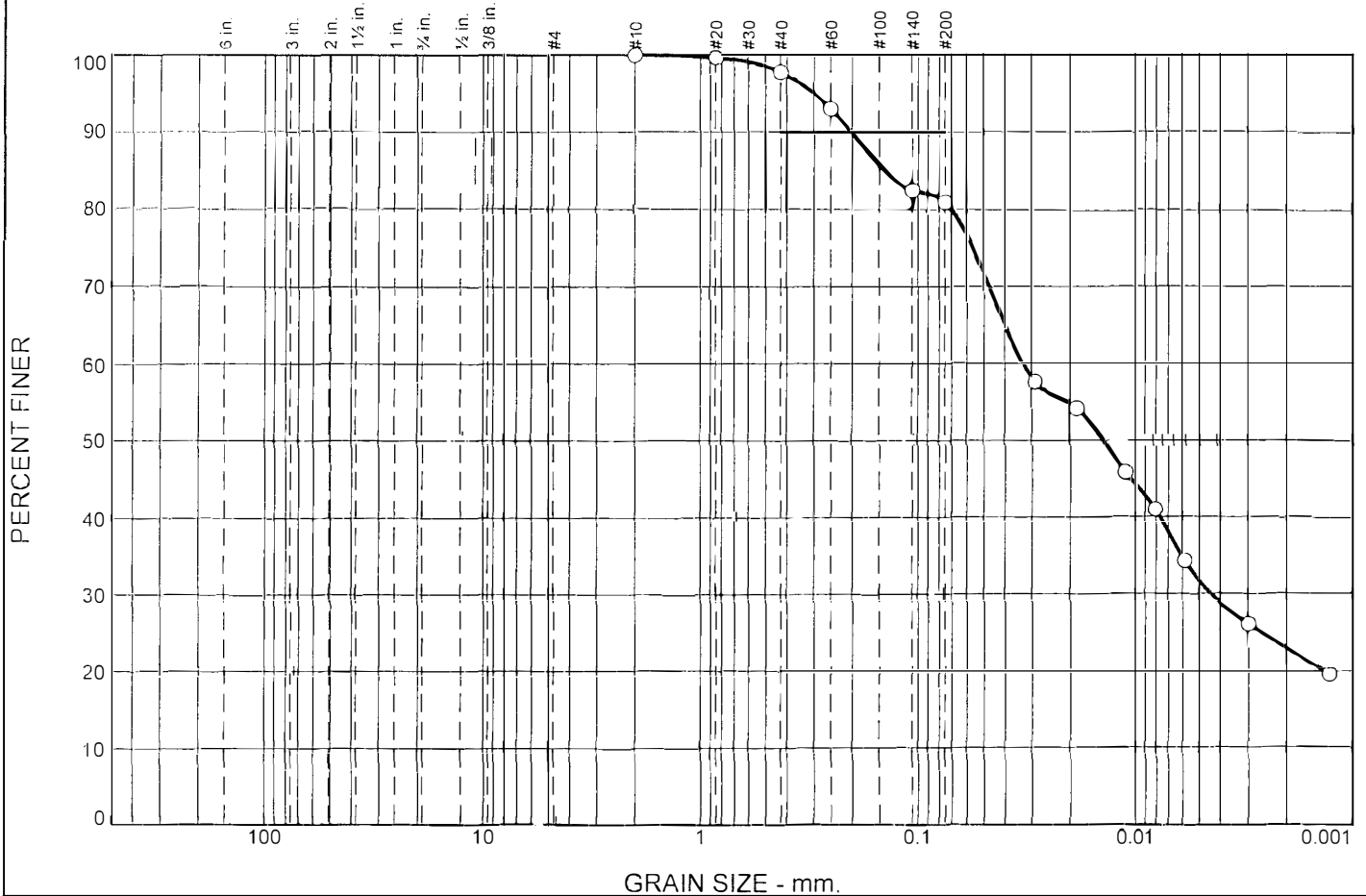
Sample Number: B-6 (Bottom)

Depth: 5-6 ft

Date: 11/6/2020

<p style="text-align: center; font-size: 1.2em;">United Consulting</p> <p style="text-align: center; font-size: 1.2em;">Norcross, Georgia</p>	<p>Client: Gwinnett co dept of Water Resources</p> <p>Project: Beaver Ruin Wetlands Park</p> <p>Project No: GCDWR20GA0427301</p> <p style="text-align: right;">Figure</p>
---	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	19.0	49.4	31.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	99.6		
#40	97.7		
#60	93.0		
#140	82.5		
#200	81.0		

Material Description

Clay-silty, some sand, gray

Atterberg Limits

PL= 24 LL= 39 PI= 15

Coefficients

D₉₀= 0.2023 D₈₅= 0.1423 D₆₀= 0.0332
D₅₀= 0.0141 D₃₀= 0.0044 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= CL AASHTO= A-6(12)

Remarks

* (no specification provided)

Sample Number: S-1 Depth: 2-4 ft

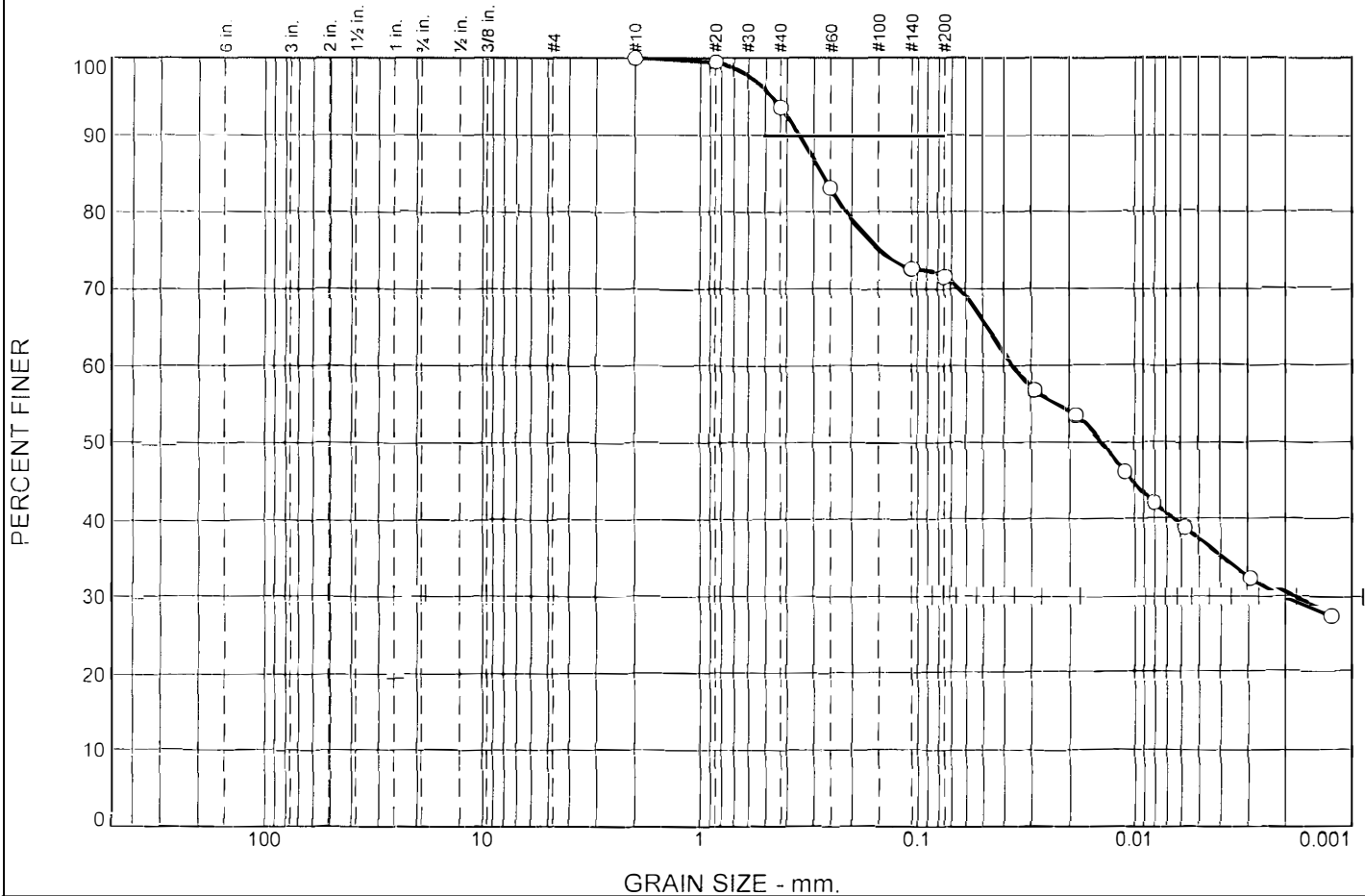
Date: 11/6/2020

United Consulting
Norcross, Georgia

Client: Gwinnett co dept of Water Resources
Project: Beaver Ruin Wetlands Park
Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	28.4	34.2	37.4

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	99.4		
#40	93.6		
#60	83.1		
#140	72.6		
#200	71.6		

Material Description

Clay, some silt and sand, orange tan

Atterberg Limits

PL= 25 LL= 45 PI= 20

Coefficients

D ₉₀ = 0.3495	D ₈₅ = 0.2745	D ₆₀ = 0.0365
D ₅₀ = 0.0143	D ₃₀ = 0.0021	D ₁₅ =
D ₁₀ =	C _u =	C _c =

Classification

USCS= CL AASHTO= A-7-6(14)

Remarks

* (no specification provided)

Sample Number: S-2 Depth: 2-4 ft

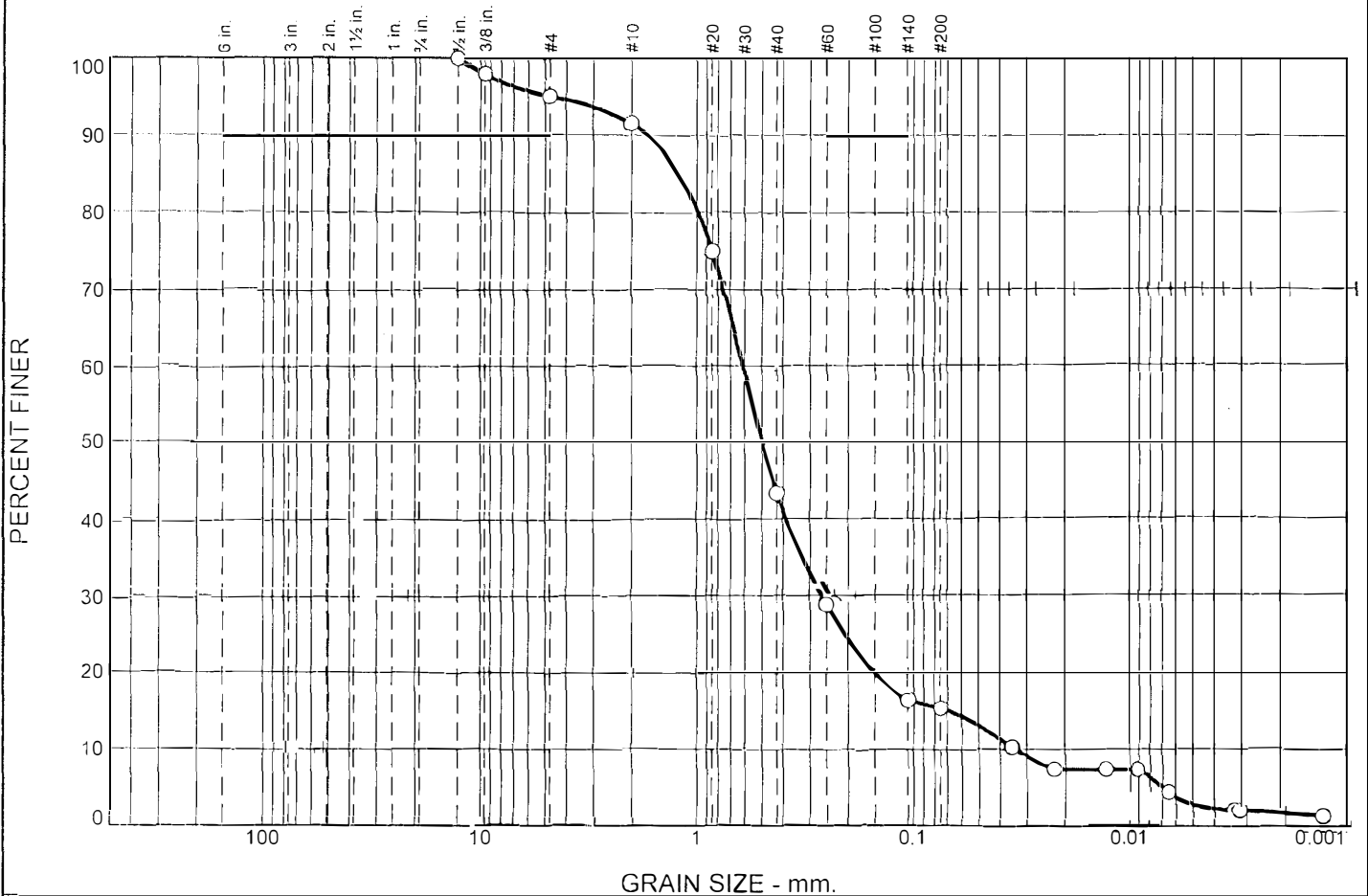
Date: 11/6/2020

United Consulting
Norcross, Georgia

Client: Gwinnett co dept of Water Resources
Project: Beaver Ruin Wetlands Park
Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	5.0	79.7	12.6	2.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.5	100.0		
0.375	97.9		
#4	95.0		
#10	91.5		
#20	74.9		
#40	43.4		
#60	28.9		
#140	16.5		
#200	15.3		

Material Description

Sand, some silt, trace gravel and clay, dark tan

Atterberg Limits

PL= NP LL= NV PI= NP

Coefficients

D₉₀= 1.6813 D₈₅= 1.2049 D₆₀= 0.6115
D₅₀= 0.4964 D₃₀= 0.2634 D₁₅= 0.0689
D₁₀= 0.0338 C_u= 18.07 C_c= 3.35

Classification

USCS= SM AASHTO= A-1-b

Remarks

* (no specification provided)

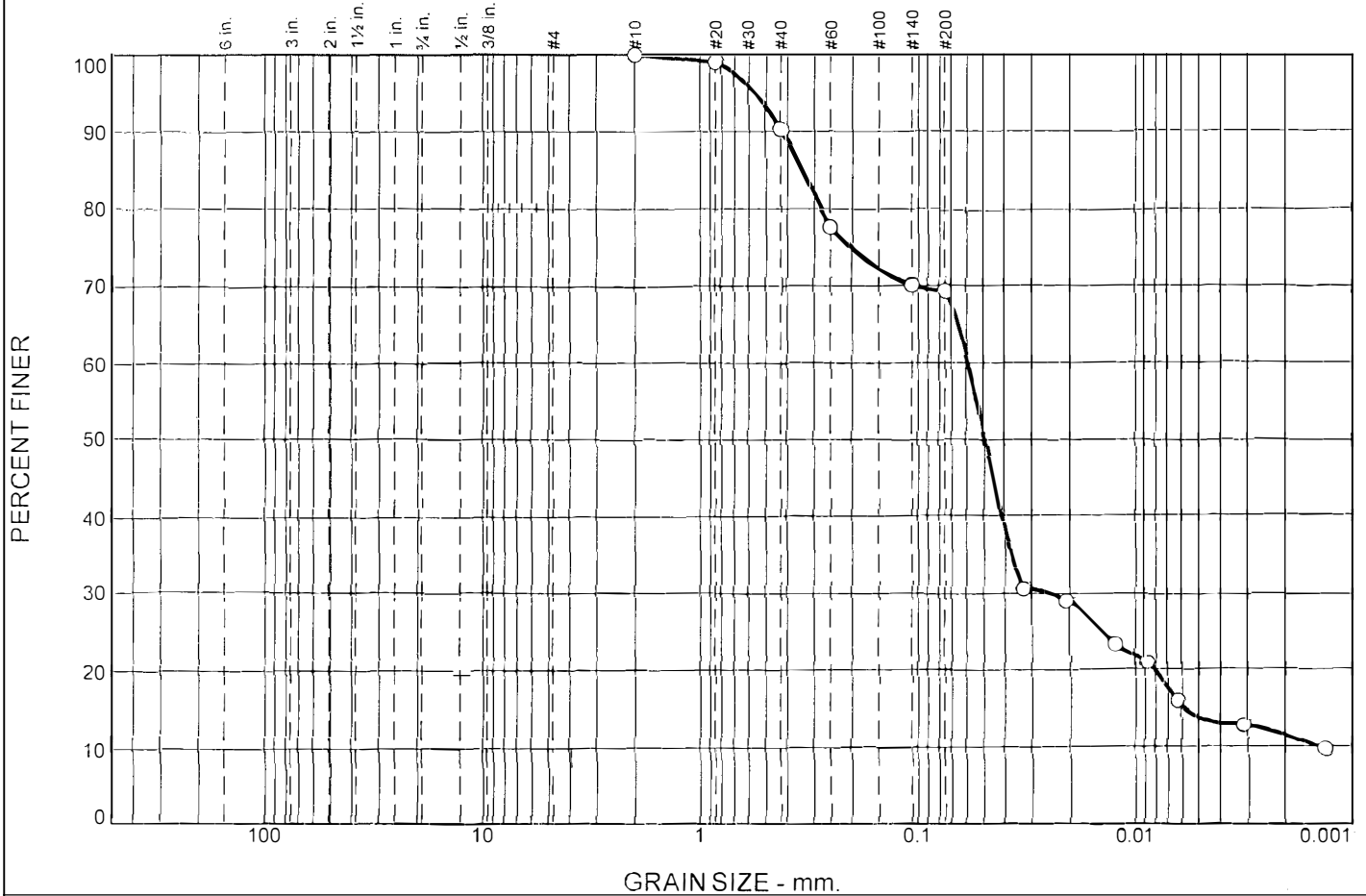
Sample Number: S-3

Depth: 2-4 ft

Date: 11/6/2020

<p style="font-size: 1.2em; margin: 0;">United Consulting</p> <p style="font-size: 1.2em; margin: 0;">Norcross, Georgia</p>	<p>Client: Gwinnett co dept of Water Resources</p> <p>Project: Beaver Ruin Wetlands Park</p> <p>Project No: GCDWR20GA0427301</p>
---	--

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	30.7	55.4	13.9

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	99.0		
#40	90.3		
#60	77.7		
#140	70.1		
#200	69.3		

Material Description

Clay-silty, some sand, dark tan

Atterberg Limits

PL= 20 LL= 26 PI= 6

Coefficients

D₉₀= 0.4182 D₈₅= 0.3383 D₆₀= 0.0588
 D₅₀= 0.0492 D₃₀= 0.0246 D₁₅= 0.0057
 D₁₀= 0.0014 C_u= 40.96 C_c= 7.19

Classification

USCS= CL-ML AASHTO= A-4(2)

Remarks

* (no specification provided)

Sample Number: S-4 Depth: 2-4 ft

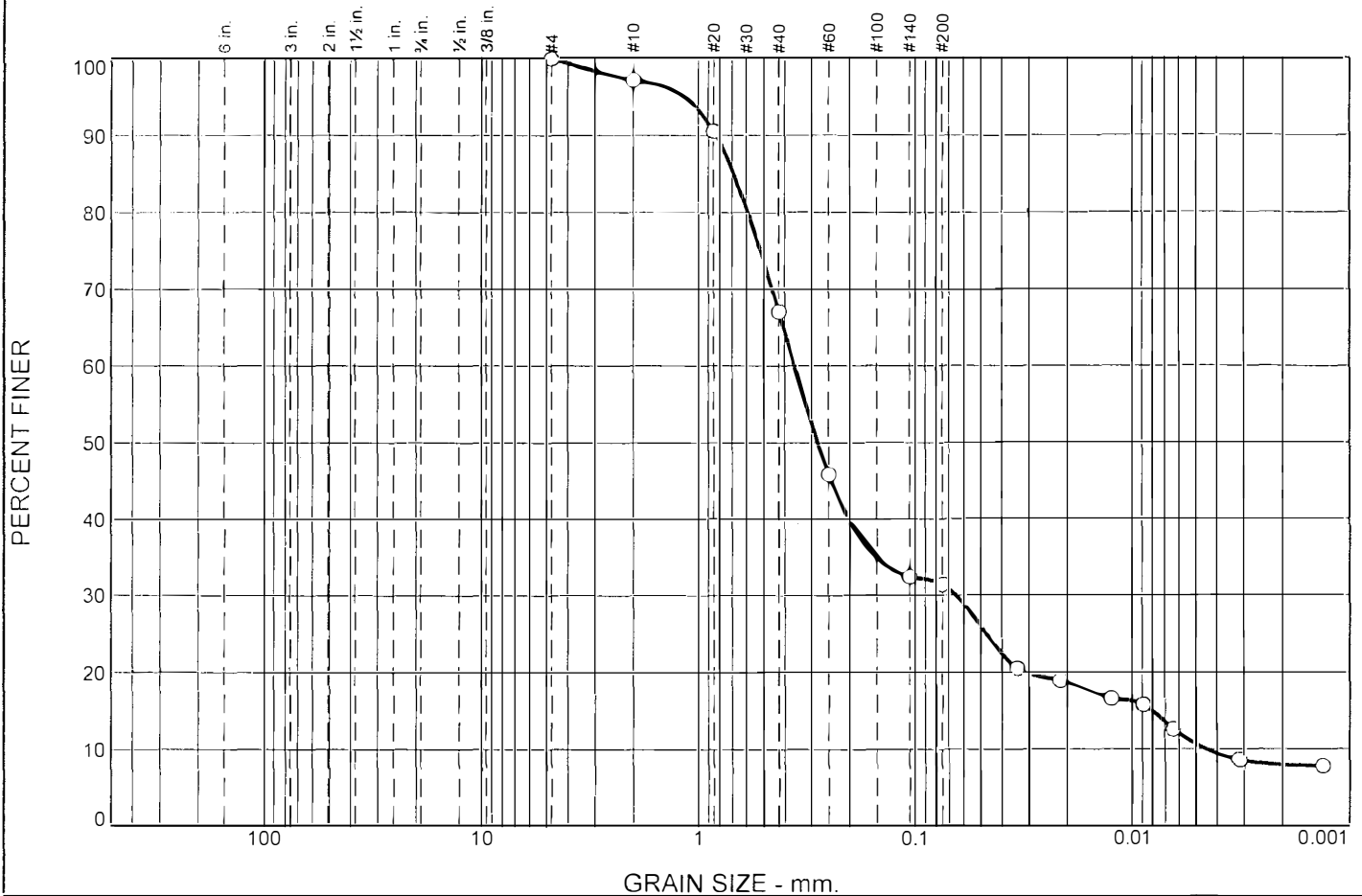
Date: 11/6/2020

United Consulting
Norcross, Georgia

Client: Gwinnett co dept of Water Resources
 Project: Beaver Ruin Wetlands Park
 Project No: GCDWR20GA0427301

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	68.6	20.8	10.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	97.2		
#20	90.6		
#40	67.1		
#60	45.9		
#140	32.4		
#200	31.4		

Material Description

Sand, some silt, trace clay, dark tan

Atterberg Limits

PL= 25 LL= 34 PI= 9

Coefficients

D₉₀= 0.8274 D₈₅= 0.6859 D₆₀= 0.3598
 D₅₀= 0.2812 D₃₀= 0.0651 D₁₅= 0.0081
 D₁₀= 0.0046 C_u= 79.00 C_c= 2.59

Classification

USCS= SM AASHTO= A-2-4(0)

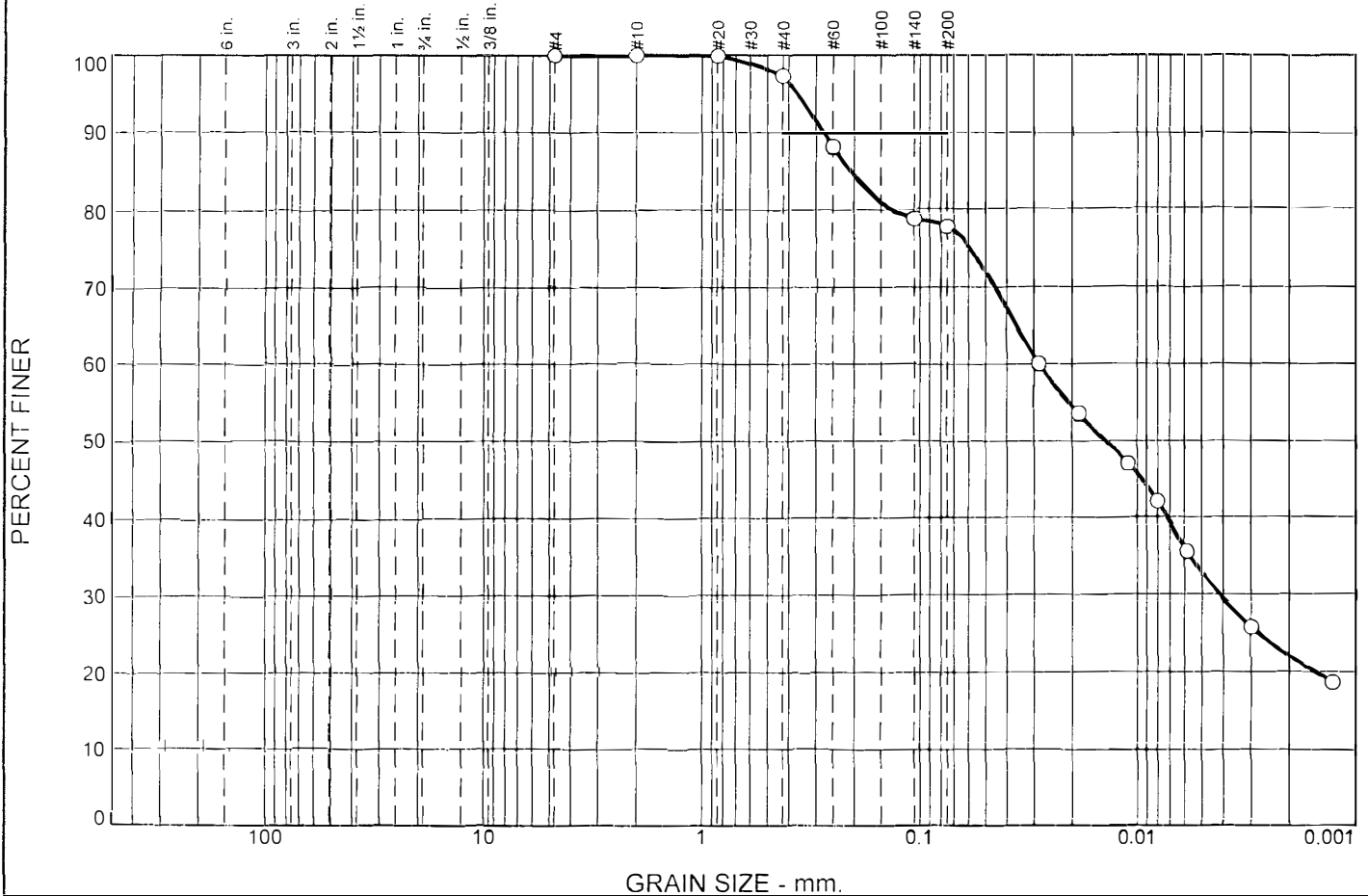
Remarks

* (no specification provided)

Sample Number: S-5 Depth: 2-4 ft

Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	22.2	45.0	32.8

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	100.0		
#20	99.9		
#40	97.3		
#60	88.1		
#140	78.8		
#200	77.8		

Material Description

Clay-silty, some sand, dark brown

Atterberg Limits

PL= 22 LL= 32 PI= 10

Coefficients

D₉₀= 0.2769 D₈₅= 0.2073 D₆₀= 0.0284
D₅₀= 0.0140 D₃₀= 0.0042 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= CL AASHTO= A-4(7)

Remarks

* (no specification provided)

Sample Number: S-6 Depth: 2-4 ft

Date: 11/6/2020

COMPACTION TEST REPORT

Project No.: GCDWR20GA0427301

Date: 11/10/2020

Project: Beaver Ruin Wetlands Park

Client: Gwinnett co dept of Water Resources

Sample Number: B-2(Bulk) Depth: 0-5 ft

Remarks:

MATERIAL DESCRIPTION

Description: Clay-silty, some sand, gray tan

Classifications -

USCS: CL

AASHTO: A-6(13)

Nat. Moist. = 25.2 %

Sp.G. =

Liquid Limit = 40

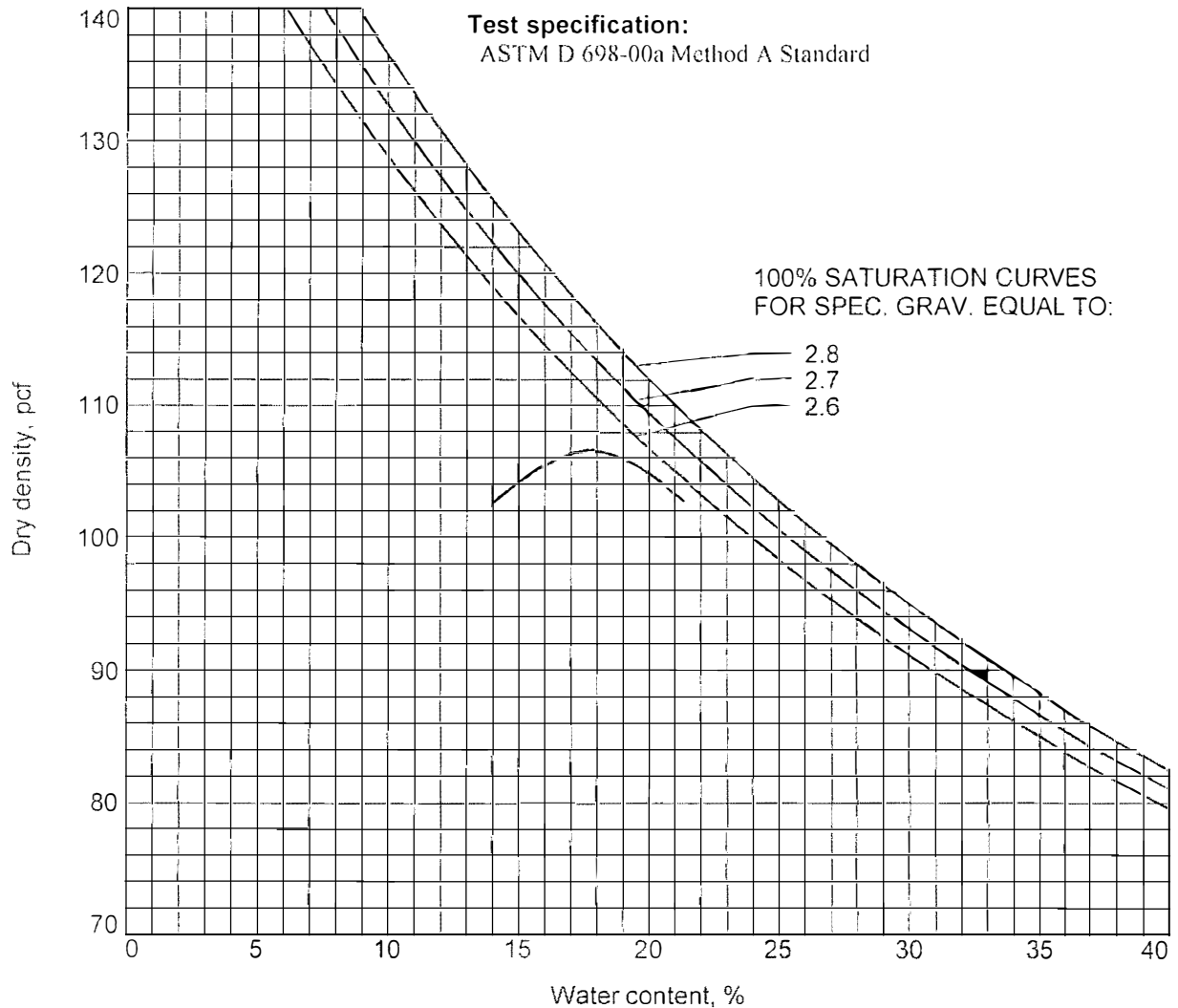
Plasticity Index = 18

% < No.200 = 77.1 %

TEST RESULTS

Maximum dry density = 106.6 pcf

Optimum moisture = 17.8 %



Figure

COMPACTION TEST REPORT

Project No.: GCDWR20GA042730 I
Project: Beaver Ruin Wetlands Park
Client: Gwinnett co dept of Water Resources
Sample Number: B-4(Bulk) **Depth:** 0-5.0'

Date: 11/10/20

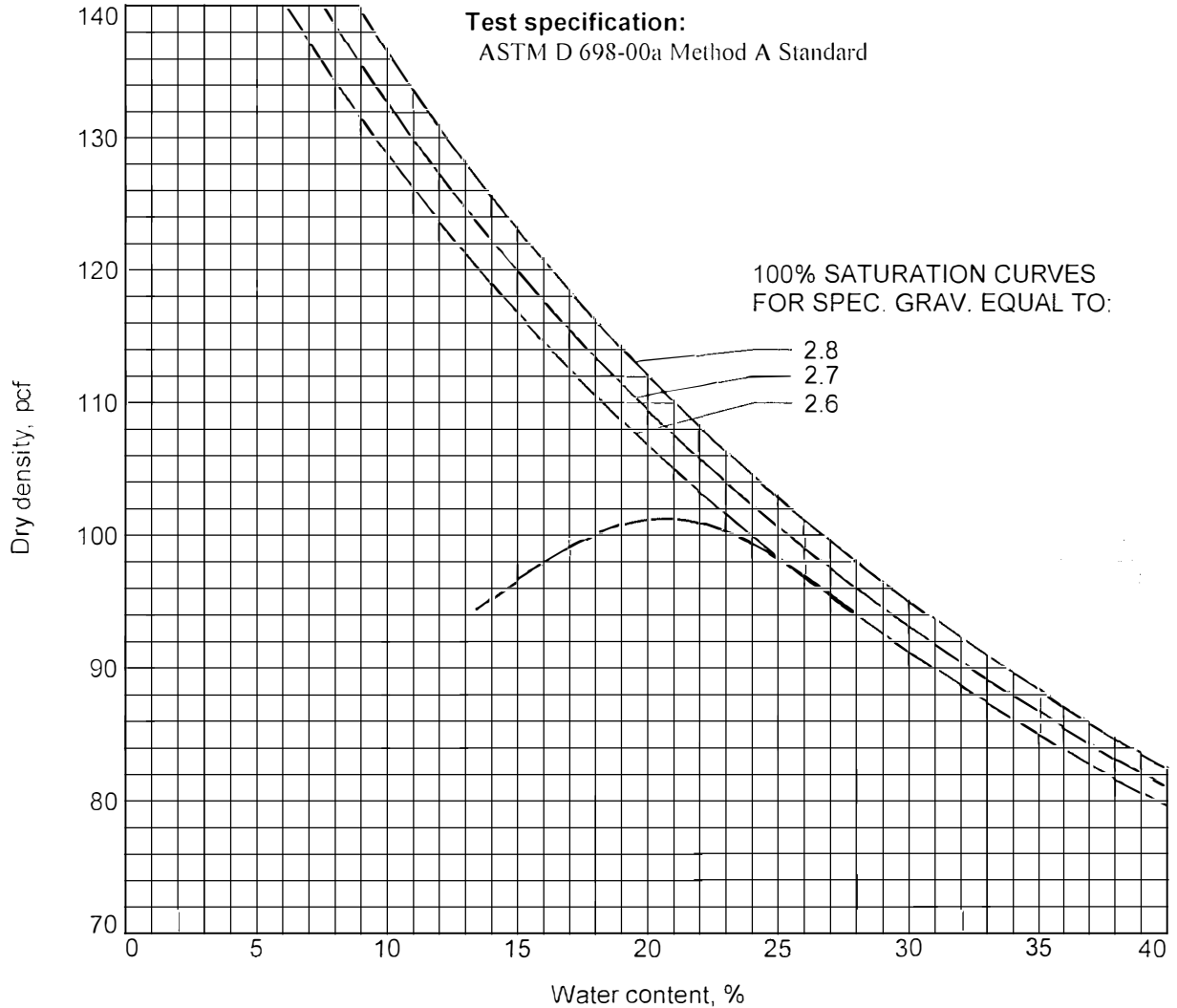
Remarks:

MATERIAL DESCRIPTION

Description: Sand, some silt and clay, orange brown

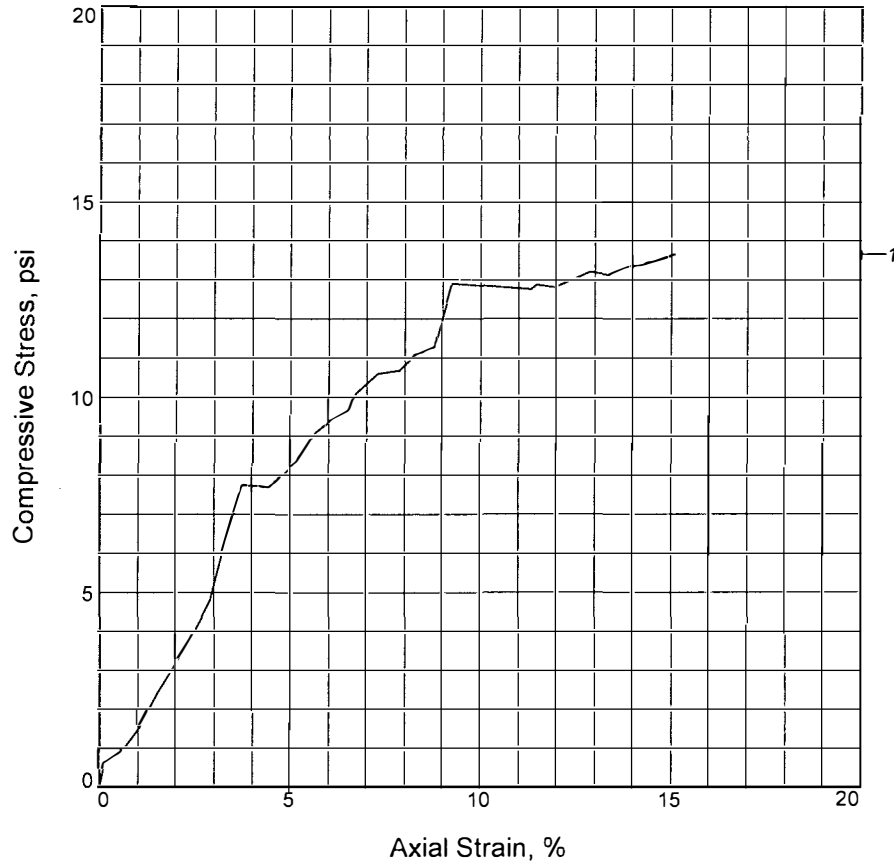
Classifications -	USCS: SM	AASHTO: A-7-5(5)
Nat. Moist. = 21.6 %		Sp.G. =
Liquid Limit = 52		Plasticity Index = 17
		% < No.200 = 45.6 %

TEST RESULTS
Maximum dry density = 101.3 pcf
Optimum moisture = 20.6 %



Figure

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	13.65			
Undrained shear strength, psi	6.83			
Failure strain, %	15.1			
Strain rate, in./min.	0.030			
Water content, %	20.1			
Wet density, pcf	131.0			
Dry density, pcf	109.0			
Saturation, %	99.6			
Void ratio	0.5459			
Specimen diameter, in.	2.87			
Specimen height, in.	5.60			
Height/diameter ratio	1.95			

Description: Clay-silty-sandy, gray and brown

LL = 38 **PL = 20** **PI = 18** **GS = 2.7** **Type: Undisturbed**

Project No.: GCDWR20GA0427301

Date Sampled: 11/6/2020

Remarks:

Client: Gwinnett co dept of Water Resources

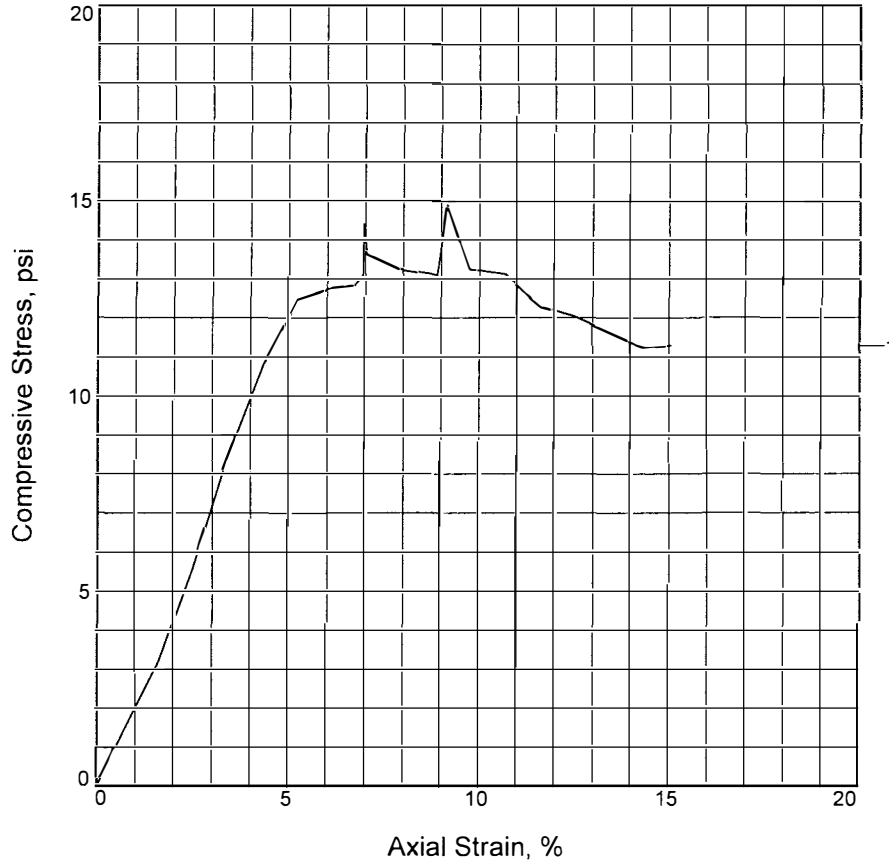
Project: Beaver Ruin Wetlands Park

Sample Number: B-3(Top) **Depth:** 4-4.5 ft

UNCONFINED COMPRESSION TEST
United Consulting
Norcross, Georgia

Figure _____

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	14.88			
Undrained shear strength, psi	7.44			
Failure strain, %	9.2			
Strain rate, in./min.	0.030			
Water content, %	18.0			
Wet density, pcf	133.8			
Dry density, pcf	113.4			
Saturation, %	99.9			
Void ratio	0.4869			
Specimen diameter, in.	2.87			
Specimen height, in.	5.60			
Height/diameter ratio	1.95			

Description: Sand, some silt and clay, gray

LL = 25 **PL = 16** **PI = 9** **GS = 2.7** **Type:** Undisturbed

Project No.: GCDWR20GA0427301

Date Sampled: 11/6/2020

Remarks:

Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

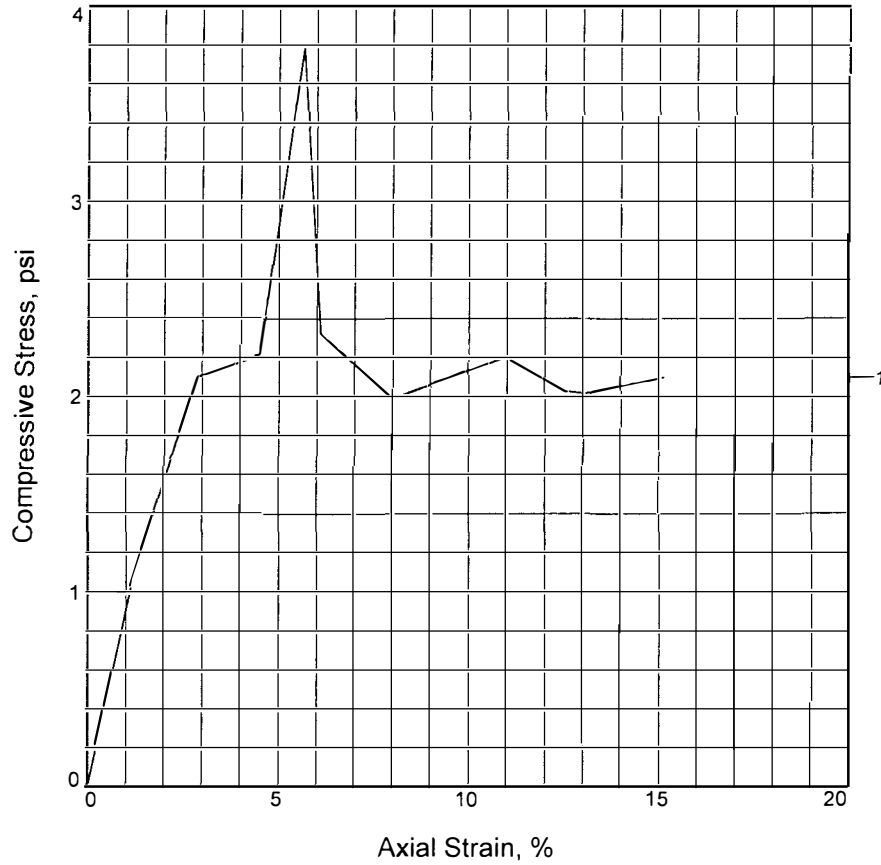
Sample Number: B-3(Middle) **Depth:** 4.5-5.5 ft

UNCONFINED COMPRESSION TEST

United Consulting
Norcross, Georgia

Figure _____

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	3.79			
Undrained shear strength, psi	1.90			
Failure strain, %	5.7			
Strain rate, in./min.	0.050			
Water content, %	21.5			
Wet density, pcf	123.8			
Dry density, pcf	101.9			
Saturation, %	88.7			
Void ratio	0.6535			
Specimen diameter, in.	2.87			
Specimen height, in.	5.00			
Height/diameter ratio	1.74			

Description: Sand, trace silt and clay, gray

LL = **PL =** **PI =** **GS= 2.7** **Type: Undisturbed**

Project No.: GCDWR20GA0427301

Date Sampled:

Remarks:

Client: Gwinnett co dept of Water Resources

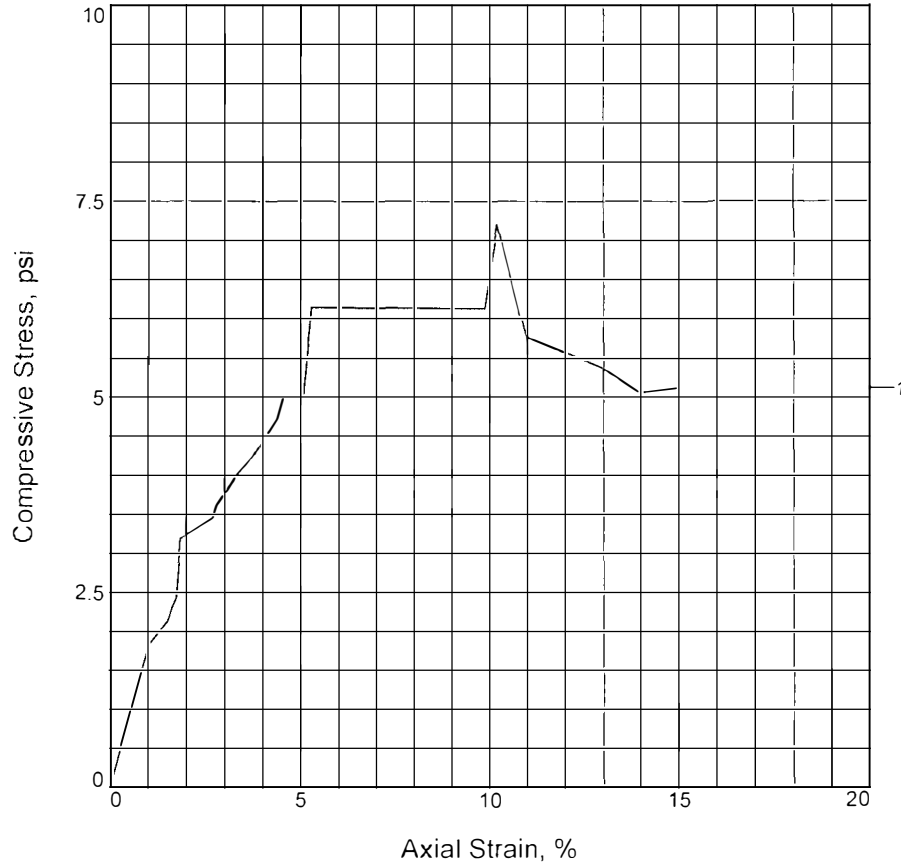
Project: Beaver Ruin Wetlands Park

Sample Number: B-3(Bottom) **Depth:** 5.5-6 ft

UNCONFINED COMPRESSION TEST
United Consulting
Norcross, Georgia

Figure _____

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	7.22			
Undrained shear strength, psi	3.61			
Failure strain, %	10.2			
Strain rate, in./min.	0.030			
Water content, %	24.6			
Wet density, pcf	126.2			
Dry density, pcf	101.3			
Saturation, %	100.0			
Void ratio	0.6641			
Specimen diameter, in.	2.87			
Specimen height, in.	5.00			
Height/diameter ratio	1.74			

Description: Sand, some clay and silt, red brown

LL = 57 PL = 32 PI = 25 GS = 2.7 **Type:** Undisturbed

Project No.: GCDWR20GGA0427301

Date Sampled: 11/12/2020

Remarks:

Client: Gwinnett co dept of Water Resources

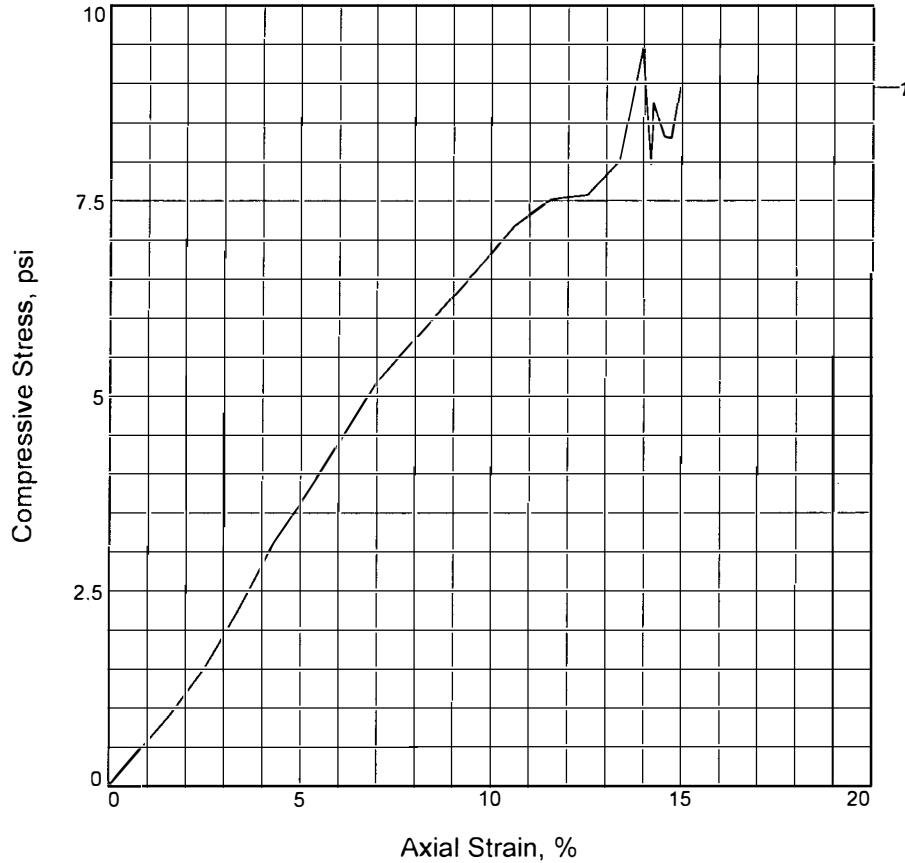
Project: Beaver Ruin Wetlands Park

Sample Number: B-6 (Top) **Depth:** 4-4.5 ft

Figure _____

UNCONFINED COMPRESSION TEST
United Consulting
Norcross, Georgia

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	9.44			
Undrained shear strength, psi	4.72			
Failure strain, %	13.9			
Strain rate, in./min.	0.030			
Water content, %	30.4			
Wet density, pcf	138.4			
Dry density, pcf	106.1			
Saturation, %	139.7			
Void ratio	0.5881			
Specimen diameter, in.	2.87			
Specimen height, in.	5.60			
Height/diameter ratio	1.95			

Description: Silt-sandy, some clay, brown

LL = 35 PL = 25 PI = 10 GS = 2.7 **Type:** Undisturbed

Project No.: GCDWR20GA0427301

Date Sampled: 11/6/2020

Remarks:
Bottom Sample consists of Organic Materials

Client: Gwinnett co dept of Water Resources

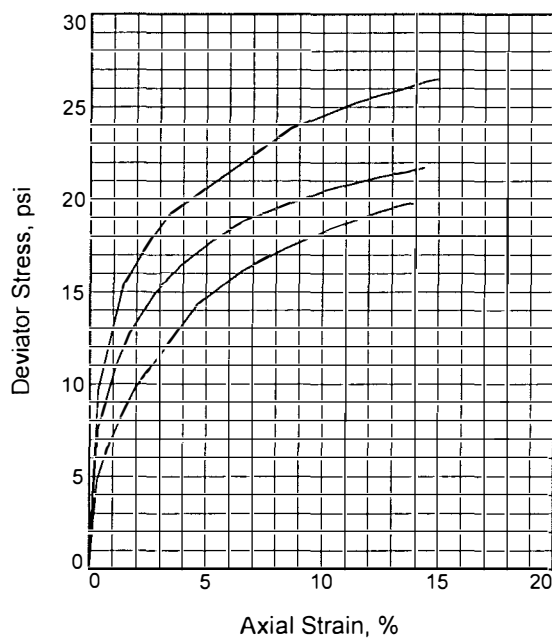
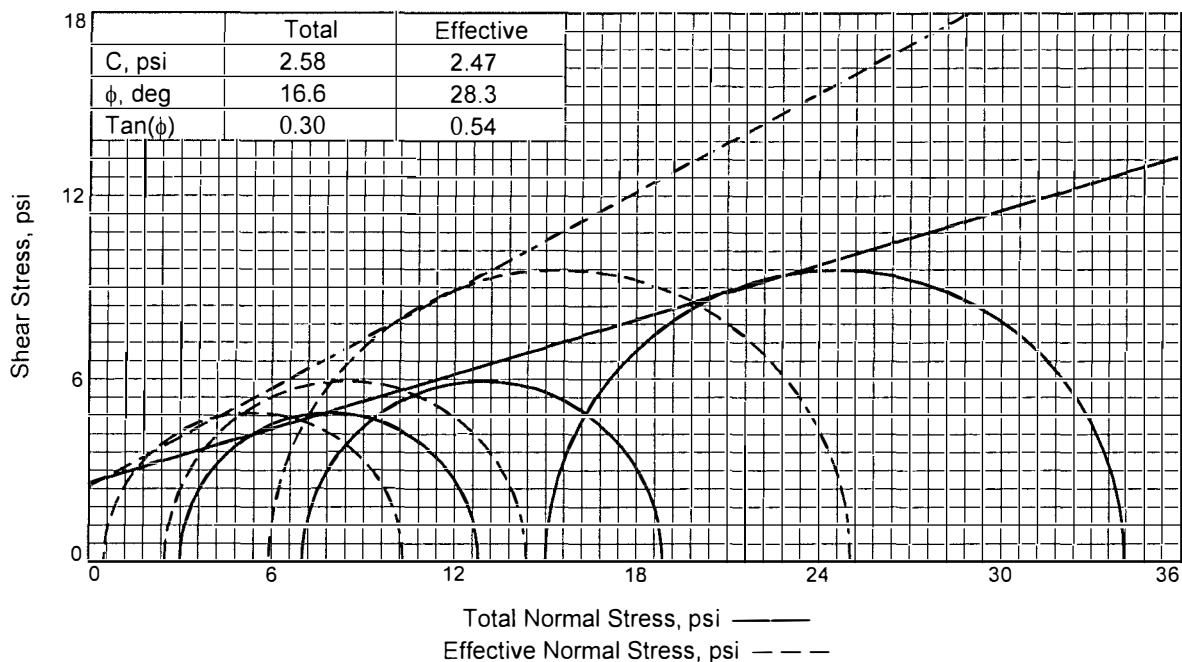
Project: Beaver Ruin Wetlands Park

Sample Number: B-6 (Bottom) **Depth:** 5-6 ft

UNCONFINED COMPRESSION TEST

United Consulting
Norcross, Georgia

Figure _____



Sample No.	1	2	3	
Initial	Water Content, %	23.9	23.9	23.9
	Dry Density, pcf	96.4	96.4	96.4
	Saturation, %	86.1	86.1	86.2
	Void Ratio	0.7493	0.7492	0.7483
	Diameter, in.	2.87	2.87	2.87
	Height, in.	6.00	6.00	6.00
At Test	Water Content, %	26.7	26.7	23.0
	Dry Density, pcf	97.9	97.9	104.0
	Saturation, %	100.0	100.0	100.0
	Void Ratio	0.7222	0.7222	0.6202
	Diameter, in.	2.86	2.86	2.80
	Height, in.	5.97	5.97	5.85
Strain rate, in./min.	0.008	0.008	0.008	
Back Pressure, psi	80.0	60.0	70.0	
Cell Pressure, psi	83.0	67.0	85.0	
Fail. Stress, psi	Total Pore Pr., psi	82.5	64.5	79.1
	Ult. Stress, psi	19.8	21.7	26.5
$\bar{\sigma}_1$ Failure, psi	Total Pore Pr., psi	77.5	59.8	76.2
	$\bar{\sigma}_3$ Failure, psi	10.3	14.4	25.1
$\bar{\sigma}_3$ Failure, psi		0.5	2.5	5.9

Type of Test:

CU with Pore Pressures

Sample Type: Remolded

Description: Sand, some silt and clay, orange brown

LL= 52 PL= 35 PI= 17

Specific Gravity= 2.7

Remarks:

Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Sample Number: B-4(Bulk) **Depth:** 0-5.0'

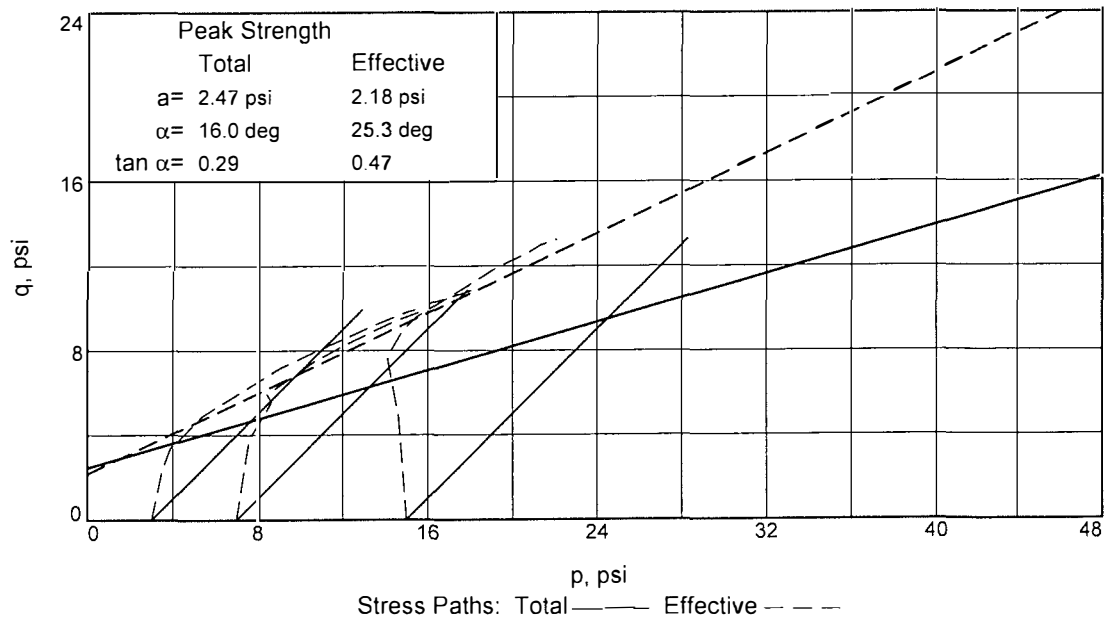
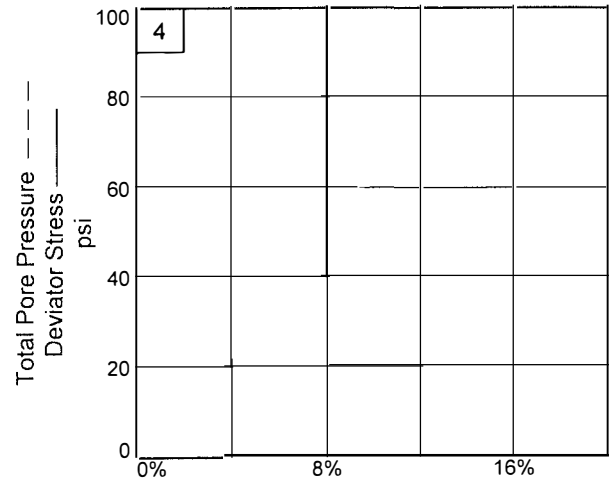
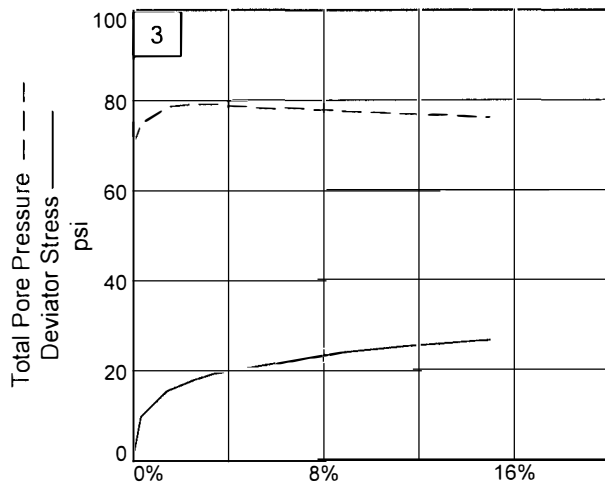
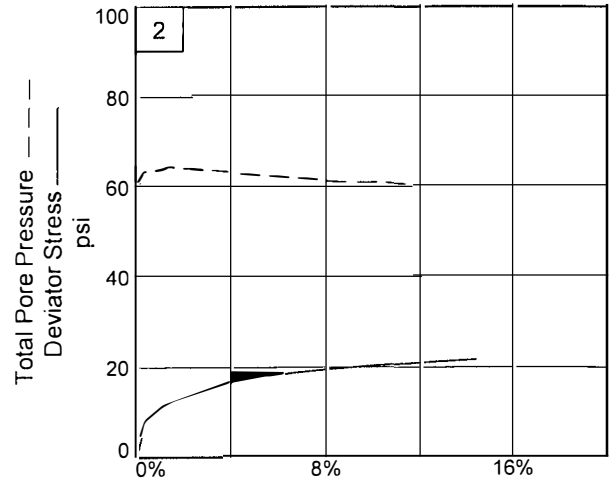
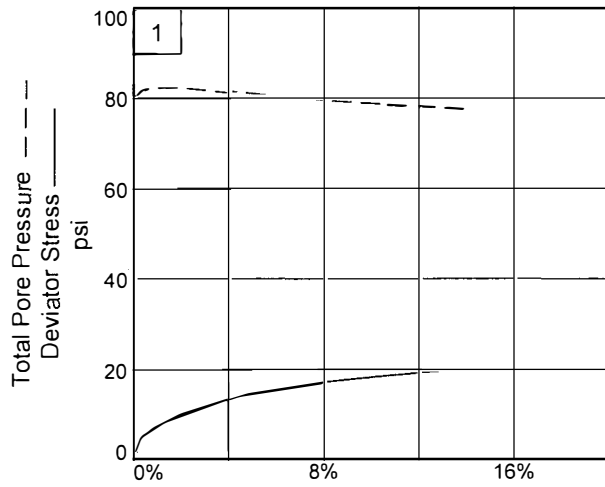
Proj. No.: GCDWR20GA0427301 **Date Sampled:** 11/6/2020

TRIAXIAL SHEAR TEST REPORT

United Consulting

Norcross, Georgia

Figure _____



Client: Gwinnett co dept of Water Resources

Project: Beaver Ruin Wetlands Park

Depth: 0-5.0' **Sample Number:** B-4(Bulk)

Project No.: GCDWR20GA0427301

Figure _____

United Consulting



ANALYTICAL ENVIRONMENTAL SERVICES, INC.

December 01, 2020

Mahvand Saleki
United Consulting Group Inc.

625 Holcomb Bridge Rd
Norcross GA 30071

RE: Beaver Ruin Wetland Park

Dear Mahvand Saleki:

Order No: 2011M90

Analytical Environmental Services, Inc. received 6 samples on 11/19/2020 2:35:00 PM for the analyses presented in following report.

“No problems were encountered during the analyses except as noted in the Case Narrative or by qualifiers in the report or QC Summary. Additionally, all results for the associated Quality Control samples were within EPA and/or AES established limits.

AES’s accreditations are as follows:

-NELAP/State of Florida Laboratory ID E87582 for analysis of Non-Potable Water, Solid & Chemical Materials, Air & Emissions Volatile Organics, and Drinking Water Microbiology & Metals, effective 07/01/20-06/30/21.

State of Georgia, Department of Natural Resources ID #800 for analysis of Drinking Water Metals, effective through 06/30/21 and Total Coliforms/ E. coli, effective 04/20/20-04/24/23.

-AIHA-LAP, LLC Laboratory ID: 100671 for Industrial Hygiene samples (Metals and PCM Asbestos), Environmental Lead (Paint, Soil, Dust Wipes, Air), and Environmental Microbiology (Fungal) Direct Examination, effective until 11/01/21.

These results relate only to the items tested as received. This report may only be reproduced in full.

If you have any questions regarding these test results, please feel free to call.

Sincerely,

Ioana Pacurar
Project Manager

SAMPLE CHAIN-OF-CUSTODY RECORD

2011M90

UNITED CONSULTING
625 Holcomb Bridge
NORCROSS, GEORGIA 30071
(770) 209-0029 FAX (770) 582-2895
www.uniteconsulting.com

PROJECT NAME: Beaver Ruin Wetland Park					Project#: GCDWR20GA0427301		ANALYSES (indicate target list)																
TAT or DUE DATE: 11/30/2020		CONTACT: Mahvand Saleki msaleki@unitedconsulting.com		PROJECT MANAGER: Rafael Ospina			pH	Resistivity	Sulphate	Chloride													
PHONE#: (770)582-2843		RECEIVING LAB: AES			PO#:																		
SAMPLE NUMBER	SAMPLE DESCRIPTION	Date Shipped	Sample Matrix	Preservative	# / Size of Cont.																		
B-1@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
B-2@2-4'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
B-3@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
B-4@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
B-5@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
B-6@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X														
SAMPLES RELINQUISHED BY:		DATE/TIME	SAMPLES ACCEPTED BY:			DATE/TIME	COMMENTS:																
PHUC VO		11-19-20	[Signature]			11/19/20																	
		2:34				2:35																	

Client: United Consulting Group Inc.
Project: Beaver Ruin Wetland Park
Lab ID: 2011M90

Case Narrative

pH Analysis by Method SW9045D:

Samples for pH analysis by Method SW9045D were received and analyzed outside holding time requirement of "immediate or 15 minutes."

Client: United Consulting Group Inc.	Client Sample ID: B-1@2-3.5'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-001	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A					(SW9050)			
Resistivity (@100% Moisture Saturation)	7460	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D					(SW9045D)			
pH	5.88	0.01	H	pH Units	306391	1	11/23/2020 13:28	CB
ION SCAN SW9056A					(SW9056A)			
Chloride	44	13		mg/Kg-dry	306486	1	11/30/2020 15:23	IP
Sulfate	53	13		mg/Kg-dry	306486	1	11/30/2020 15:23	IP
PERCENT MOISTURE D2216								
Percent Moisture	20.7	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-2@2-4'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-002	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	4850	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	5.74	0.01	H	pH Units	306391	1	11/23/2020 13:41	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	49	12		mg/Kg-dry	306486	1	11/30/2020 15:39	IP
Sulfate	34	12		mg/Kg-dry	306486	1	11/30/2020 15:39	IP
PERCENT MOISTURE D2216								
Percent Moisture	18.8	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-3@2-3.5'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-003	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	9030	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	5.44	0.01	H	pH Units	306391	1	11/23/2020 13:43	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	43	12		mg/Kg-dry	306486	1	11/30/2020 15:55	IP
Sulfate	40	12		mg/Kg-dry	306486	1	11/30/2020 15:55	IP
PERCENT MOISTURE D2216								
Percent Moisture	16.2	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-4@2-3.5'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-004	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	18400	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	5.74	0.01	H	pH Units	306391	1	11/23/2020 13:46	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	42	12		mg/Kg-dry	306486	1	11/30/2020 14:35	IP
Sulfate	16	12		mg/Kg-dry	306486	1	11/30/2020 14:35	IP
PERCENT MOISTURE D2216								
Percent Moisture	18.5	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-5@2-3.5'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-005	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	13300	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	6.05	0.01	H	pH Units	306391	1	11/23/2020 13:49	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	40	11		mg/Kg-dry	306486	1	11/30/2020 14:51	IP
Sulfate	30	11		mg/Kg-dry	306486	1	11/30/2020 14:51	IP
PERCENT MOISTURE D2216								
Percent Moisture	13.2	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-6@2-3.5'
Project Name: Beaver Ruin Wetland Park	Collection Date: 11/19/2020
Lab ID: 2011M90-006	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A		(SW9050)						
Resistivity (@100% Moisture Saturation)	13900	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D		(SW9045D)						
pH	5.19	0.01	H	pH Units	306391	1	11/23/2020 13:51	CB
ION SCAN SW9056A		(SW9056A)						
Chloride	45	13		mg/Kg-dry	306486	1	11/30/2020 15:07	IP
Sulfate	BRL	13		mg/Kg-dry	306486	1	11/30/2020 15:07	IP
PERCENT MOISTURE D2216								
Percent Moisture	22.6	0		wt%	R440362	1	11/22/2020 00:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

SAMPLE/COOLER RECEIPT CHECKLIST

1. Client Name: United Consulting Group Inc.

AES Work Order Number: 2011M90

2. Carrier: FedEx UPS USPS Client Courier Other _____

	Yes	No	N/A	Details	Comments
3. Shipping container/cooler received in good condition?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	damaged <input type="checkbox"/> leaking <input type="checkbox"/> other <input type="checkbox"/>	
4. Custody seals present on shipping container?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
5. Custody seals intact on shipping container?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
6. Temperature blanks present?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
7. Cooler temperature(s) within limits of 0-6°C? [See item 13 and 14 for temperature recordings.]	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	Cooling initiated for recently collected samples / ice present <input type="checkbox"/>	
8. Chain of Custody (COC) present?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
9. Chain of Custody signed, dated, and timed when relinquished and received?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
10. Sampler name and/or signature on COC?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
11. Were all samples received within holding time?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
12. TAT marked on the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	If no TAT indicated, proceeded with standard TAT per Terms & Conditions. <input type="checkbox"/>	

13. Cooler 1 Temperature 0.1 °C Cooler 2 Temperature _____ °C Cooler 3 Temperature _____ °C Cooler 4 Temperature _____ °C
 14. Cooler 5 Temperature _____ °C Cooler 6 Temperature _____ °C Cooler 7 Temperature _____ °C Cooler 8 Temperature _____ °C

15. Comments: _____

I certify that I have completed sections 1-15 (dated initials). BH 11/20/20

	Yes	No	N/A	Details	Comments
16. Were sample containers intact upon receipt?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
17. Custody seals present on sample containers?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
18. Custody seals intact on sample containers?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
19. Do sample container labels match the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	incomplete info <input type="checkbox"/> illegible <input type="checkbox"/> no label <input type="checkbox"/> other <input type="checkbox"/>	
20. Are analyses requested indicated on the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
21. Were all of the samples listed on the COC received?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	samples received but not listed on COC <input type="checkbox"/> samples listed on COC not received <input type="checkbox"/>	
22. Was the sample collection date/time noted?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
23. Did we receive sufficient sample volume for indicated analyses?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
24. Were samples received in appropriate containers?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
25. Were VOA samples received without headspace (< 1/4" bubble)?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
26. Were trip blanks submitted?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>	listed on COC <input type="checkbox"/> not listed on COC <input type="checkbox"/>	

27. Comments: _____

I certify that I have completed sections 16-27 (dated initials). BH 11/20/20

This section only applies to samples where pH can be checked at Sample Receipt.

	Yes	No	N/A	Details	Comments
28. Have containers needing chemical preservation been checked? *	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
29. Containers meet preservation guidelines?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
30. Was pH adjusted at Sample Receipt?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		

* Note: Certain analyses require chemical preservation but must be checked in the laboratory and not upon Sample Receipt such as Coliforms, VOCs and Oil & Grease/TPH.

This also excludes metals by EPA 200.7, 200.8 and 245.1 which will be verified between 16 and 24 hours after preservation.

I certify that I have completed sections 28-30 (dated initials). BH 11/20/20

Locked

Client: United Consulting Group Inc.
 Project Name: Beaver Ruin Wetland Park
 Lab Order: 2011M90

Dates Report

Lab Sample ID	Client Sample ID	Collection Date	Matrix	Test Name	TCLP Date	Prep Date	Analysis Date
2011M90-001A	B-1@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-001A	B-1@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-001A	B-1@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-001A	B-1@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M90-002A	B-2@2-4'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-002A	B-2@2-4'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-002A	B-2@2-4'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-002A	B-2@2-4'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M90-003A	B-3@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-003A	B-3@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-003A	B-3@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-003A	B-3@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M90-004A	B-4@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-004A	B-4@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-004A	B-4@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-004A	B-4@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M90-005A	B-5@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-005A	B-5@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-005A	B-5@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-005A	B-5@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M90-006A	B-6@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M90-006A	B-6@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M90-006A	B-6@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M90-006A	B-6@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Wetland Park
Workorder: 2011M90

ANALYTICAL QC SUMMARY REPORT

BatchID: 306391

Sample ID: LCS-306391	Client ID:	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: LCS	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027582							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 6.990 0.01 7.000 99.9 90 110

Sample ID: 2011M90-001ADUP	Client ID: B-1@2-3.5'	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: DUP	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027609							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 5.800 0.01 5.880 1.37 10 H

Sample ID: 2011M91-002ADUP	Client ID:	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: DUP	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027610							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 5.850 0.01 5.940 1.53 10 H

Qualifiers:	> Greater than Result value	< Less than Result value	B Analyte detected in the associated method blank
	BRL Below reporting limit	E Estimated (value above quantitation range)	H Holding times for preparation or analysis exceeded
	J Estimated value detected below Reporting Limit	N Analyte not NELAC certified	R RPD outside limits due to matrix
	Rpt Lim Reporting Limit	S Spike Recovery outside limits due to matrix	

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Wetland Park
Workorder: 2011M90

ANALYTICAL QC SUMMARY REPORT

BatchID: 306477

Sample ID: LCS-306477	Client ID:	Units: ohms*cm	Prep Date: 11/23/2020	Run No: 440558							
SampleType: LCS	TestCode: Soil Resistivity SW9050A	BatchID: 306477	Analysis Date: 11/24/2020	Seq No: 10030885							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Resistivity (@100% Moisture Saturatic 9891 0 10000 98.9 90 110

Sample ID: 2011M90-001ADUP	Client ID: B-1@2-3.5'	Units: ohms*cm	Prep Date: 11/23/2020	Run No: 440558							
SampleType: DUP	TestCode: Soil Resistivity SW9050A	BatchID: 306477	Analysis Date: 11/24/2020	Seq No: 10030887							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Resistivity (@100% Moisture Saturatic 7457 0 7463 0.075 30

Sample ID: 2011M91-002ADUP	Client ID:	Units: ohms*cm	Prep Date: 11/23/2020	Run No: 440558							
SampleType: DUP	TestCode: Soil Resistivity SW9050A	BatchID: 306477	Analysis Date: 11/24/2020	Seq No: 10030901							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Resistivity (@100% Moisture Saturatic 9416 0 9425 0.094 30

Qualifiers:	> Greater than Result value	< Less than Result value	B Analyte detected in the associated method blank
	BRL Below reporting limit	E Estimated (value above quantitation range)	H Holding times for preparation or analysis exceeded
	J Estimated value detected below Reporting Limit	N Analyte not NELAC certified	R RPD outside limits due to matrix
	Rpt Lim Reporting Limit	S Spike Recovery outside limits due to matrix	

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Wetland Park
Workorder: 2011M90

ANALYTICAL QC SUMMARY REPORT

BatchID: 306486

Sample ID: MB-306486	Client ID:	Units: mg/Kg	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MBLK	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036056							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride BRL 10
 Sulfate BRL 10

Sample ID: LCS-306486	Client ID:	Units: mg/Kg	Prep Date: 11/24/2020	Run No: 440738							
SampleType: LCS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036057							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride 108.4 10 100.0 108 90 110
 Sulfate 272.0 10 250.0 109 90 110

Sample ID: 2011M92-003AMS	Client ID:	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036061							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride 172.7 11 114.1 44.88 112 80 120
 Sulfate 302.7 11 285.2 133.2 59.4 80 120 S

Sample ID: 2011M92-008AMS	Client ID:	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/28/2020	Seq No: 10042731							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride 155.9 12 115.7 45.12 95.8 80 120
 Sulfate 268.3 12 289.3 36.80 80.0 80 120

Sample ID: 2011M92-003AMSD	Client ID:	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MSD	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036062							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride 170.8 12 115.9 44.88 109 80 120 172.7 1.12 20

Qualifiers: > Greater than Result value < Less than Result value B Analyte detected in the associated method blank
 BRL Below reporting limit E Estimated (value above quantitation range) H Holding times for preparation or analysis exceeded
 J Estimated value detected below Reporting Limit N Analyte not NELAC certified R RPD outside limits due to matrix
 Rpt Lim Reporting Limit S Spike Recovery outside limits due to matrix

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Wetland Park
Workorder: 2011M90

ANALYTICAL QC SUMMARY REPORT

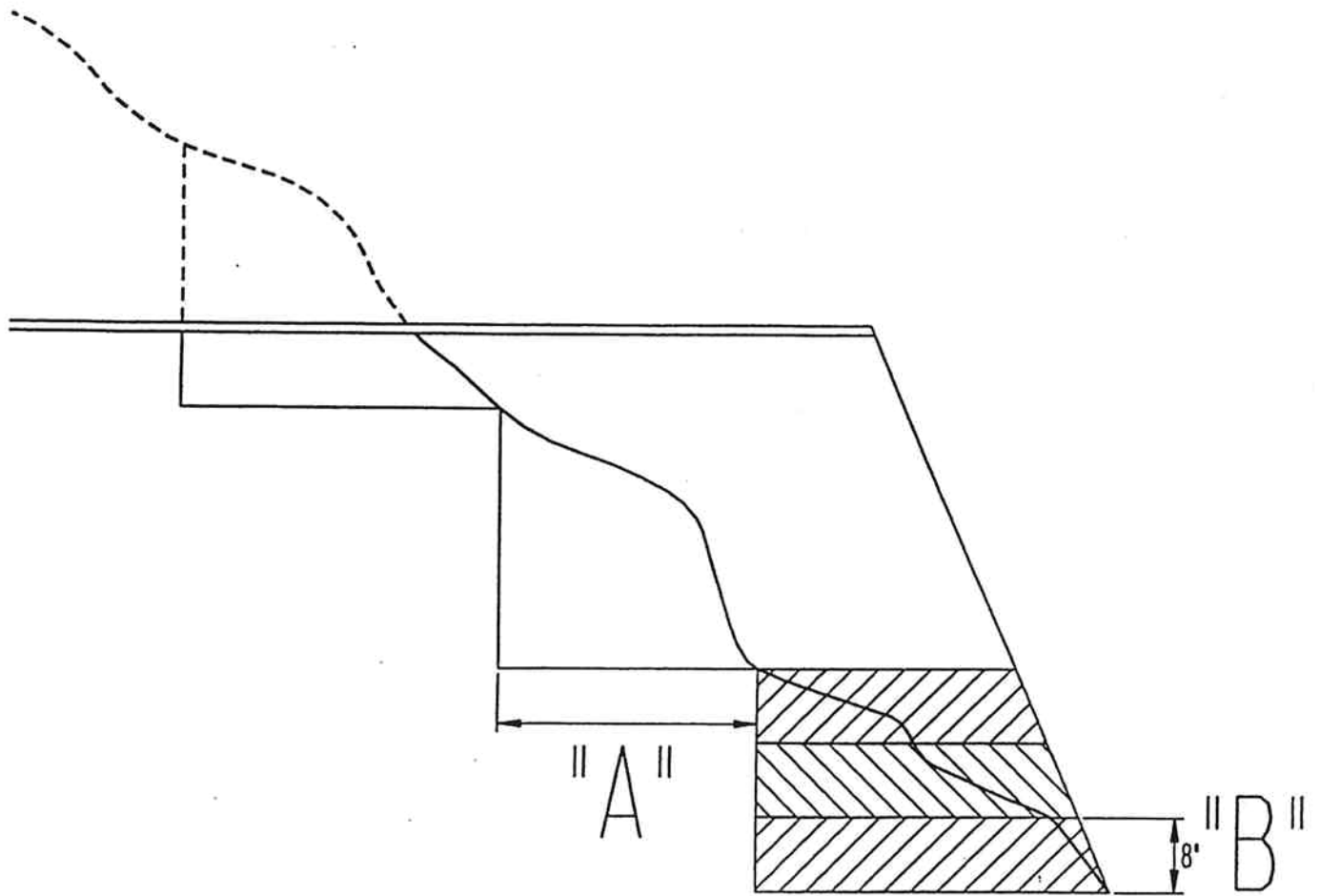
BatchID: 306486

Sample ID: 2011M92-003AMSD	Client ID:	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738
SampleType: MSD	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036062

Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual
Sulfate	307.6	12	289.7	133.2	60.2	80	120	302.7	1.61	20	S

Qualifiers:	>	Greater than Result value	<	Less than Result value	B	Analyte detected in the associated method blank
	BRL	Below reporting limit	E	Estimated (value above quantitation range)	H	Holding times for preparation or analysis exceeded
	J	Estimated value detected below Reporting Limit	N	Analyte not NELAC certified	R	RPD outside limits due to matrix
	Rpt Lim	Reporting Limit	S	Spike Recovery outside limits due to matrix		

End of Report



1. THE ABOVE DIAGRAM ILLUSTRATES A TYPICAL BENCHING FOR PLACEMENT OF FILL ON A SLOPING SURFACE.
2. THE DIAGRAM SHOWS THAT BEFORE FILL IS PLACED, THE FIRST STEP IS CUT INTO THE SLOPE A MAXIMUM DISTANCE OF ABOUT 8 FEET 'A' (ABOUT $\frac{3}{4}$ THE WIDTH OF USUAL D-8 BULLDOZER BLADE). SUCCESSIVE LAYERS OF FILL ARE THEN PLACED. BEFORE FINAL LAYER IS PLACED, THE SECOND STEP IS CUT 8 FEET INTO THE SLOPE AND SUCCESSIVE LAYERS ARE AGAIN PLACED.
3. SELECT FILL MATERIAL SHOULD BE PLACED IN 8 INCH LIFTS AND COMPACTED TO THE SPECIFIED DENSITY ('B').

TYPICAL BENCHING DETAIL



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD, NORCROSS, GEORGIA 30071
 OFFICE (770)-209-0029 FAX (770)-582-2900

Important Information about This

Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply this report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light-industrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by:* the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmation-dependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.*

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help

others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical-engineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold-prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical-engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; *none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.*

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your GBC-Member geotechnical engineer for more information.



8811 Colesville Road/Suite G106, Silver Spring, MD 20910

Telephone: 301/565-2733 Facsimile: 301/589-2017

e-mail: info@geoprofessional.org www.geoprofessional.org

Copyright 2015 by Geoprofessional Business Association (GBA). Duplication, reproduction, or copying of this document, or its contents, in whole or in part, by any means whatsoever, is strictly prohibited, except with GBA's specific written permission. Excerpting, quoting, or otherwise extracting wording from this document is permitted only with the express written permission of GBA, and only for purposes of scholarly research or book review. Only members of GBA may use this document as a complement to or as an element of a geotechnical-engineering report. Any other firm, individual, or other entity that so uses this document without being a GBA member could be committing negligent or intentional (fraudulent) misrepresentation.



UNITED
CONSULTING

REPORT

**For Gwinnett County
Government – Parks &
Recreation**

Geotechnical Exploration
Beaver Ruin Wetlands Park
Duluth, Gwinnett County, Georgia

Project No.: GCP&R-20-GA-04517-01
January 7, 2021





January 7, 2021

Rafael I. Ospina, P.E.
United Consulting
4400 Peachtree Dunwoody Road, Suite 100
Atlanta, Georgia 30340
Phone: 770-209-0029

Re: [Rafael I. Ospina, P.E.](#)

Report of Geotechnical Investigation
Beaver Ruin Wetlands Park
Fulton County, Georgia
Project No. -20-0417-01

Dear Sir,

Reference is made to your letter of January 7, 2021, regarding the above-mentioned project. The work was completed in general accordance with the proposal of 2020-04-17-01 dated 07/14/20 and has been issued on 7/21/20.

We appreciate the opportunity to assist you with this project and look forward to continue participation should you have any questions or if we can be of assistance.

Sincerely,

UNITED CONSULTING

Rafael I. Ospina, P.E.



Consulting Geotechnical Engineer

Chris L. Roberds, P.G.

Senior Geotechnical Engineer

Thank you,

unc-sps/10824/GCP&R-20-GA-04517-01/Geotechnical Documents/GCP&R-20-GA-04517-01 - Geo.docx



TABLE OF CONTENTS

10	T												
20	T	T											
0													
40													
0	B			T		10							
0	L	B	T	T	T	12							
70					T	1							
71	isting	ill				1							
72	ite	epa	ation			1							
7	iffi	lt	a	ation		14							
74	o	n	ate	onsi	e	ations	14						
7	a	ing	onsi	e	ations	1							
7	o	n	ation	esign	an	onst	tion	1					
7	1	i	st	teel	T	ss	e	est	ian	B	i	ge	1
7	11	hallo	o	n	ation	e	o	e	n	ations	1		
7	12	ee	p	o	n	ation	e	o	e	n	ations	1	
7	2	e	on	teel	T	ss	e	est	ian	B	i	ge	1
7	21	hallo	o	n	ation	e	o	e	n	ations	1		
7	22	ee	p	o	n	ation	e	o	e	n	ations	1	
7	o	n	ete	T	ails	Boa	alks					17	
7	1	eli	al	ie	e	o	e	n	ations			1	
7	4	Lightly	Loa	e	t	t	e	s				1	
77	o	n	loo	labs								20	
7	a	th	o	k								20	
7	l	opes										21	
710	ill	la	e	ent								21	
711	et	aining	alls									22	
0	L	T	T									24	

TABLES

- Table 1 □ Boa alk ie ea tion Loa s
- Table 2 □ B i ge- onto T ss ea tion Loa s
- Table □ a y of bs fa e on itions
- Table 4 □ oil o osi ity Test es lts
- Table □ a y of eli ina y T ss B i ge o n ation e o en ations
- Table □ a y of eli ina y eli al ie esign e o en ations
- Table 7 □ llo able Bea ing ess e fo Lightly Loa e t t es
- Table □ Late al a th ess es



APPENDIX

General Notes a table of Milling Operations
Figure 1 □ Boiling Location Plan
Location of Sites
Laboratory of Sites
T Boiling Logs 1
Electrical Design Specifications 1
Laboratory Sheet
Lithian Last Test Report 2
Moisture Content Tests 2
Main Distribution Tests 1
In-Office Compression Test Report 2
Thermal Tests Tests 2
Analytical Lab Tests Tests 1
Benchmarking



1.0 EXECUTIVE SUMMARY

United Consulting has completed a geotechnical exploration for the Beaumont Interlands Park to be located to the south of Atlanta Boulevard in Lithia Springs County Georgia. Please refer to the text of the report for a more detailed discussion of the site's characteristics below.

The geotechnical exploration program included fifteen (15) Trial Borings, one (1) offset boring and laboratory testing.

1. Below the ground surface boring B-11 encountered approximately 2 feet of fill soils borings B-101 and B-11 encountered between 4 to 6 feet of fill soils and borings B-102 and B-10 encountered 2 feet of fill soils. The fill encountered generally consists of very loose to fine sand with varying amounts of silt. Layering is generally apparent to be free of debris and organic content and has a natural settlement Test resistance - all of 2 blows per foot bpf to 11 to bpf.

2. Partially weathered rock was encountered in borings B-101 through B-10, B-10, B-10, B-10 and B-114 at depths ranging from 1 foot to 2 feet. Generally, the rock in borings B-101 through B-110 and B-114 at depths ranging from 1 foot to 2 feet exhibits a reaction on impact with a blasting associate with rock and not generally expected for a strong material of the site. Note that shallow rock may be present between a depth of the average plane.

3. Groundwater was encountered in borings B-101, B-10, B-104, B-10, B-10, B-10 and B-111 through B-114 at depths ranging from 1 foot to 1 foot at the time of drilling. 24 hours after drilling, groundwater will be expected for this project for construction of special foundations or a foundation below ground. The amount should be prepared to be expected to be expected to be expected as needed. Groundwater levels should be anticipated to fluctuate with the change of seasons during periods of very low precipitation or to changes in the flood plain or water table for the area.

4. Note that the site is prepared as expected. It is our opinion that the proposed foundations can be supported on helical pier footings. The proposed tallest structures can be supported on shallow foundations. Helical pier or composite pile foundations and other structures can be supported on conventional shallow foundations designed for a very allowable soil bearing pressure. Detailed recommendations for foundations are included in the text.



2.0 PROJECT INFORMATION

The project site is located south of Atlanta Boulevard in Lithia Springs, Georgia. The project site is located in an urban area with streets and an intersection. The project site is adjacent to Atlanta Boulevard and is bounded by Atlanta Boulevard to the north and by residential areas to the east. The general location of the project site is shown on the attached site location map.

Topographic site plan was provided by the client dated 11/22/2017. Elevations at the site range from about 100 in the north to 105 feet along the street fronting in the southeast portion of the site.

It is estimated that the project will consist of street construction and development of a parking lot in the boulevard area. Details of the site are as follows:

- 27' L of 12" at-grade on street
- 240' L of 12" on boulevard
- 110' L and 10' L 12" sidewalks
- 2400' L of at-grade lot
- Street lighting and site lighting

Based on an aerial and associated attachments for the site dated 11/2/2020, it is estimated that the boulevard paving details will be as follows:

Table 1: Boardwalk Pier Reaction Loads

Direction	Service Loads (kips)	Factored Loads (kips)
Vertical	24 LLL	4 LLL
Lateral (horizontal)	10	2

Based on an aerial and associated attachments for the site dated 12/1/2020, it is estimated that the bridge-contour truss will be supported on 4 spans and the elevations at each span location will be as follows:

Table 2: Bridge-Contour Truss Reaction Loads

Direction/Load Type	Unfactored Loads (kips)
Vertical LLL	47
Lateral (horizontal) in	
Vertical (horizontal) in	-
Vertical (horizontal) in	-10



o p eli ina y fo n ation e o en ations e ill ass e a ial se i e loa s anging fo 20 kips o less to 0 kips fo the est oo obse ation pa ilion an othe st t es

f the a t al plans site ga ing an fo n ation loa s info ation a y signifi antly fo the abo e anti ipate al es nite ons lting st be onta te to ete ine if o e o en ations sho l be e-e al ate an o e ise



3.0 PURPOSE

The purpose of this geotechnical exploration was to assess the general type and condition of the subsurface materials at the project site and to provide foundation recommendations for boardwalk retaining walls observation to ensure the facility stays safe during earthquake activity and other geotechnical related issues relevant to this project.



4.0 SCOPE

The scope of geotechnical exploration includes the following items:

1. Boring layout and logging negotiations
2. Final reconnaissance of the site for a geotechnical standpoint
including fifteen 12-inch diameter Test Tube borings and one offset boring to assess the quality and consistency of the subsurface soils
4. Final evaluation of the soil samples obtained including field-testing program for the identification and classification
of the following laboratory testing consisting of fifteen 1-gallon sieve analysis with hydrometer and fifteen 1-gallon liquid limit, plasticity, 40 natural moisture tests, two non-flame compression tests and one dilatancy test on representative soil samples as well as eight permeability flow and settlement tests at representative locations
analyzing the existing soil conditions with respect to the proposed construction and
7. Reporting this report to document the results of field-testing program and engineering analysis and to provide findings and general recommendations



5.0 SUBSURFACE CONDITIONS

The geotechnical exploration for the project consists of fifteen (15) Test Borings and one (1) offset boring designated B-101 to B-111.

Initially, each of the borings encountered a thin surficial layer. Beneath the surficial materials, boring B-101 encountered approximately 2 feet of fill soils, borings B-102 and B-103 encountered between 4 to 6 feet of fill soils, and borings B-104 and B-105 encountered 2 feet of fill soils. The fill encountered consists of very loose to fine sand with varying amounts of silt clay and silt. Borings B-106 and B-107 also encountered layers of fine sand with some silt and clay. The Standard Penetration Test (SPT) results are as follows in the fill and range from 2 blows per foot (bpf) to 11 bpf and those within the fill layers are as follows:

Below the fill in aforementioned borings and the ground surface in the remaining borings, typical residual soils of the immediate physiography in the region were encountered in the borings. The residual soils generally consist of very loose to very dense sand with varying amounts of silt clay and silt. The soils are generally soft to stiff with varying amounts of sand, silt, and clay. The SPT results are as follows within the residual soils and range from 2 to 7 bpf, those within the residual soils range from 2 to 1 bpf and those within the residual soils range from 2 to 2 bpf.

Typically, the maximum blow count was encountered in borings B-101 through B-103, B-106, B-107, and B-114 at depths ranging from 1 foot to 2 feet. This is a testament to the fact that can be penetrated with a soil boring gauge that has blow counts in excess of 100 bpf. The blow counts were classified as very dense sand with varying amounts of silt and clay.

The groundwater level in borings B-101 through B-110 and B-114 at depths ranging from 1 foot to 2 feet. The groundwater level in Test Borings is the depth that the boring cannot be advanced with a soil boring gauge. The groundwater level within residual soils generally represents a seasonal water table less than 2 feet above the base of the boring.

Groundwater was encountered in borings B-101, B-102, B-104, B-105, B-106, B-107, B-108, B-109, B-110, B-111, B-112, B-113, and B-114 at depths ranging from 1 foot to 1 foot at the time of drilling. Within 24 hours after drilling, groundwater levels should be anticipated to fluctuate with the change of seasons. The groundwater level is very low to high precipitation. The water table changes in the flood plain or at the post-peak of the site.

The borings were backfilled with soil cuttings.

For a more detailed description of the subsurface conditions, please refer to the boring logs in the Appendix. A boring log summary table is presented below.



Table 3: Summary of Subsurface Conditions

Structure	Boring No.	Ground Surface Elevation ¹ (ft-msl)	Bottom of Fill Depth (ft)	24-hr GW Depth (ft.)	Depth to PWR (ft.)	Depth to Refusal (ft.)	Termination Depth (ft)
Steel Trestle Estimation Boring	B-101						
	B-102		2			7	7
	B-114				1	2	2
Concrete Tails Boatwalk	B-10	01		2	0		
	B-104	02		1	2	2	2
	B-10	04			1	17	17
	B-10	01	2		0	7	7
	B-10	01			1	14	14
	B-10	0			1	0	
	B-10	0				1	1
	B-110					11	11
	B-111				4		0
	B-112	2					0
Retention Area	B-107	07				1	1
Retention Area Foundation	B-11	1	2				2
Test Point	B-11	12	4				20
Notes 1. Ground surface elevations are estimated from site topography appropriate by the client. Date filed: 11/22/201							



6.0 LABORATORY TESTING PROGRAM

Laboratory testing for this project includes fifteen (15) grain size analysis with hydrometer and fifteen (15) the best limits forty (40) natural moisture tests to determine optimum moisture content and one (1) triaxial test on representative soil samples. The results of the moisture content tests are shown on the boring logs next to the respective soil samples tested. A narrative description of the laboratory tests and the laboratory test results are included in the Appendix.

Light permeability, chloride and sulfate tests were also conducted on representative soil samples and the results tabulated below.

Table 4: Soil Corrosivity Test Results

Boring	Depth (ft.)	Soil pH (S.U.)	Soil Resistivity (ohm-cm)	Chloride (mg/kg, ppm)	Sulfate (mg/kg, ppm)
B-102	2 - 4	7.2	14100		0
B-10	2 -	4.1	1400		
B-104	2 -	4.04	100		27
B-10	2 - 4		2100	4	10
B-10	2 - 4	1	10	74	4
B-110	2 -		1000		21
B-112	2 - 4	7	0	4	0
B-114	2 -		100	4	7



7.0 DISCUSSION AND RECOMMENDATIONS

The following observations are based on the existing of the proposed construction the data obtained in the soil test borings at site reconnaissance and observations with subsurface conditions like those encountered at the project site

It is noted that notwithstanding the presence of the proposed construction the data obtained in the soil test borings at site reconnaissance and observations with subsurface conditions like those encountered at the project site

7.1 Existing Fill

Below the ground surface boring B-11 encountered approximately 2 feet of fill soils borings B-101 and B-11 encountered between 4 to feet of fill soils and borings B-102 and B-10 encountered 2 feet of fill soils. The fill encountered generally consists of very loose to fine sand with varying amounts of silt clay and is generally appeared to be free of debris and organic content and has a permeability Test resistance - average of 2 blows per foot bpf to 11 to bpf

Since any site containing non-entire existing fill materials it is not necessary to find deep areas of fill soft soils trash pits or debris topsoil or less elements of proposed construction blast or other non-suitable materials within existing fill materials. The quality of the fill should be sufficient at the time of construction by providing and possibly the excavation of test pits and soft or other non-suitable soils if encountered should be removed from the area of the planned construction notwithstanding the presence that the project budget in less stringent requirements in the event that areas containing low consistency soils that cannot be densified in place or other non-suitable materials existing overall encountered within the fill

7.2 Site Preparation

In order to develop mainly for borings on ground existing vegetation and trees in clearing their footprint should be removed from the area of the proposed construction overall of trees should include overall of their footprint height may extend to several feet below ground

Any elements of proposed construction or non-entire utilities should be located to at least 10 feet or the perimeter of proposed building footprints. Sanitary utility lines should be located and removed from utility pipes are left in place within the non-structural areas of the site they should be filled-in and pressed with the ground having a 2 - day compressive strength of at least 100 psi

In order to place any engineer fill or concrete of construction areas to be filled shall be foundations slabs and pavements should be provided with a fully loaded tank - a level of proof loading should be performed under the observation of the geotechnical engineer on his representation so that areas which exhibit piping or a type of settlement proof loading may be treated by a method or other by the geotechnical engineer. This method may consist of nailing and backfilling with suitable engineer fill replacing with aggregate and a layer of sheet piling or other method that is deemed suitable



Due to the presence of non-competent existing fill soils a easement requiring stabilization and overall an
engineer shall be anticipated and budgeted for during site preparation.

7.3 Difficult Excavation

Typically, the rock mass encountered in borings B-101 through B-110 and B-114 at depths ranging from 1 foot to 2 feet generally consists of sandstone and shale. It is noted that shallow rock may be present between areas of the easement.

It is also important to note that depths to rock and a void should be noted in the geologic log and rock should be noted in the construction log at shallow depths between borings to the boring locations for this study.

Typically, the rock is loosened by ripping with large open-pulling single tooth rippers in association with the use of special equipment. The use of explosives is typically not recommended for this type of rock. The use of explosives is typically not recommended for this type of rock.

It is noted that the following definitions for rock are in the International Union of Pure and Applied Chemistry (IUPAC) definitions and help a contractor to estimate the cost of excavation.

1. General excavation by using an original volume of more than 1 cubic yard which cannot be excavated with a single-tooth ripper and by a method having a minimum weight of not less than 10,000 lbs. of single-pull material.
2. The excavation by using an original volume of more than 12 cubic yards which cannot be excavated with a backhoe having a bucket weighing more than 40,000 lbs. and single-tooth teeth.

7.4 Groundwater Considerations

Groundwater was encountered in borings B-101, B-104, B-110, and B-111 through B-114 at depths ranging from 1 foot to 1 foot at the time of drilling. It is noted that the groundwater is not expected to significantly impact construction. The groundwater level is expected to fluctuate with the change of seasons during periods of high precipitation or changes in the flood plain water table for the area.



7.5 Caving Considerations

Recommendations should be consistent with the geotechnical safety and health regulations regarding flattening of the excavation side walls and the use of bracing may be necessary to maintain stability during construction.

7.6 Foundation Design and Construction

7.6.1 First Steel Truss Pedestrian Bridge

The proposed preliminary steel truss pedestrian bridges, the first one located on the west end of the project by bents B-101 and B-102 and the second one on the east end of the project by bent B-114. Both shall use deep foundation systems as detailed for the following:

7.6.1.1 Shallow Foundation Recommendations

Following site preparation as required, the first steel truss pedestrian bridge shall be supported by bents B-101 and B-102 and shall be supported on a shallow foundation system. Based on the subsurface exploration data and pier load, a net allowable soil bearing pressure of 2,000 pounds per square foot (psf) is recommended for foundation design for a maximum total settlement of 1 inch for the footing bearing at least 12 inches below the ground surface and at least 2 feet below the footing is not to be backfilled with 12 inches of #7 stone below 12 inches of compacted aggregate base.

Based on a net allowable soil bearing pressure of 1,000 pounds per square foot (psf) and based on foundation design, a minimum depth of 24 feet below ground surface shall be required for stabilization of the foundation on bent B-101 at least 24 feet below ground surface. 24-hour stability shall be maintained on the footing bearing elevation ground level. The foundation shall be designed and placed to allow for backfill and footing construction. The foundation shall be placed to allow for backfill shall be at least 2 feet outside the footing limits.

For the remaining footing dimensions of 20 inches for strip footings and 24 inches for square footings, footings shall bear at least 12 inches below finished grade for construction. The geotechnical engineer shall evaluate each footing foundation prior to steel reinforcement on site. The foundation shall be placed to allow for backfill and footing construction. The foundation shall be placed to allow for backfill shall be at least 2 feet outside the footing limits.

Foundation shall be maintained to prevent a reduction of water in footing foundations. Foundation shall be properly soil softened by the water shall be provided to the geotechnical engineer or his representative shall be available for the area.

7.6.1.2 Deep Foundation Recommendations

Due to the presence of shallow bedrock within the proposed 20 feet below ground surface foundation system consisting of driven piles, as noted, is a viable foundation option for the first steel truss pedestrian bridge. The steel pile shall be supported on end-bearing aggregate piles placed to a depth of approximately 7 feet below ground surface with an



allowable bearing pressure of at least 20 ksf. It is assumed that the side shear and the passive pressure in the upper feet of the pile be neglected in the foundation analysis so side resistance is expected to be negligible for this steel truss pedestrian bridge. On the proposed design loads, a general pile with at least 1 inch diameter and a $f_c = 4,000$ psi installed to a general depth may be an alternative foundation system for the bridge elements to resist both axial and lateral loads for less than 0 inch lateral deflection.

7.6.2 Second Steel Truss Pedestrian Bridge

The second steel truss bridge may be supported by both shallow deep foundation systems. The selection of the foundation system will depend on construction cost and construction impact to environmentally sensitive areas.

7.6.2.1 Shallow Foundation Recommendations

Following site preparation as assumed, the second steel truss pedestrian bridge structure area of bridge B-114 could be supported on shallow deep foundations. Based on the subsurface exploration data and pile load test, at least 2 feet below the footing is not a bankfill with 12 inches of 7 stone below 12 inches of compacted aggregate base. Below that is a net allowable soil bearing pressure of 2,000 pounds per square foot. A shallow foundation design for a total settlement of 1 inch for the footing bearing at least 12 inches below the ground surface is recommended in bridge B-114 as an alternative at least 2 feet below ground surface. 24-hour stability analysis will depend on the footing bearing elevation. Groundwater table may be expected during construction and replacement with compacted granular fill and footing construction.

It is assumed that footing dimensions of 20 inches for strip footings and 24 inches for square footings should bear at least 12 inches below existing finished grades for foundation. The geotechnical engineer shall evaluate each footing foundation prior to steel information on the plan and sections that are observed should be compared to the test bearing data and design elements. Final bearing material is assumed that it should be evaluated and replaced or otherwise treated as assumed by the geotechnical engineer.

Foundation groundwater should be maintained to prevent a reduction of water in footing foundations. Foundation groundwater should be expected to be partially soil softened by the water should be expected and the geotechnical engineer or his representative should evaluate the area.

7.6.2.2 Deep Foundation Recommendations

The second steel truss pedestrian bridge may be supported on a deep foundation system to minimize impact to environmentally sensitive areas. The existing station top-of-shoulder bank construction is being considered for the project. This construction approach would include installation of the deep foundation system for top of the shoulder. A pile glass composite piles installed with a battered angle would be a viable deep foundation system option for the second steel truss pedestrian bridge.



Installation of fiber glass piles shall follow the manufacturer's recommendations to ensure they are not over-tightened. The spacing of the bolts and the piling should provide the integrity of the material. The use of washers and backing plates are recommended for any bolt connections into the pile despite the high strength of fiber glass. Connections should be designed to be spaced at a large area as compared to steel. All connections shall be designed by the project engineer.

Based on the load specifications, the preliminary design calculations to determine pile size and configuration and estimate installation depths. The preliminary fiber glass foundation system consists of 12-inch diameter piles with a minimum axial compressive strength of at least 100 ksi. All thickness of 0.7 inches are installed to a minimum depth of 1 foot. 10-inch diameter pile diameter or provide the axial strength and geotechnical load capacity. It is not possible to geotechnical lateral load capacity keep lateral deflections to less than 0.1 inches for the project.

Note that only one boring B-114 was available in the location of the section. This information should be supplemented with the soil borings boring B-11 located at the other end of the bridge as well as the area with a light-duty steel piles are not considered for this project as heavy pile driving may not be suitable for pile installation and not be suitable for backfill top-on construction.

Table 5: Summary of Preliminary Truss Bridge Foundation Recommendations

Structure	Boring No.	Foundation Type	Allowable Bearing Pressure ² (psf)	Pile Embedment Depth ² (ft-bgs)
Bridge 01	B-101 B-102	1 - diameter cast piles	1000	7
		12 - diameter fiberglass piles	2000	1
<p>Notes</p> <p>1. At least 2 feet below the depth of footing needs to be beneath and backfill with 12 inches of 7 stone below 12 inches of open aggregate base B.</p> <p>2. Load capacity in an - soil an associated attachment for Joseph O'Connell L.</p> <p>Date: 12/1/2020</p>				

7.6.3 Concrete Trails/Boardwalks

When specifying footings, it is initially considered for the boardwalks where the presence of soft loose soils within the upper five to ten feet below ground surface and the presence of shallow ground water. Shallow footings are not considered a viable foundation option for the boardwalk project. It is recommended to consider a cost-effective foundation system for the boardwalk project.



Helical piers are installed by rotating helical anchors through the pipe or between adjacent to ensure bearing capacity on the anchor and the specific pier type helical piers may be designed for a working capacity of tons. The helical piers may have an uplift capacity similar to the compression capacity provided by the efficient bearing of the helical pier section. Lateral resistance is typically provided by installing piers at a batter of 1h 4 14° to 1h 1 4°. The helical pier anchor is installed typically provides detailed design and installation details helical pier shafts are typically provided with three helices with helices spaced typically at 10, 12 and 14 inches in diameter of the total anchor helices are arranged in series typically for 10, 12 and 14 inches in diameter helical pier shafts are in different types and sizes ranging from 3/4 inch solid steel shafts 1 1/2 to 2 1/2 inches in diameter to hollow steel shafts ranging from 2 7/8 to 4 inches in diameter. The helical pier configurations and sizes are also available by different helical pier systems. The capacity of the helical pier is controlled by the diameter to be applied to the helical pier anchor assembly during installation. The nominal ultimate helical pier compression tension capacity is related to the torque required during installation. Helical pier shafts are available for shallow installations where the bottom of the pier is expected to be driven into rock creating a "spin on" condition.

During installation of the helical pier shafts, the operator should be maintained by a representative of the contractor to verify pier type, location, length, installation conditions, and estimate capacity. The contractor should be allowed to verify the contractor's proposed equipment and installation procedure prior to mobilization and construction.

When opening on lateral availability and other factors, it is possible that other deep foundation alternatives may be economically feasible for this project. The contractor should be glad to evaluate other deep foundation options and provide recommendations for such if needed. Additional subsurface exploration may be required depending on the type of alternative deep foundation option considered.

7.6.3.1 Helical Pier Recommendations

Based on the load provided, the following are recommended helical pier design alternatives to meet the helical pier shaft configuration and estimated installation depths. The helical pier foundation system consists of two batter piles at 1h 4 14° installation angle with three helices 10, 12, and 14 inches in diameter as they are installed to depths below helical shafts ranging from 14 to 20 feet depending on the subsurface conditions encountered in the site borings complete along the borehole for this project. The batter helical piers are designed to provide 0 kips of ultimate compression load, 24 kips of axial load, and 2 kips of axial load for the lateral load, 1 kips pile driven into compression or tension load. Note that helical pier installation contractor should allow the contractor to design for the project and that the pier design and construction are for estimating foundation quantities and engineer's cost estimates. The helical pier foundation design and construction are based on the details below and in detail in the Appendix.

When opening on lateral availability and other factors, it is possible that other deep foundation alternatives may be economically feasible for this project. The contractor should be glad to evaluate other deep foundation options and provide recommendations for such if needed. Additional subsurface exploration may be required depending on the type of alternative deep foundation option considered.



Table 6: Summary of Preliminary Helical Pier Design Recommendations

Structure	Boring No.	Depth to Dense Soil (ft-bgs) ($N_{60} > 30$ bpf)	Pile Type	Battered Pile Design Compression Service Load ¹ (kips)	Battered Pile Minimum Installation Torque ² (Ft-lb) ($K_t = 10 \text{ ft}^{-1}$)	Minimum Depth to Bottom Helix (ft-bgs)
Concrete Tails Boatwalk	B-10		17 - dia 1- \square shaft 14 12 10 elias eie 2 Battered Piles at 1h 4 14° ft To rotating 10 00 t-lb	0	10	
	B-104	1				11
	B-10	4				12
	B-10 10					1
	B-10					
	B-10	1				1
	B-110					11
	B-111	2				2
	B-112	2				2
<p>Notes</p> <p>1 Battered piles are designed to handle the service axial load 24.4 kips and lateral load 1 kips. The 1 kips service lateral load in each pile total of kips per bent is transferred to pile axial compression and tension load respectively when the load is applied along the bent.</p> <p>2 At least one vertical pile load testing the top large helix 14 shall be performed to check the factored service lateral ultimate helical pile ultimate rotational length bearing capacity for the installation to be used in the field. The ultimate initial to ultimate ratio is based on a $t = 10 \text{ ft}^{-1}$ pin-on-tiles test to obtain a geofactor.</p>						

7.6.4 Lightly Loaded Structures

Following site preparation as shown in the proposed lightly loaded structure, the adjacent pile installation shall be based on shallow foundation systems. Based on the subsurface exploration data, an assumed axial service load of 20 kips or less to a depth of 0 kips range of net allowable soil bearing pressures of 1,000 to 2,000 pounds per square foot.



are shown for foundation design for a total settlement of 1 in h These are shown in the table below

Table 7: Allowable Bearing Pressure for Lightly Loaded Structures

Boring	Structure	Column Loads (kips)	Allowable Bearing Pressure (psf)
B-107	intermediate	≤20	1000
		0	2000
		0	2000
B-11	intermediate foundation	≤20	2000
		0	2000
		0	1000
B-11	test oo	≤20	1000
		0	2000
		0	2000

7.7 Ground Floor Slabs

Ground floor slabs are shown as being 12 inches thick. It has been determined that the floor slab design is often disturbed by water foundation utility line installation and other construction activities between grouting a slab construction. For this reason, the geotechnical engineer should evaluate the slab design immediately prior to placing the concrete. The geotechnical engineer to be retained should be responsible to obtain an explanation from the engineer fill to at least 100 percent of its standard unit weight.

7.8 Earthwork

The on-site soils free of organic and other deleterious materials should generally be suitable for use as engineering fill with proper moisture content. Aerially applied earthwork can be used as engineering fill if it breaks progressively to meet gradation requirements and also be filled with soil to meet gradation requirements.

Due to the presence of high silt contents, some of the on-site soil may be sensitive to moisture variations. During rainy seasons, these soils will be difficult to compact. A partial consolidation during the placement of wet earthwork on-site soils may need to be considered. An explanation of the soils. These soils should be placed within a narrow range of their optimum moisture content typically within about 1 percent of optimum moisture to achieve proper compaction. Typical estimates for suitable fill are no organic plasticity index less than 2 and a liquid limit of 40 or less with not more than 10 percent greater than 4-inches. These estimates should also be applied to impure soils if necessary.



osity and moisture content shall always be maintained to prevent saturation of the proposed soils in case of seasonal rainfall. The bearing capacity of the soils shall also be determined based on the soil moisture content and the moisture content shall be maintained. The bearing capacity of the soils shall also be determined based on the moisture content taken by the contractor to help protect the soils from saturation during construction.

Moisture content determinations shall be performed for each soil type set to provide adequate assurance for quality assurance and testing. The natural moisture content at the time of construction shall be maintained so that they are within moisture content limits that will allow the earth to be compacted to the required density.

7.9 Slopes

It is recommended that the fill is to be placed on existing slopes of grades greater than 4:1. The slopes shall be benched to prevent sliding of the fill mass along the existing surface. This can be achieved by notching the slope face by at least about 1 to 2 feet horizontally with the top to be as each lift is completed. Typical benching detail is provided in the appendix.

Permanent slopes shall be constructed no steeper than 2:1. All slopes of up to 20 feet in total height constructed to 2:1 shall be acceptable assuming proper benching and placement of engineering fill. Slopes greater than 20 feet shall be evaluated for global stability and shall be designed by a licensed geotechnical engineer. Slopes higher than 20 feet shall be benched if less than desirable soils such as topsoil or wet soils are to be placed on slopes. If an appropriate level of quality control and construction testing and the supervision of the geotechnical engineer is not planned, steep slopes constructed to 2:1 slopes will not likely be achieved. Flat slopes shall be considered.

All slopes shall be protected for erosion during construction and provide with appropriate permanent vegetation. Other slopes after construction shall be protected for runoff flow by means of berms and drainage ditches to prevent runoff on slopes. Although on-site channels appropriate vegetation shall consist of fast-growing grasses that will rapidly establish a dense root mat over the entire slope. Landscaping consisting of isolated shrubs and pine stands will not provide adequate slope protection.

Minimum berms retaining all setbacks for the nearest edge of foundations of at least 10 feet for the rest of slopes is recommended. Minimum setbacks of 5 feet is recommended for permanent berms.

7.10 Fill Placement

Moisture content determinations shall be performed for each soil type set to provide adequate assurance for quality assurance and testing. The natural moisture content at the time of construction shall be maintained within moisture content limits which will allow the earth to be compacted to the required density. This is generally within the percentage points of the optimum moisture. The contractor shall be permitted to increase or decrease soil moisture content as needed to achieve the required moisture content of construction.



The fill shall be placed in thin lifts not to exceed in thickness and compacted evenly on the fill before to at least percent of tan a to T a i y density within top to feet and at least percent of tan a to a i y density else here on the site to then backfill alk-behind type of compaction equipment is typically selected so as to ensure proper fill in thin lifts not to exceed in height especially within areas and percent areas

Geotechnical engineer on a field-basis shall observe during operations in-place density tests taken by that individual will assess the degree of compaction being obtained. The frequency of the testing shall be determined by the geotechnical engineer

7.11 Retaining Walls

The following retaining wall conditions pertain to cast-in-place bilting and site retaining walls within the easement area and are not intended for block walls for block walls are planned on the site. Notifications shall be notified by a separate additional evaluation will be required to provide conditions specific to the planned wall types and locations

The design of retaining walls shall include the determination of the lateral pressure that will act on the wall. The lateral earth pressure is a function of the soil properties such as the angle of internal friction and the cohesion of the soil. This determination is basically dependent upon the relative rigidity of the wall system

The active earth pressure condition develops when the wall moves away from the soil as a result of rotation. The active condition exists when there is no lateral restraint on the soil such as walls which are rigidly restrained like a basement foundation wall. The passive condition occurs when the wall moves into the soil

The following equivalent fluid pressures are provided for the earth pressure conditions

Table 8 - Lateral Earth Pressures

Earth Pressure Condition	Earth Pressure Coefficient	Recommended Equivalent Fluid Pressure
Active	0.33	4 psf/foot
At-Rest	1.00	4 psf/foot
Passive	2.77	2 psf/foot

Note that consistent horizontal deflections are required to mobilize the passive pressure the effective design shall consider a safety factor of 2 to the state ultimate passive earth pressure design

The equivalent fluid pressures are based on an assumed soil density of 120 pcf and an internal friction angle of 20 degrees and cohesion of 0. The coefficient of friction of 0.4 for sliding may be used for the retaining wall design



The parameters listed above are based on a level properly compacted backfill no further than the full-soil interface and no secondary effects of design of retaining walls. It shall be in accordance with the buoyant unit weight of the in-place soil shall be used to determine the lateral earth pressure. The hydrostatic pressure is based on the actual ponding elevation shall be utilized in the analysis.

Every opening in a wall shall not be subjected to a backfill within 2 feet laterally behind any retaining wall unless the wall is designed for the increase in pressure due to a fully backfilled wall. The effective weight of the retaining wall shall be included in this design. Retaining walls backfill shall be compacted to a minimum of 95% relative compaction. Retaining walls shall be designed for a footing width of a minimum of 12 inches. Retaining walls shall be designed for a minimum of 2 feet in height.

The retaining walls shall be designed by a professional engineer familiar with retaining wall design and existing conditions. The design shall consider sloping backfills, surcharges, and other factors affecting all loadings. The design shall also consider global stability.



8.0 LIMITATIONS

This report is for the use of **Gwinnett County** and the designs of the project described herein may only be applied to this specific project. Conditions and observations have been prepared using generally accepted standards of professional engineering practice in the state of Georgia. Other liability is expressly disclaimed. The firm is not responsible for conditions or observations of others.

The right to rely upon this report and the data therein may not be assigned without the written permission of United Consulting.

The scope of this evaluation is limited to an evaluation of the load-carrying capabilities and stability of the soils. It does not include a determination of the presence of contaminants or other geologic substances. The presence and absence are not implied or suggested by this report and should not be inferred.

Conditions and observations are based upon design information furnished to us and obtained from the previously described exploration and testing program and other pertinent data. They do not reflect variations in subsurface conditions that may exist between borings and in the plane areas of the site. Hidden variations between apparent and actual conditions will be necessary to evaluate actual conditions and observations based upon on-site observations of the conditions.

If the design location of the project is changed, the conditions obtained herein should be considered invalid unless otherwise specified. Changes and observations are either verified or unverified. When design is complete, the firm should be given the opportunity to review the foundation planning plan and applicable portions of the specifications to confirm that they are consistent with the intent of the observations.

UNITED CONSULTING



APPENDIX

General Notes/Narrative of Drilling Operations

Figure 1 – Boring Location Plan

Exploration Procedures

Laboratory Procedures

SPT Boring Logs (16)

Helical Pile Design Recommendations (1)

Lab Summary Sheet (3)

Liquid and Plastic Test Report (2)

Moisture Content Results (2)

Grain Size Distribution Curves (15)

Unconfined Compression Test Report (2)

Triaxial Test Results (2)

Analytical Lab Test Results (19)

Benching Detail

GENERAL NOTES

The soil classifications noted on the Boring Logs are visual classifications unless otherwise noted. Minor constituents of a soil sample are termed as follows:

Trace	0 - 10%
Some	11 - 35%
Suffix "y" or "ey"	36 - 49%

LEGEND



Split Spoon Sample obtained during Standard Penetration Testing



Relatively Undisturbed Shelby Tube Sample



Groundwater Level at Time of Boring Completion



Groundwater Level at 24 hours (or as noted) after Termination of Boring

w Natural Moisture Content

LL Liquid Limit

PL Plastic Limit Atterberg Limits

PI Plasticity Index

PF Percent Fines (Percent Passing #200 Sieve)

γ_d Dry Unit Weight (Pounds per Cubic Foot or PCF)

γ_m Moist or In-Situ Unit Weight (PCF)

γ_{sat} Saturated Unit Weight (PCF)

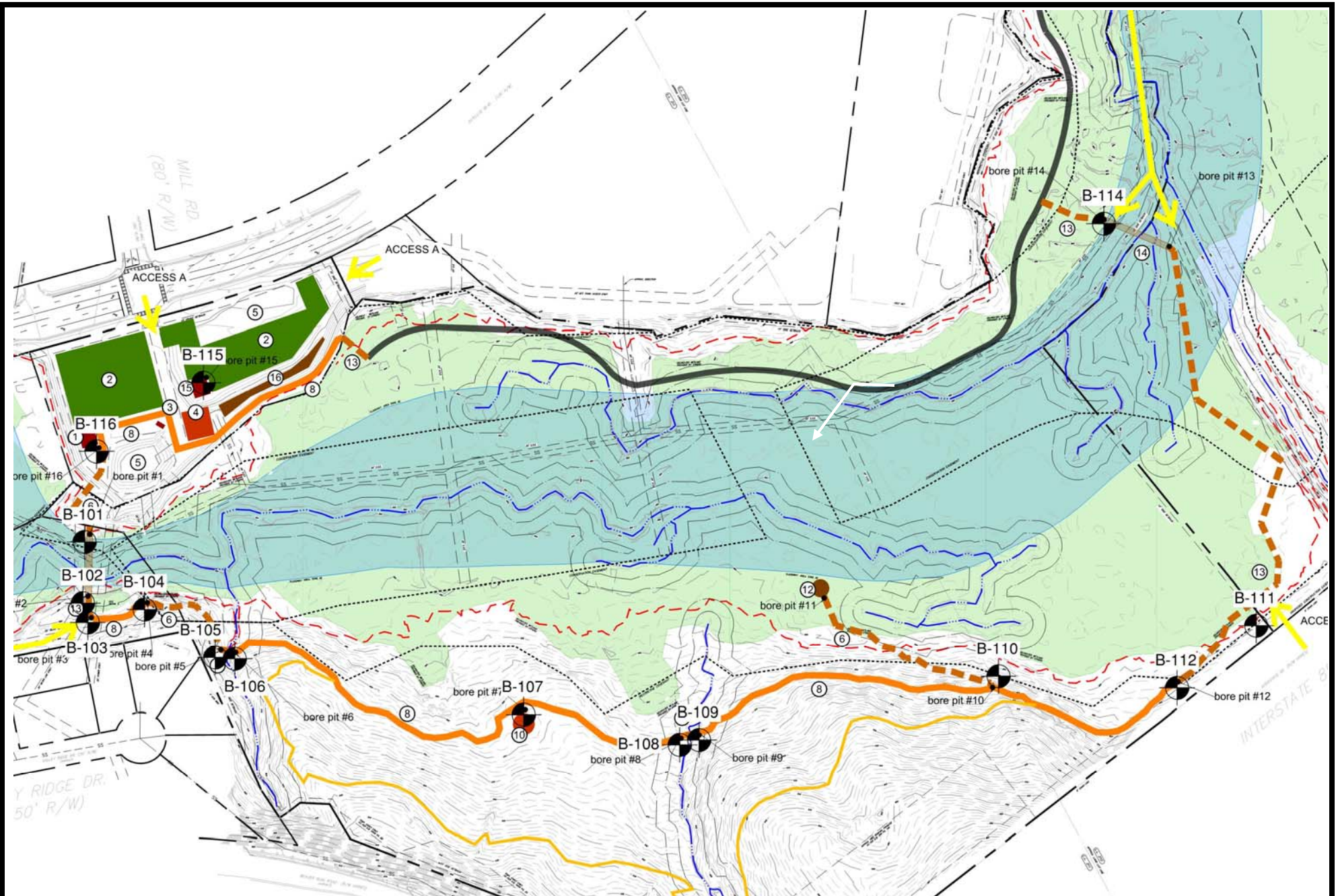
B L T T LL T

The test borings are made by mechanically advancing heli al hollow steel augers into the ground samples are collected at regular intervals in each of the borings following established procedures for performing the standard penetration Test in accordance with

Test procedure 1 soil samples are obtained with a standard 140 mm diameter split barrel sampler. The sampler is first seated to penetrate any loose strata and then driven an additional foot with the blow count of a 140-pounds hammer freely falling a distance of 30 inches. The number of blows required to drive the sampler the final foot is designated the standard penetration resistance. The driving resistance known as the blow count is related with the relative density of granular soils and the consistency of cohesive deposits.

The following table expresses soil consistency and relative densities based on standard penetration resistance values determined by the standard penetration Test.

	<u>SP</u>	<u>consistency</u>
lay an	0-2	very soft
	-4	soft
	-	medium
	-1	stiff
	1 - 0	very stiff
	e 1	hard
	<u>SP</u>	<u>relative density</u>
an	0-4	very Loose
	-10	Loose
	11-1	medium
	20-2	medium dense
	0-4	dense
	0	very dense



Scale:	NTS
Prepared:	SRT
Checked:	RIO
Project No.:	GCP&R-20-GA-04517-01

Notes

Client:	Gwinnett County Parks and Recreation
Site:	Beaver Ruin Wetlands Park South of Satellite Boulevard Duluth, Gwinnett County, Georgia
Title:	Boring Location Plan

FIG. 1



EXPLORATION PROCEDURES

Standard Penetration Test (SPT) borings

Fifteen (15) Test borings designate B-101 through B-112 B-114 through B-111 and one (1) offset boring designate as B-10. See Appendix A at the appropriate locations in Figure 1 on the attached Boring Location Plan Figure 1. The Test borings were performed in general accordance with ASTM D 1586. Soil samples obtained during testing were analyzed and classified according to the Unified Soil Classification System (USCS) in accordance with ASTM D 2487. The name of field operations is in Appendix B in the Appendix.

The test locations in the field were determined by the geotechnical engineer using a hand level and a surveying instrument for existing site features. The test locations should be confirmed by appropriate ground surface elevations were obtained for topographic application by client at file date 11/22/2011. So ground surface elevations at the boring locations should be confirmed by appropriate



LABORATORY PROCEDURES

Grain Size (Sieve) Analysis with or without Hydrometer

Grain size analysis tests are performed to determine the particle size distribution of selected samples tested. The grain size distribution of soils coarser than a number 200 sieve is determined by passing the samples through a standard set of nested sieves materials finer than the number 200 sieve are suspended in water and the grain size distribution is plotted for the time rate of settlement of the different size particles. Fine soil passes through a 200 sieve. Organic soils of that type soak in a solvent for a minimum of 48 hours. Soil is then placed in a glass jar with a hydrometer readings are taken at specified times. Graph is a function of data. These tests are like those described by T 421 and T 422. The results are in Table in the Appendix.

Liquid and Plastic Limits (Atterberg Limits)

Liquid Limit and Plastic Limit tests are in the classification of the soils and provide an indication of the soil behavior with moisture change. The plasticity number is based on the Liquid Limit (LL) and the Plastic Limit (PL). The Liquid Limit is the moisture content at which the soil will flow as a heavy consistency and is the upper limit of the plastic range as determined in accordance with T 41. The Plastic Limit is the moisture content at which the soil begins to lose its plasticity as determined in accordance with T 41. The plasticity number is the difference between the Liquid Limit and Plastic Limit. The Plasticity Number is the ratio of the difference between the in-place moisture and the plastic limit to the Plastic Limit. The data obtained are in the Appendix.

Moisture Content

The moisture content is determined for selected soil samples obtained in the split spoon sample representative portion of each sample as weighed and then placed in an oven and dried at 110 degrees centigrade for at least 1 to 1 1/2 hours. The oven is cooled and the soil is weighed again. The weight of the moisture lost is determined by this data the moisture content of the sample is then calculated as the weight of moisture divided by weight of the soil expressed as a percentage. This test is in accordance with T 221. The moisture content results are in the Appendix on the attached boring logs.

Moisture content is a self indicator of a soil's compressibility. If the soil is to be used as fill the moisture content may be compared to the range of moisture content for high plasticity soils. The moisture content may be a higher



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-101
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/21/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
895	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% PL=21; LL=27; PI=6
	Sand - some silt and clay, trace mica, some rock; loose; dark brown (Fill) (SC-SM) - firm		1		3-3-4-5	7	19	13.9
			2		5-7-4	11	18	13.7
		5			N/A	N/A	12	
890			3		N/A	N/A	12	Offset 5' west and auger refusal at 6' Shelby tube sample collected from 4'-6' bgs
	Partially weathered rock sampled as Sand - trace silt and clay, some rock; very dense; gray (Residual) AUGER REFUSAL AT 6.5 FEET		4		50/1"	50/1"	1	
885		10						Groundwater encountered at 4 feet at the time of drilling and at 3 feet 24 hours after drilling
880		15						
875		20						
870		25						
865		30						
860		35						
855		40						

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-102
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/25/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
900	Grass; 4" Topsoil	0						Automatic Hammer Efficiency = 94.7%	
	Sand - some clay, trace silt; very loose; red-brown (Fill)		1		1-1-1-1	2	3		
	Sand - trace clay and silt, some rock; medium dense; orange-brown/black/white (Residual) (SM)		2		4-12-16-19	28	6		
895	- some silt and clay, trace gravel; loose; brown and tan	5	3		18-4-3-2	7	15		22.3
	Partially weathered rock sampled as Sand - some clay, trace silt, some rock; very dense; orange-brown/gray-brown		4		4-50/5"	50/5"	9	20.7	No groundwater encountered at time of boring
890	AUGER REFUSAL AT 7 FEET	10							
885		15							
880		20							
875		25							
870		30							
865		35							
860		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-103
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/25/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
	3" Topsoil	0						
900	Sand - some silt and clay, trace mica; very loose; red-brown/orange-brown (Residual) (SM)	1	1	1-1-2-1	3	24	19.6	Automatic Hammer Efficiency = 94.7% PL=26; LL=35; PI=9
	- some clay, trace silt, trace rock; loose	2	2	2-1-6	7	18		Near drain ditch and creek
	- trace clay; tan-brown/red-brown	5	3	N/A	N/A	24		Shelby tube sample collected from 4'-6' bgs
895	- some silt, trace clay; dense; gray-brown/orange-brown	4	4	12-14-23-30	37	24	15.3	Groundwater encountered at 2 feet at the time of and 24 hours after drilling
	Partially weathered rock sampled as Sand - some clay, trace silt, some rock; very dense; brownish-gray	10	5	50/3"	50/3"	3	12.3	
890	AUGER REFUSAL AT 9 FEET							
		15						
885								
		20						
880								
		25						
875								
		30						
870								
		35						
865								
		40						
860								

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-104
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/24/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass; 3" Topsoil	0							Automatic Hammer Efficiency = 94.7%
900	Sand - some silt, trace clay, trace mica; loose; orange-brown/tan-brown (Residual) - trace rock		1		3-3-3-3	6	24	9.4	
			2		3-4-6	10	18		
	Clay - some sand, trace silt, trace mica; orange-brown	5	3		N/A	N/A	24		Shelby tube sample collected from 4'-6' bgs
895	Sand - trace silt and clay, trace mica; loose; orange-brown - firm		4		4-4-5-9	9	24	13.3	
			5		7-9-9-8	18	24		
890		10							
	- some silt, some mica; golden brown		6		4-7-9	16	18		
885									Groundwater encountered at 16 feet 24 hours after drilling Groundwater encountered at 18 feet at the time of drilling
	- some rock; dense		7		21-23-25	48	18		
880		20							
	Partially weathered rock sampled as Sand - trace silt and clay, some rock; very dense; brownish-gray AUGER REFUSAL AT 25 FEET	25	8		50/6"	50/6"	5		
875									
		30							
870									
		35							
865									
		40							



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-105
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/25/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
905	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% PL=24; LL=45; PI=21 Offset 15' North	
	Clay - sandy, some silt, trace mica; soft; red-brown/orange-brown (Residual) (CL)		1		2-2-2-2	4	24		27.5
	Sand - trace silt and clay, trace mica; firm; orange-brown/gray-brown		2		3-5-7-7	12	24		16.4
900	- trace rock; medium dense	5	3		8-12-15-14	27	24		8.5
			4		8-12-15-10	27	24		15.7
895	- some rock; firm	10	5		5-5-6-4	11	24		
890	Partially weathered rock sampled as Sand - trace silt and clay, some rock; very dense; red-brown/gray	15	6		6-50/3"	50/3"	5		
	AUGER REFUSAL AT 17.5 FEET							No groundwater encountered at time of boring	
885		20							
880		25							
875		30							
870		35							
865		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-106A
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/24/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)	
900	Grass; 3" Topsoil	0						Offset 10 feet north of B 106; Straight-augered to 8 feet bgs
895								
890	Sand - some silt, trace clay, trace mica and rock; firm; tan-brown/dark brown (Residual)	5	5		3-5-10-9	15	24	Groundwater encountered at 5 feet 24 hours after drilling
885	Partially weathered rock sampled as Sand - trace silt, some rock; very dense; gray AUGER REFUSAL AT 14 FEET	15	6		50/1"	50/1"	1	Groundwater encountered at 10 feet at the time of drilling
880		20						
		25						
875								
		30						
870								
		35						
865								
		40						
860								



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-107
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/24/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7%	
905	Clay - some sand, trace silt, trace mica; firm; red-brown/tan-brown (Residual) - stiff		1		2-3-3-4	6	24		
			2		3-4-5	9	18		
		5	3		N/A	N/A	24		
900	Sand - some silt, trace clay, trace rock; loose; golden-brown		4		2-3-3-2	6	24		Shelby tube sample collected from 4'-6' bgs Groundwater encountered at 6 feet 24 hours after drilling Groundwater encountered at 8 feet at the time of drilling
			5		2-3-5-5	8	24		
		10							
895	- some rock; dense		6		5-8-23	31	18		
		15							
890	AUGER REFUSAL AT 16.5 FEET								
		20							
885									
		25							
880									
		30							
875									
		35							
870									
		40							



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-108
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/24/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
905	Grass; 4" Topsoil	0						Automatic Hammer Efficiency = 94.7%	
	Sand - some clay, trace silt, trace mica; loose; red-brown/gray (Residual)	1	1	█	2-3-4-4	7	24	19.0	Groundwater encountered at 1 foot 24 hours after drilling Offset 10 feet east and refused at 10 feet bgs Groundwater encountered at 5.5 feet at the time of drilling
	Clay - some sand, trace silt, trace mica; firm; gray-brown/tan-brown	2	2	█	3-3-4-3	7	24		
900		5	3	█	2-2-3-3	5	24	23.3	
	Sand - some clay, trace silt, trace rock; loose; gray-brown	4	4	█	3-3-3-3	6	24	20.8	
	Partially weathered rock sampled as Sand - trace silt, some rock; very dense; gray	5	5	█	50/3"	50/3"	1		
895	AUGER REFUSAL AT 9.5 FEET	10							
890		15							
885		20							
880		25							
875		30							
870		35							
865		40							



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-109
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/24/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% PL=26; LL=46; PI=20 Groundwater encountered at 4 feet at the time of drilling and at 3 feet 24 hours after drilling Shelby tube sample collected from 4'-6' bgs: PL=35; LL=50; PI=15	
905	Clay - sandy, some silt, trace gravel; firm; orange-brown/gray (Residual) (CL)		1		2-3-4-3	7	24		23.1
			2		2-3-3	6	18		26.0
	Sand - some silt and clay; loose; dark tan (SM) - trace clay, mica and rock fragments; golden brown	5	3		N/A	N/A	24		30.3
900			4		2-3-3-2	6	24		38.6
			10	5		2-2-3-2	5		16
895									
	Partially weathered rock sampled as Sand - trace silt and clay, some rock; very dense; gray-brown AUGER REFUSAL AT 15 FEET	15	6		3-13-50/2"	50/2"	12		
890									
		20							
885									
		25							
880									
		30							
875									
		35							
870									
		40							
865									

PL=Plastic Limit
 LL=Liquid Limit
 PI=Plasticity Index
 NM=Natural Moisture



BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-111
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/25/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
890	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% PL=34; LL=51; PI=17 Shelby tube sample collected from 4'-6' bgs: PL=30; LL=49; PI=19 Groundwater encountered at 5 feet at the time of drilling and at 4 feet 24 hours after drilling	
	Silt - sandy, some clay, trace mica; firm; red-brown/orange-brown (Residual) (MH) - trace clay; soft; red-brown/tan-brown		1		2-2-3-2	5	24		25.9
			2		3-2-2	4	18		19.9
885	- some sand and clay; dark brown (ML)								
	Clay - some sand, trace silt; soft; gray - very soft		3		N/A	N/A	24		30.6
			4		2-2-2-2	4	24		36.6
880			5		1-1-1-1	2	24		
		10							
875	Silt - some sand, trace clay, trace mica; firm; orange-brown/gray-brown	15	6		4-2-3	5	18		
870	Sand - some clay, trace silt, trace mica and rock; loose; orange-brown/gray-brown	20	7		2-3-6	9	15		
865	- medium dense	25	8		6-12-11	23	18		
860	Clay - some sand, trace silt, trace mica and rock; stiff; orange-brown/gray-brown	30	9		3-3-7	10	18		
	BORING TERMINATED AT 30 FEET								
855		35							
850		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD
 NORCROSS, GEORGIA 30071
 (770)209-0029, FAX (770)582-2800

BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-112
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/25/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES				NOTES		
			NO.	TYPE	BLOWS/6"	N-VALUE		RECOV. (%)	W (%)
	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% Bulk sample collected from 0'-5' bgs Groundwater encountered at 5 feet at the time of drilling and at 3.5 feet 24 hours after drilling	
890	Sand - some silt, trace clay, trace mica; loose; red-brown/orange-brown (Residual) - very loose		1		1-2-3-2	5	24		16.7
	- some clay		2		2-2-2-2	4	24		
			3		2-2-1-2	3	24		26.1
885	Clay - some sand, trace silt; very soft; gray		4		1-1-1-1	2	24		
	Sand - some clay, trace silt, trace mica; very loose; red-brown/gray		5		1-1-1-1	2	4		
880		10							
	Silt - some sand, trace clay, trace mica; soft; golden brown		6		1-2-1	3	10		
875		15							
	- firm		7		2-2-3	5	18		
870		20							
	- trace rock; stiff		8		3-4-6	10	10		
865		25							
	- very stiff		9		6-11-14	25	18		
860	BORING TERMINATED AT 30 FEET	30							
		35							
855									
		40							



BORING LOG

CONTRACTED WITH: Gwinnett County Parks and Recreation BORING NO.: B-114
 PROJECT NAME: Beaver Ruin Parks and Recreation DATE: 9/23/20
 JOB NO.: GCP&R-20-GA-04517-01 DRILLER: Carolina Drilling RIG: CME 45 LOGGED BY: J.J.

ELEV.	DESCRIPTION	DEPTH in FEET	SAMPLES					NOTES	
			NO.	TYPE	BLOWS/6"	N-VALUE	RECOV. (%)		W (%)
885	Grass; 3" Topsoil	0						Automatic Hammer Efficiency = 94.7% PL=25; LL=41; PI=16	
	Sand - some silt and clay, trace mica; loose; dark brown (Residual) (SC) - trace silt; orange-brown/red-brown		1		2-2-3-3	5	17		21.4
			2		2-2-3	5	5		
880	Clay - sandy, some silt, trace mica; tan-gray (CL)		3		N/A	N/A	24	15.5	Shelby tube sample collected from 4'-6' bgs: PL=19; LL=34; PI=15 Non-Plastic
	Sand - some gravel, trace silt and clay; firm; gray-brown (SW-SM) - some silt, trace rock fragments; loose; orange-brown/gray-brown (SM)		4		3-5-8-7	13	24	19.8	
			5		2-3-3-3	6	24	35.1	Non-Plastic
875		10							Groundwater encountered at 7 feet at the time of drilling and at 5 feet 24 hours after drilling Non-Plastic
	- trace gravel; firm		6		3-4-8	12	18	22.7	
870		15							
			7		30-50/6"	50/6"	10	13.7	
865	Partially weathered rock sampled as Sand - some silt, trace clay, some rock; very dense; gray-brown	20							
			8		10-16-24	40	18	12.4	
860	Sand - trace clay, silt, and rock fragments; dense; gray	25							
			9		50/1"	50/1"	1		
855	Partially weathered rock sampled as Sand - some silt, trace clay, some rock; very dense; gray-brown AUGER REFUSAL AT 29 FEET	30							
850		35							
845		40							

LL=Liquid Limit
 PL=Plastic Limit
 PI=Plasticity Index

Beaver Ruin Wetlands Park
Gwinnett County - Parks and Recreation

Helical Pile Design Calculations Summary (Axial and Lateral Capacity)															
Structure	Boring ID	Ground Surface Elevation ¹ (ft-msl)	Depth to Dense Soil (ft-bgs) (N ₆₀ > 30 bpf)	Factored Axial Loads ² (Kips)	Service Level Axial Loads ² (Kips)	Factored Lateral Load ² (Kips)	Service Level Lateral Load ² (Kips)	Service Level Lateral Load Converted to Compression/Tension Load ³ (kips)	Pile Type ^{4,5}	Battered Pile Design Compression/Tension Service Load ³ (Kips)	Battered Piles Minimum Installation Torque ⁶ (Ft-lb) K _t = 10 ft ⁻¹	Minimum Depth to Top Helix (ft-bgs)	Minimum Depth to Bottom Helix Plate (Vertical Pile Length) (ft-bgs)	Spin Out Pile (Plate Extended to Rock)	Estimated Helical Pile Tip Elevation ⁷ (ft-msl)
Concrete Trails/ Boardwalk	B-103	901	6	33.54	24.34	2.63	1.5	6.2	CHANCE SS175 - Square 1-¾" Shaft 14",12",10" Helices as Required (2 Battered Piles at 1h:4v (14°) @ ≥ 6 ft) Torque Rating 10,500 Ft-lb	30.5	6,108	5.5	9	Y	892
	B-104	902	18.5									4.5	11	N	891
	B-105	904	4									5.5	12	N	892
	B-106 & 106A	901	6									6.5	13	N	888
	B-108	905	8									6.5	9.5	Y	895.5
	B-109	906	13.5									8.5	15	Y	891
	B-110	896	6									4.5	11	N	885
	B-111	889	23.5									18.5	25	N	864
	B-112	892	28.5									22.5	29	N	863

Notes:

- (1) Ground Surface Elevations are interpolated from provided Topographic Plan provided by the client dated (file date) 11/22/2019 and should be considered approximate.
- (2) Loads provided by John Pyle of PermaTrak in an E-Mail Attachment dated 11/23/2020
- (3) Battered piles are designed to handle the axial and lateral Service Loads. The 1.5 kips Service Lateral Load in each pile (total of 3 kips per bent) is transferred to pile axial compression and tension load, respectively when the load is applied along the bent.
- (4) Alternative pile sizes and helix size configurations may be used by the helical pile installer provided the minimum pile ultimate (Factored) capacities design loads specified for the project are met
- (5) We recommend a minimum FOS=2 for Compression and Tension Strength of helical piles.
- (6) At least one vertical pile load test using the top large helix (14") should be performed to check the Kt factor used to calculate the ultimate helical pile ultimate (Nominal Strength) bearing capacity from the installation torque measured in the field.
- (7) Final pile tip elevation to be determined in the field based on the minimum pile installation torque rating required to achieve the ultimate capacity of the pile.

**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Contant %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)
Borehole Number	Sample ID					% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %	Moisture %	Dry (lb/cuft)								
													L.L.	P.L.			P.I.	L.I.		
B-101	1	Bag	0-2	SC-SM	13.9	27	21	6	-1.18	97.2	36.7	30.0	-	-	-	-	-	-	-	
B-101	2	Bag	2-4	SC-SM	13.7	24	17	7	-0.47	100.0	39.1	36.0	-	-	-	-	-	-	-	
B-102	2	Bag	2-4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-102	3	Bag	4-6	SM	22.3	43	27	16	-0.29	90.3	31.9	29.0	-	-	-	-	-	-	-	
B-102	4	Bag	6-8	SM	20.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-103	1	Bag	0-2	SM	19.6	35	26	9	-0.71	100.0	32.5	28.0	-	-	-	-	-	-	-	
B-103	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-103	4	Bag	6-8	-	15.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-103	5	Bag	8-10	-	12.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-104	1	Bag	0-2	-	9.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-104	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-104	4	Bag	6-8	-	13.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-105	1	Bag	0-2	CL	27.5	45	24	21	0.17	100.0	55.6	50.0	-	-	-	-	-	-	-	
B-105	2	Bag	2-4	-	8.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-105	3	Bag	4-6	-	6.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-106	1	Bag	0-2	-	15.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-106	2	Bag	2-4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-106	3	Bag	4-6	-	15.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-106	4	Bag	6-8	-	6.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-108	1	Bag	0-2	-	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-108	2	Bag	2-4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 MOISTURE (Mc)
 NP - NO PLASTICITY
 NV - NO VALUE

United Consulting

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

**Beaver Ruin Wetlands Park
SUMMARY OF SOIL DATA**

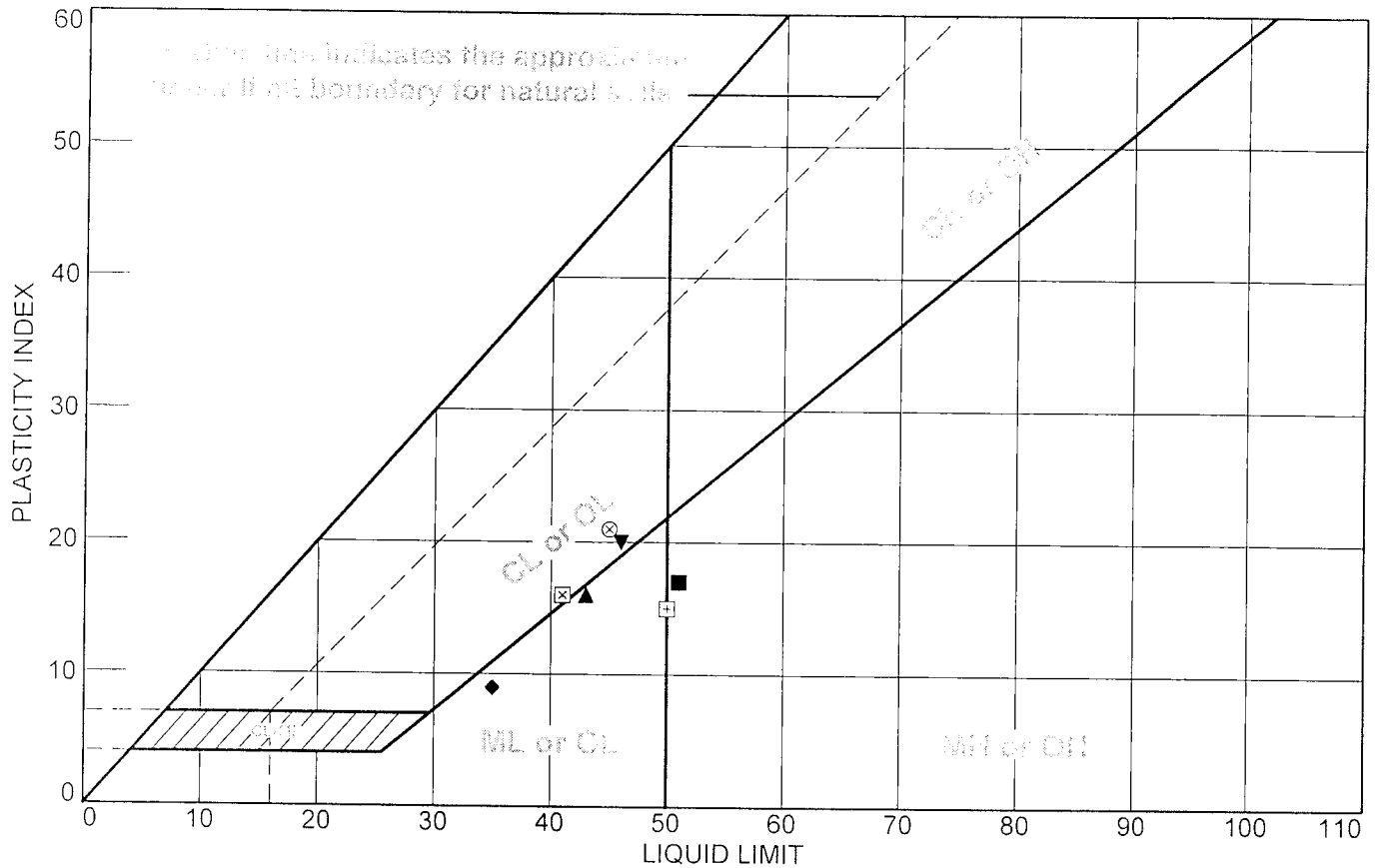
Sample Identification		Sample Type	Sample Depth	Soil Classification	As R'cd Moisture %	Atterberg Limits				Grain Size Distribution			Compaction		Gs	Organic Contant %	Unit Weight		Permeability (cm/sec)	Additional Tests Conducted (See Notes)
Borehole Number	Sample ID					% Finer No. 4 Sieve	% Finer No. 200 Sieve	% Finer .005 mm	Maximum Dry Density (lb/cuft)	Optimum Moisture %	Moisture %	Dry (lb/cuft)								
													L.L.	P.L.			P.I.	L.I.		
B-108	3	Bag	4-6	-	23.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-108	4	Bag	6-8	-	20.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-109	1	Bag	0-2	CL	23.1	46	26	20	-0.15	98.2	50.5	49	-	-	-	-	-	-	-	
B-109	2	Bag	2-3.5	-	26.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-109	3	Shelby	4-6	SM	30.3	50	35	15	-0.31	100.0	33.3	30	-	-	2.7	-	-	-	-	U
B-109	4	Bag	6-8	-	38.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-110	1	Bag	0-2	-	18.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-110	2	Bag	2-3.5	-	11.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,R,C,S
B-110	4	Bag	6-8	-	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-111	1	Bag	0-2	MH	25.9	51	34	17	-0.48	100.0	62.4	59	-	-	-	-	-	-	-	
B-111	2	Bag	2-3.5	-	19.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-111	3	Shelby	4-6	ML	30.6	49	30	19	0.03	100.0	67.7	63	-	-	-	-	-	-	-	U
B-111	4	Bag	6-8	-	36.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-112	1	Bag	0-2	-	16.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-112	1A	Bulk	0-5	SC	22.2	34	24	10	-0.18	100.0	29.7	28	-	-	-	-	-	-	-	
B-112	2	Bag	2-4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-112	3	Bag	4-6	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
B-114	1	Bag	0-2	SC	21.4	41	25	16	-0.23	100.0	43.5	38	-	-	-	-	-	-	-	
B-114	2	Bag	2-3.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	P,Re,C,S
B-114	3	Shelby	4-6	CL	15.5	34	19	15	-0.23	100.0	53.1	46	-	-	2.7	-	16.7	116.2	-	T
B-114	4	Bag	6-8	SW-SM	19.8	NV	NP	NP	NP	84.1	9.6	7	-	-	-	-	-	-	-	

ABBREVIATIONS: LIQUID LIMIT (LL)
 PLASTIC LIMIT (PL)
 PLASTICITY INDEX (PI)
 LIQUIDITY INDEX (LI)
 MOISTURE (Mc)
 NP - NO PLASTICITY
 NV - NO VALUE

United Consulting

NOTES: T = TRIAXIAL TEST
 U = UNCONFINED COMPRESSION TEST
 S = SULFATE CONTENT
 C = CHLORIDE CONTENT
 P = pH
 Re = Resistivity
 Vc = Volume /shrinkage change

LIQUID AND PLASTIC LIMITS TEST REPORT



SOIL DATA							
SOURCE	SAMPLE NO.	DEPTH	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
●	B-114	6-8 ft	19.8	NP	NV	NP	SW-SM
■	B-111	0-2 ft	25.9	34	51	17	MH
▲	B-102	4-6 ft	22.3	27	43	16	SM
◆	B-103	0-2 ft	19.6	26	35	9	SM
▼	B-109	0-2 ft	23.1	26	46	20	CL
*	B-114	13.5-15 ft	22.7	NP	NV	NP	SM
○	B-114	8-10 ft	35.1	NP	NV	NP	SM
□	B-109 (Top)	4-6 ft	30.3	35	50	15	SM
⊙	B-105	0-2 ft	27.5	24	45	21	CL
⊠	B-114	0-2 ft	21.4	25	41	16	SC

United Consulting

Norcross, Georgia

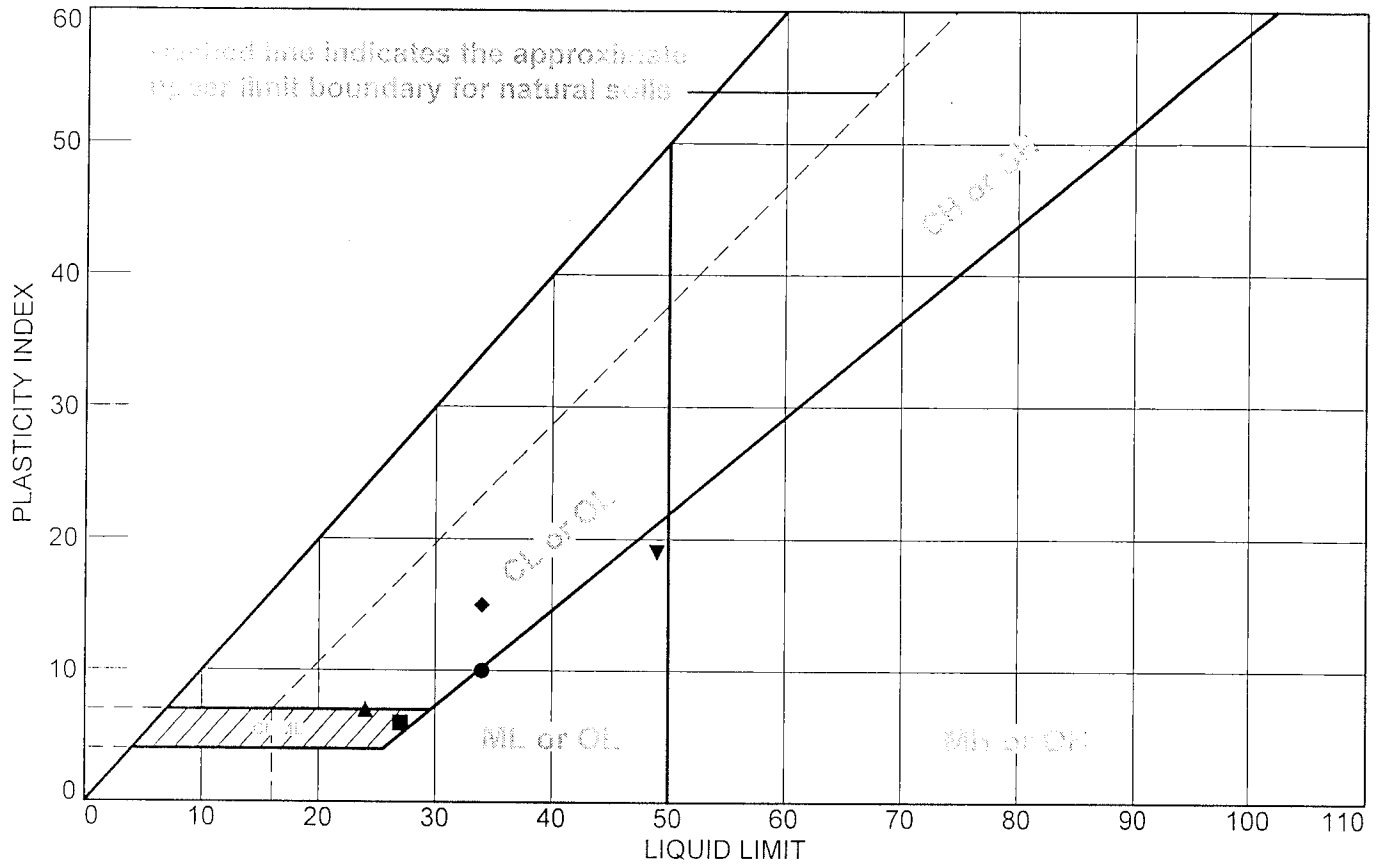
Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Run Parks and Recreation

Project No.: GCP&R20GA0451701

Figure

LIQUID AND PLASTIC LIMITS TEST REPORT



SOIL DATA

	SOURCE	SAMPLE NO.	DEPTH	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
●		B-112	0-5 ft	22.2	24	34	10	SC
■		B-101	0-2 ft	13.9	21	27	6	SC-SM
▲		B-101	2-4 ft	13.7	17	24	7	SC-SM
◆		B-114	4-6 ft	15.5	19	34	15	CL
▼		B-111 (Middle)	4-6 ft	30.6	30	49	19	ML

United Consulting

Norcross, Georgia

Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Run Parks and Recreation

Project No.: GCP&R20GA0451701

Figure

Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCP&R20GA0451701
Project Name: Beaver Ruin Parks & Recreation
Received Date: 11/12/2020

Tested By: SH
Date Tested: 11/6/2020
Reviewed by: MS
Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
B-103	6-8	32.99	155.24	139.03	15.3
B-111	6-8	33.31	167.10	131.24	36.6
B-112	0-2	32.80	164.12	145.29	16.7
B-106	4-6	32.96	155.89	139.11	15.8
B-106	0-2	37.63	183.09	163.13	15.9
B-108	4-6	32.86	207.08	174.18	23.3
B-104	6-8	33.05	154.70	140.43	13.3
B-110	0-2	32.67	203.26	176.97	18.2
B-105	6-8	32.86	161.61	144.15	15.7
B-109	2-3.5	32.89	172.24	143.45	26.0
B-104	0-2	32.97	155.72	145.19	9.4
B-106	6-8	33.1	164.69	156.18	6.9
B-108	0-2	27.16	161.10	139.67	19.0

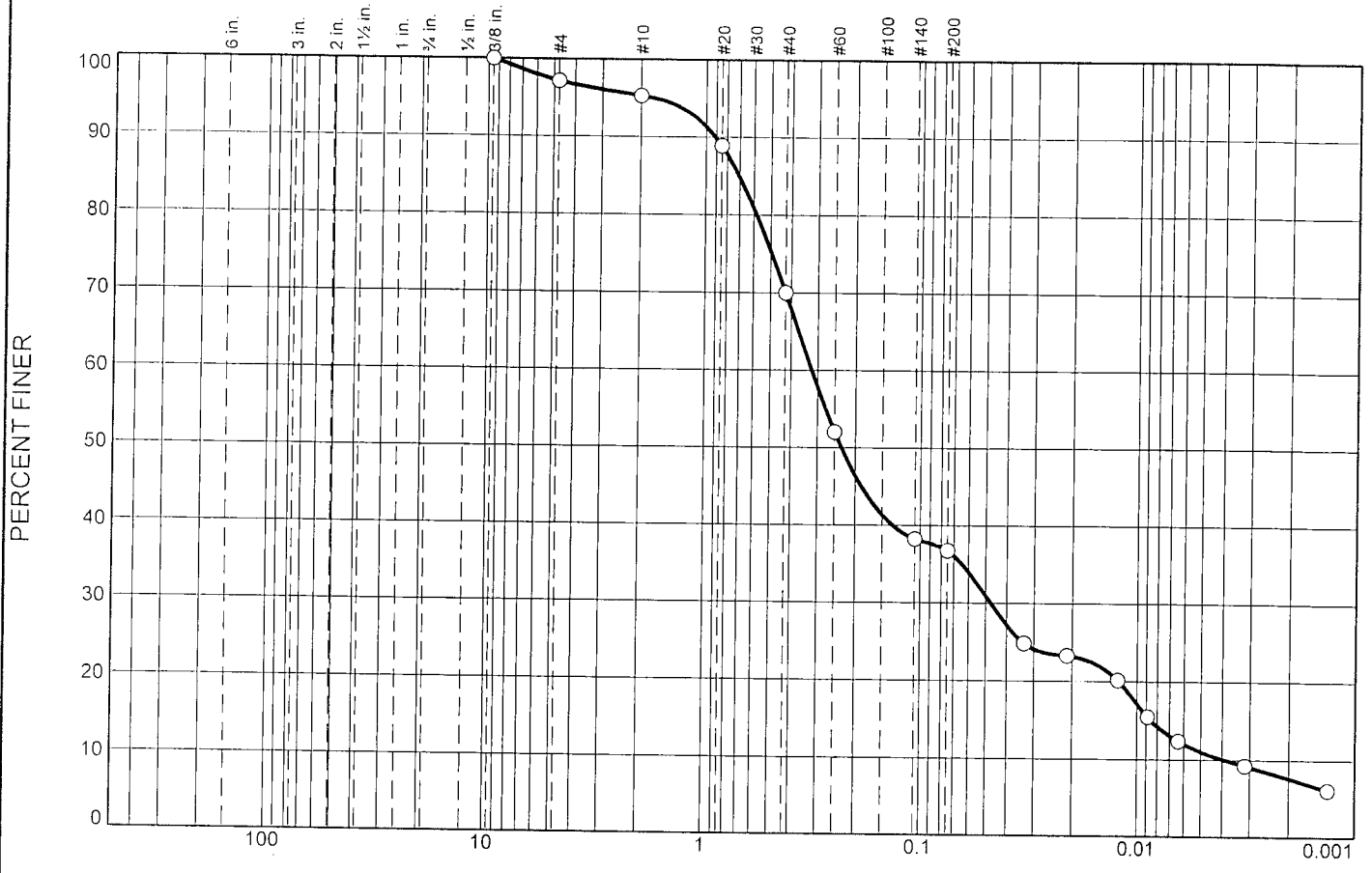
Moisture Content
ASTM D 2216 / AASHTO T-265 / UC SOP L4
DATA SHEET

Project #: GCP&R20GA0451701
Project Name: Beaver Ruin Parks & Recreation
Received Date: 11/12/2020

Tested By: SH
Date Tested: 11/6/2020
Reviewed by: MS
Revised date: 11/23/2020

BORING NO.	DEPTH (ft.)	Tare Weight (g)	Wet Sample and Tare (g)	Dry Sample and Tare (g)	Moisture Content (%)
B-103	8-10	33.15	203.53	184.83	12.3
B-105	2-4	33.35	157.41	139.95	16.4
B-105	4-6	33.18	167.50	157.03	8.5
B-114	18.5-20	33.12	190.83	171.79	13.7
B-110	6-8	37.49	202.58	169.55	25.0
B-108	6-8	37.43	167.16	144.78	20.8
B-109	6-8	33.27	166.01	129.06	38.6
B-111	2-3.5	33.1	175.84	152.13	19.9
B-102	6-8	32.99	178.65	153.64	20.7
B-114	23.5-25	27.11	170.42	154.56	12.4
B-112	4-6	37.58	216.11	179.13	26.1
B-110	2-3.5	22.99	209.05	189.23	11.9

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	2.8	60.5	25.7	11.0

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.375	100.0		
#4	97.2		
#10	95.3		
#20	88.9		
#40	70.0		
#60	52.0		
#140	38.2		
#200	36.7		

* (no specification provided)

Material Description

Sand, some silt and clay, trace silt, brown

Atterberg Limits

PL= 21 LL= 27 PI= 6

Coefficients

D₉₀= 0.9084 D₈₅= 0.7045 D₆₀= 0.3201
D₅₀= 0.2327 D₃₀= 0.0475 D₁₅= 0.0086
D₁₀= 0.0039 C_u= 81.10 C_c= 1.78

Classification

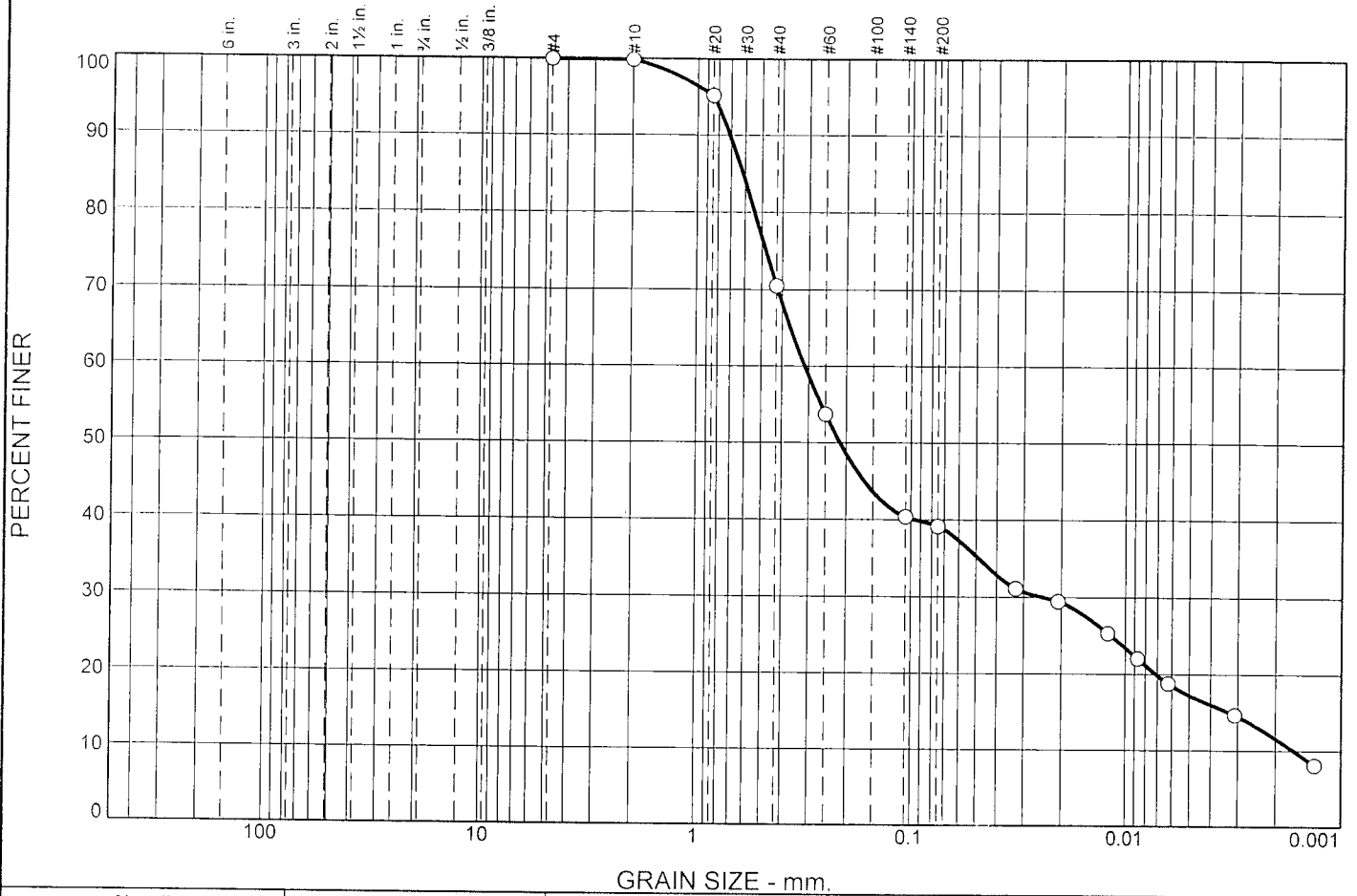
USCS= SC-SM AASHTO= A-4(0)

Remarks

Sample Number: B-101 Depth: 0-2 ft

Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	60.9	21.9	17.2

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	95.2		
#40	70.4		
#60	53.7		
#140	40.3		
#200	39.1		

* (no specification provided)

Material Description

Sand, some silt and clay, dark brown

Atterberg Limits

PL= 17 LL= 24 PI= 7

Coefficients

D₉₀= 0.7082 D₈₅= 0.6156 D₆₀= 0.3130
D₅₀= 0.2143 D₃₀= 0.0245 D₁₅= 0.0033
D₁₀= 0.0017 C_u= 189.13 C_c= 1.15

Classification

USCS= SC-SM AASHTO= A-4(0)

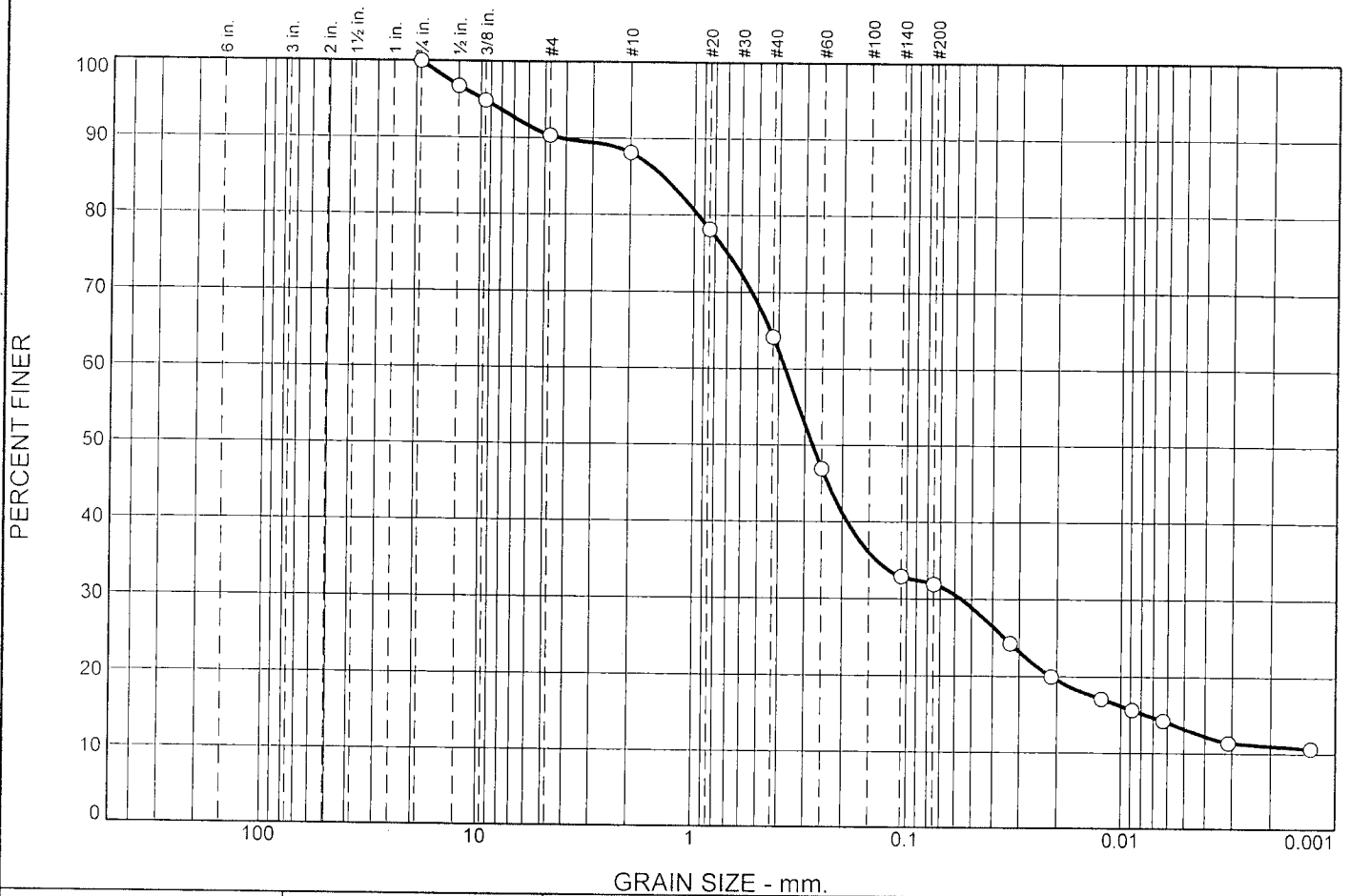
Remarks

Sample Number: B-101 Depth: 2-4 ft

Date: 11/6/2020

<p style="font-size: 1.2em; margin: 0;">United Consulting</p> <p style="margin: 0;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Ruin Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p>
<p>Figure</p>	

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	9.7	58.4	18.7	13.2

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.75	100.0		
0.5	96.7		
0.375	94.9		
#4	90.3		
#10	88.1		
#20	78.2		
#40	64.1		
#60	46.9		
#140	32.9		
#200	31.9		

Material Description

Sand, some silt and clay, trace gravel, brown and tan

Atterberg Limits

PL= 27 LL= 43 PI= 16

Coefficients

D₉₀= 4.3019 D₈₅= 1.4034 D₆₀= 0.3722
 D₅₀= 0.2764 D₃₀= 0.0562 D₁₅= 0.0076
 D₁₀= C_u= C_c=

Classification

USCS= SM AASHTO= A-2-7(1)

Remarks

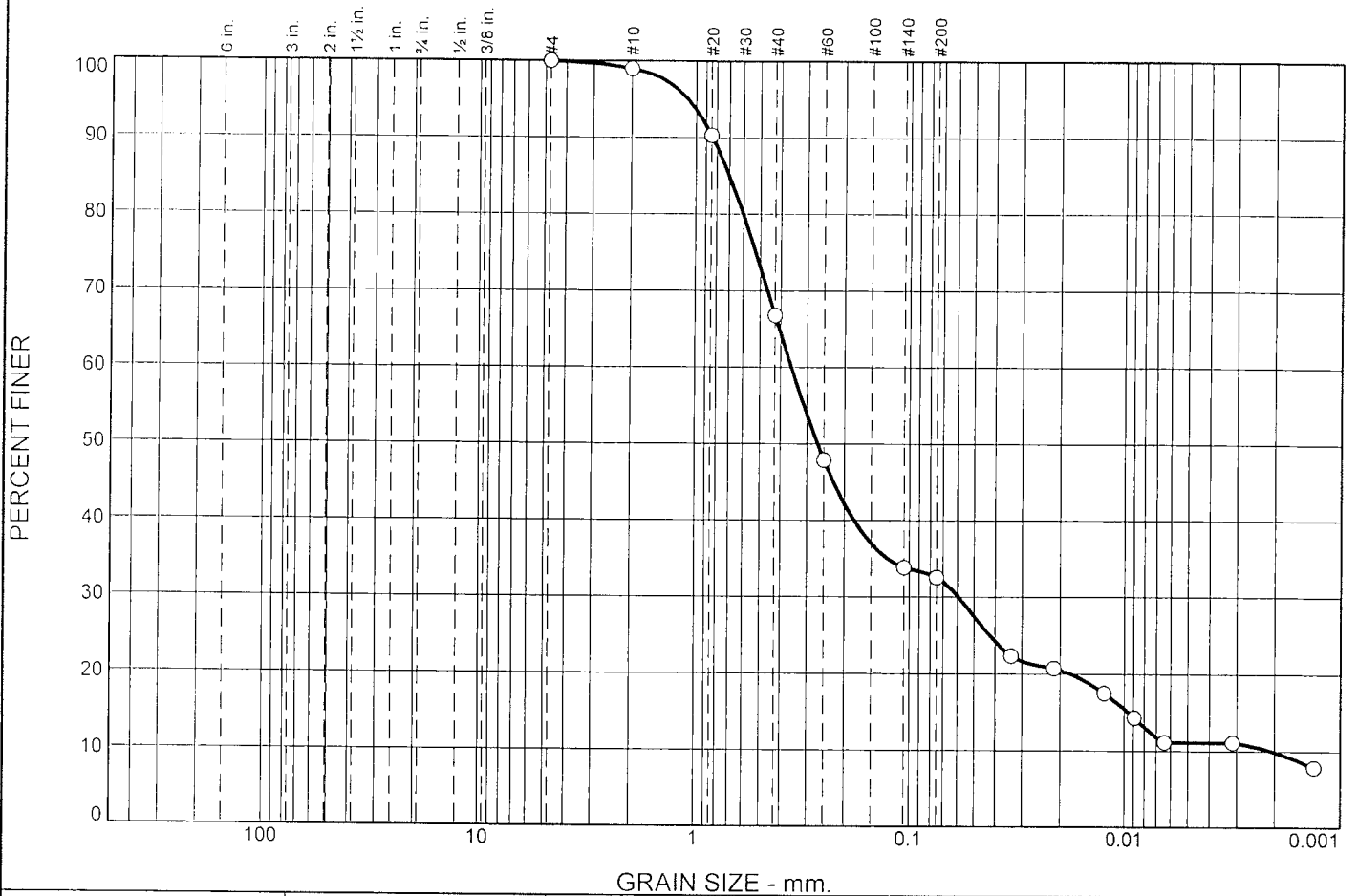
* (no specification provided)

Sample Number: B-102 Depth: 4-6 ft

Date: 11/6/2020

<p style="font-size: 1.2em; margin: 0;">United Consulting</p> <p style="margin: 0;">Norcross, Georgia</p>	<p style="margin: 0;">Client: GWINNETT CO PARKS & RECREATION</p> <p style="margin: 0;">Project: Beaver Ruin Parks and Recreation</p> <p style="margin: 0;">Project No: GCP&R20GA0451701</p> <p style="text-align: right; margin: 0;">Figure</p>
--	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	67.5	21.4	11.1

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.0		
#20	90.3		
#40	66.8		
#60	47.9		
#140	33.8		
#200	32.5		

Material Description

Sand, some silt and clay, dark brown

Atterberg Limits

PL= 26 LL= 35 PI= 9

Coefficients

D₉₀= 0.8381 D₈₅= 0.7008 D₆₀= 0.3563
 D₅₀= 0.2679 D₃₀= 0.0593 D₁₅= 0.0096
 D₁₀= 0.0021 C_u= 171.35 C_c= 4.75

Classification

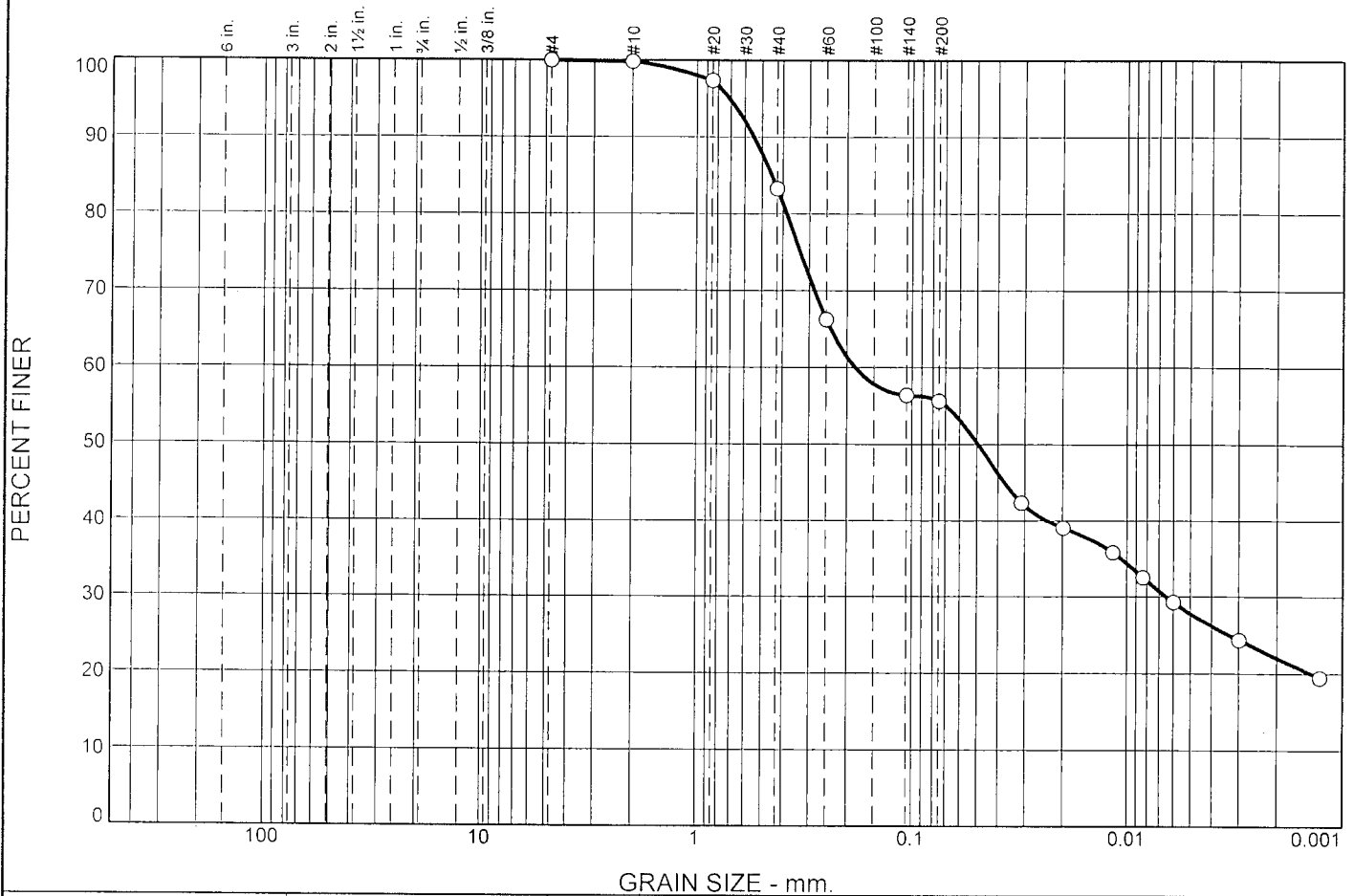
USCS= SM AASHTO= A-2-4(0)

Remarks

* (no specification provided)

Sample Number: B-103 Depth: 0-2 ft Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	44.4	27.9	27.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.8		
#20	97.4		
#40	83.3		
#60	66.2		
#140	56.4		
#200	55.6		

* (no specification provided)

Material Description

Clay-sandy, some silt, dark brown

Atterberg Limits

PL= 24 LL= 45 PI= 21

Coefficients

D₉₀= 0.5454 D₈₅= 0.4500 D₆₀= 0.1834
D₅₀= 0.0494 D₃₀= 0.0065 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= CL AASHTO= A-7-6(9)

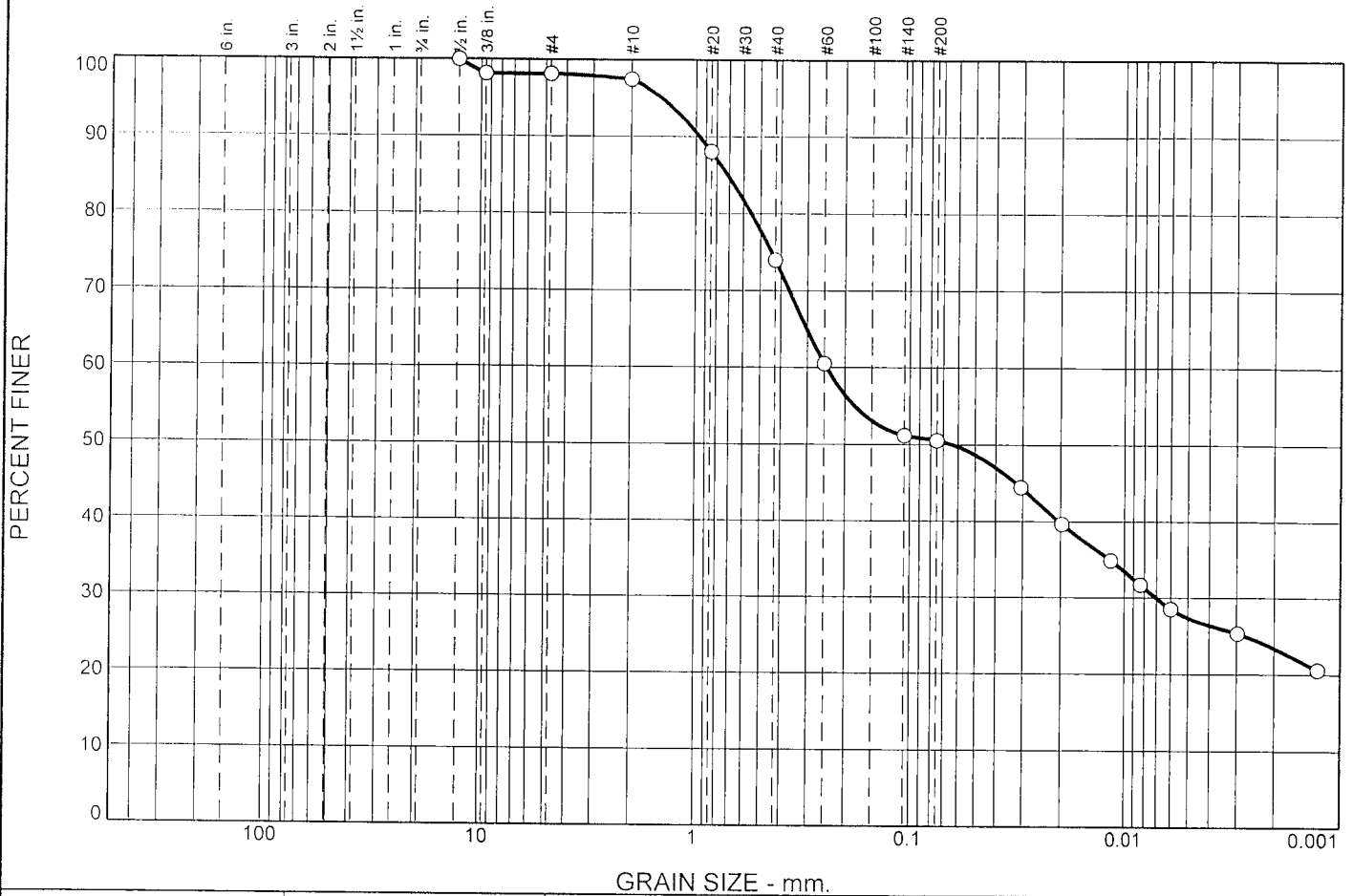
Remarks

Sample Number: B-105 Depth: 0-2 ft

Date: 11/6/2020

<p style="font-size: 1.2em; font-weight: bold; margin: 0;">United Consulting</p> <p style="font-size: 1.2em; font-weight: bold; margin: 0;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Ruin Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p> <p style="text-align: right;">Figure</p>
---	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt
0.0	1.8	47.7	23.2
			% Clay
			27.3

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.5	100.0		
0.375	98.2		
#4	98.2		
#10	97.5		
#20	88.1		
#40	73.9		
#60	60.5		
#140	51.2		
#200	50.5		

Material Description

Clay-sandy, some silt, trace gravel, dark tan

Atterberg Limits

PL= 26 LL= 46 PI= 20

Coefficients

D₉₀= 0.9628 D₈₅= 0.7101 D₆₀= 0.2444
D₅₀= 0.0638 D₃₀= 0.0071 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= CL AASHTO= A-7-6(7)

Remarks

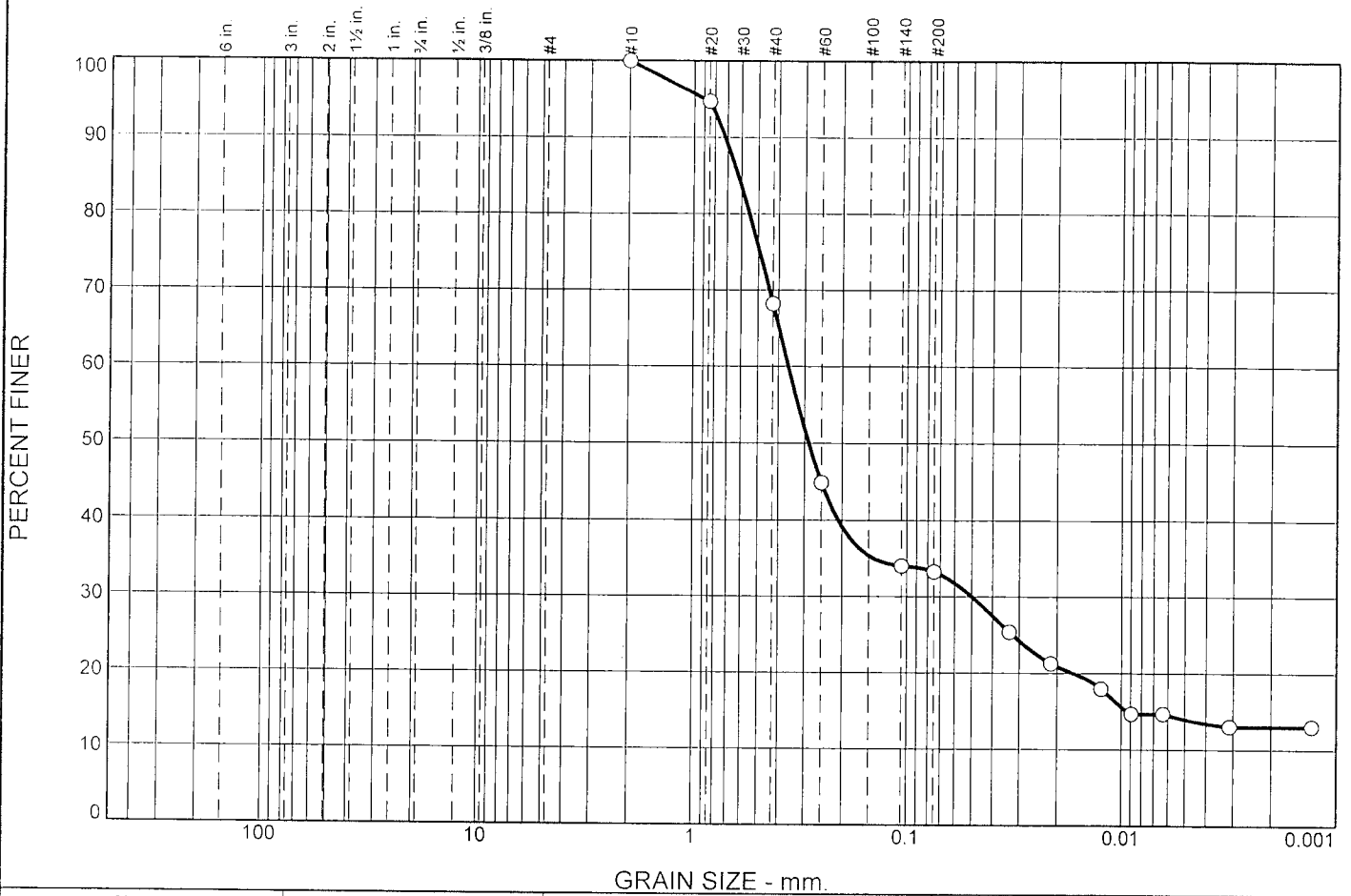
* (no specification provided)

Sample Number: B-109 Depth: 0-2 ft

Date: 11/6/2020

<p style="font-size: 1.2em; font-weight: bold; margin: 0;">United Consulting</p> <p style="font-size: 1.2em; font-weight: bold; margin: 0;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Run Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p> <p style="text-align: right;">Figure</p>
---	--

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	66.7	19.3	14.0

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	94.7		
#40	68.2		
#60	44.9		
#140	34.0		
#200	33.3		

Material Description

Sand, some silt and clay, dark tan

Atterberg Limits

PL= 35 LL= 50 PI= 15

Coefficients

D₉₀= 0.7172 D₈₅= 0.6229 D₆₀= 0.3586
 D₅₀= 0.2870 D₃₀= 0.0499 D₁₅= 0.0094
 D₁₀= C_u= C_c=

Classification

USCS= SM AASHTO= A-2-7(1)

Remarks

* (no specification provided)

Sample Number: B-109 (Top)

Depth: 4-6 ft

Date: 11/6/2020

United Consulting

Norcross, Georgia

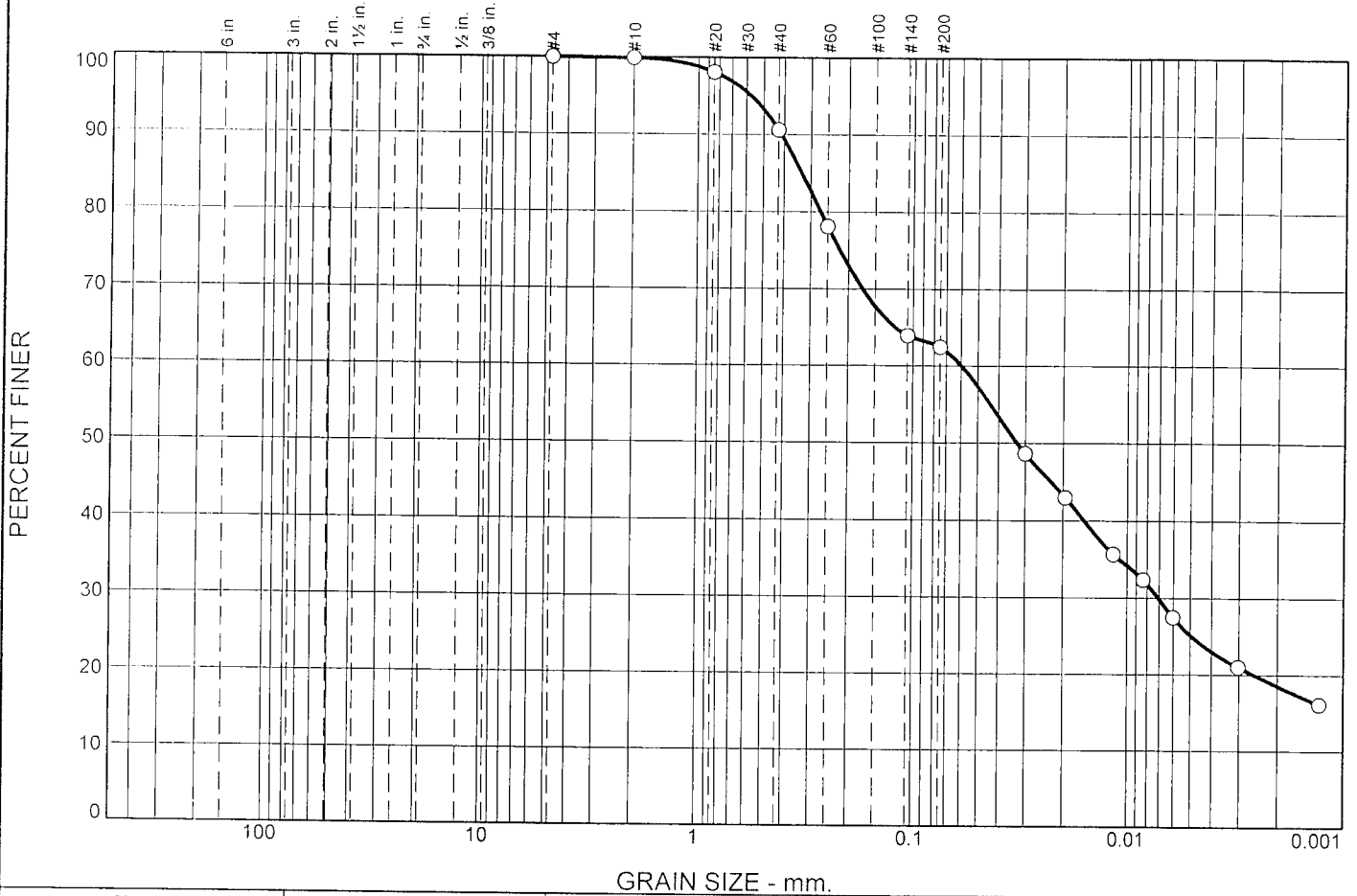
Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Ruin Parks and Recreation

Project No: GCP&R20GA0451701

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	37.6	37.3	25.1

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	98.1		
#40	90.6		
#60	78.1		
#140	63.9		
#200	62.4		

* (no specification provided)

Material Description

Silt-sandy, some clay, red brown

Atterberg Limits

PL= 34 LL= 51 PI= 17

Coefficients

D₉₀= 0.4122 D₈₅= 0.3300 D₆₀= 0.0596
D₅₀= 0.0328 D₃₀= 0.0071 D₁₅=
D₁₀= C_u= C_c=

Classification

USCS= MH AASHTO= A-7-5(10)

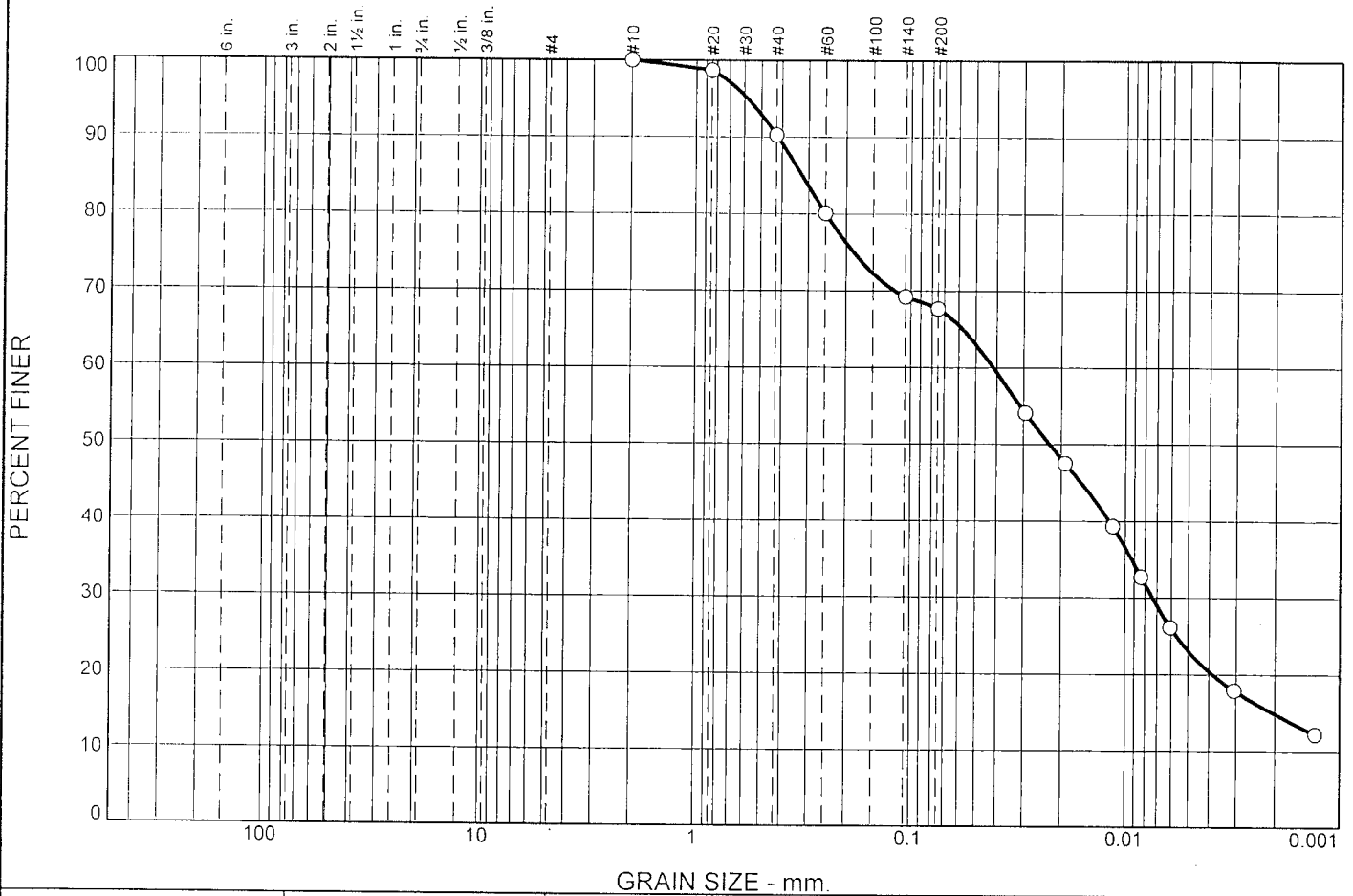
Remarks

Sample Number: B-111 Depth: 0-2 ft

Date: 11/6/2020

<p style="font-size: 1.2em; font-weight: bold;">United Consulting</p> <p style="font-size: 1.2em; font-weight: bold;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Ruin Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p> <p style="text-align: right;">Figure</p>
---	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt
0.0	0.0	32.3	44.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100.0		
#20	98.7		
#40	90.3		
#60	80.1		
#140	69.2		
#200	67.7		

Material Description

Silt, some sand and clay, dark brown

Atterberg Limits

PL= 30 LL= 49 PI= 19

Coefficients

D₉₀= 0.4183 D₈₅= 0.3219 D₆₀= 0.0415
 D₅₀= 0.0227 D₃₀= 0.0074 D₁₅= 0.0021
 D₁₀= C_u= C_c=

Classification

USCS= ML AASHTO= A-7-5(13)

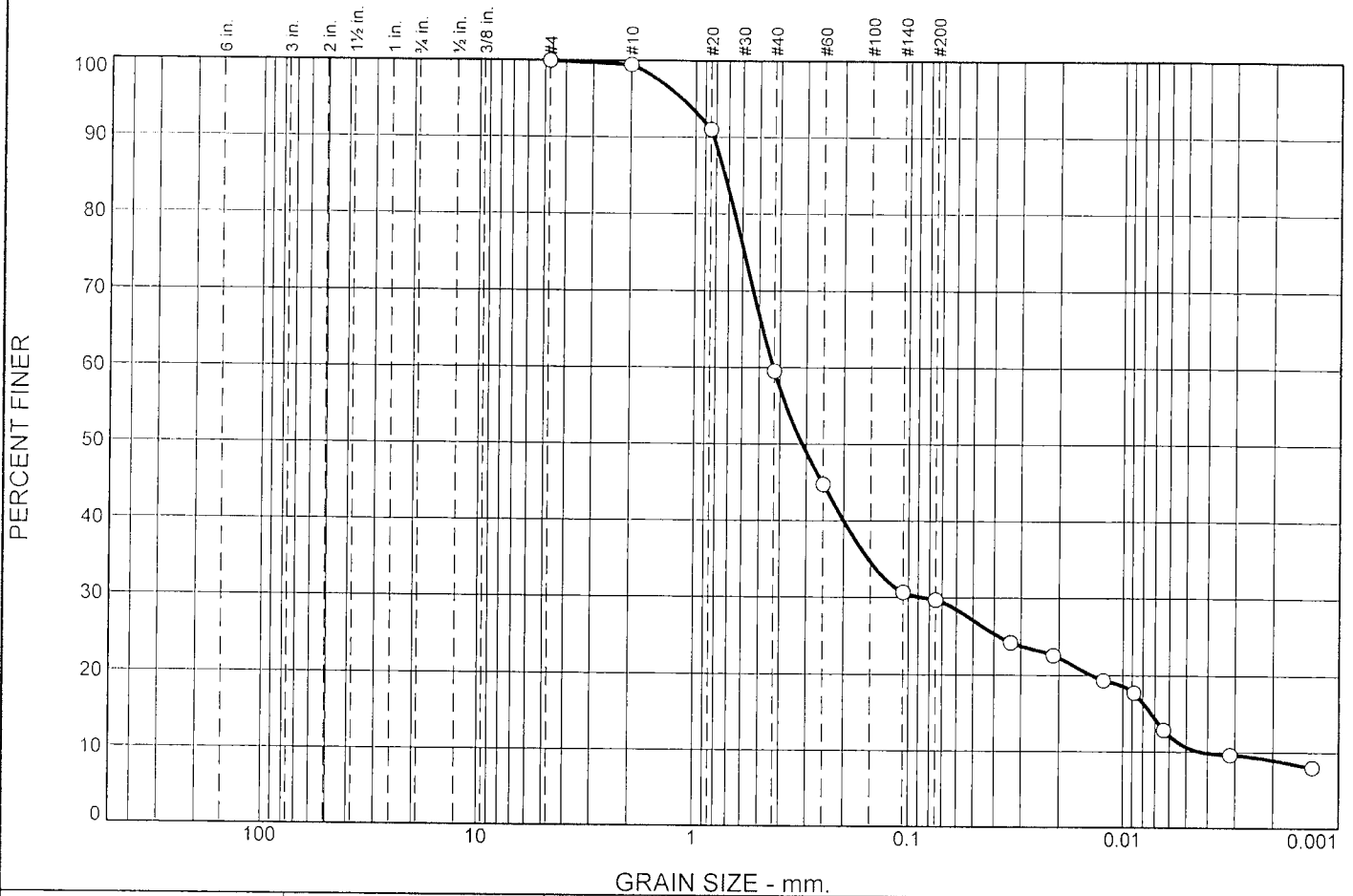
Remarks

* (no specification provided)

Sample Number: B-111 (Middle) Depth: 4-6 ft Date: 11/6/2020

<p style="font-size: 1.2em; font-weight: bold;">United Consulting</p> <p style="font-size: 1.2em; font-weight: bold;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Ruin Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p> <p style="text-align: right;">Figure</p>
---	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	70.3	19.1	10.6

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.5		
#20	91.1		
#40	59.6		
#60	44.7		
#140	30.6		
#200	29.7		

Material Description

Sand, some silt, trace clay, brown

Atterberg Limits

PL= 24 LL= 34 PI= 10

Coefficients

D₉₀= 0.8243 D₈₅= 0.7281 D₆₀= 0.4298
 D₅₀= 0.3142 D₃₀= 0.0867 D₁₅= 0.0073
 D₁₀= 0.0044 C_u= 98.36 C_c= 4.01

Classification

USCS= SC AASHTO= A-2-4(0)

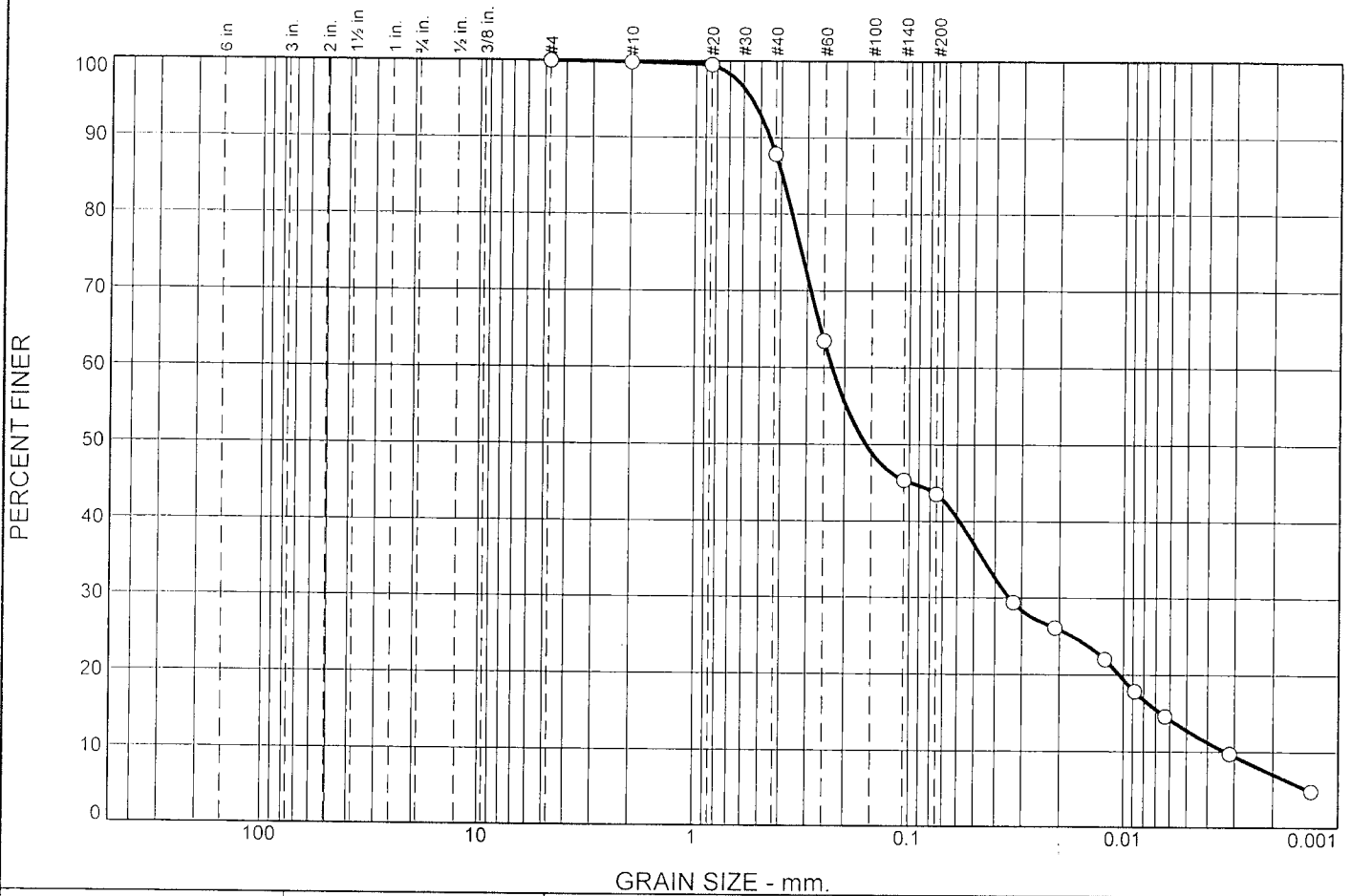
Remarks

* (no specification provided)

Sample Number: B-112 Depth: 0-5 ft

Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	56.5	30.8	12.7

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.8		
#20	99.5		
#40	87.8		
#60	63.4		
#140	45.3		
#200	43.5		

* (no specification provided)

Material Description

Sand, some silt and clay, dark brown

Atterberg Limits

PL= 25 LL= 41 PI= 16

Coefficients

D₉₀= 0.4524 D₈₅= 0.3958 D₆₀= 0.2292
D₅₀= 0.1593 D₃₀= 0.0344 D₁₅= 0.0066
D₁₀= 0.0033 C_u= 69.01 C_c= 1.55

Classification

USCS= SC AASHTO= A-7-6(4)

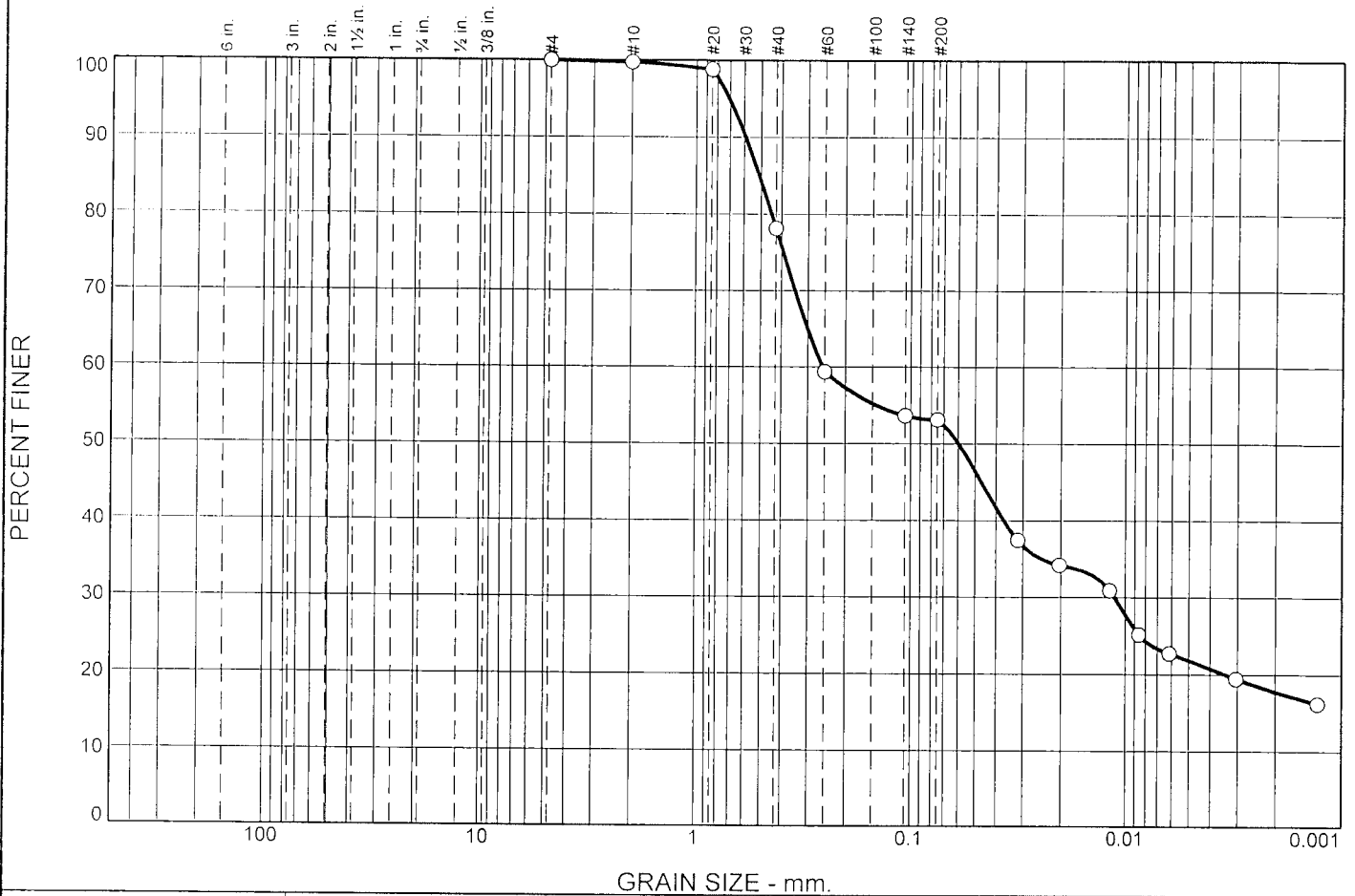
Remarks

Sample Number: B-114 Depth: 0-2 ft

Date: 11/6/2020

<p style="font-size: 1.2em; font-weight: bold; margin: 0;">United Consulting</p> <p style="font-size: 1.2em; font-weight: bold; margin: 0;">Norcross, Georgia</p>	<p>Client: GWINNETT CO PARKS & RECREATION</p> <p>Project: Beaver Ruin Parks and Recreation</p> <p>Project No: GCP&R20GA0451701</p> <p style="text-align: right;">Figure</p>
---	---

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	46.9	31.3	21.8

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.7		
#20	98.8		
#40	78.1		
#60	59.4		
#140	53.6		
#200	53.1		

Material Description

Clay-sandy, some silt, tan and gray

Atterberg Limits

PL= 19 LL= 34 PI= 15

Coefficients

D₉₀= 0.5909 D₈₅= 0.5099 D₆₀= 0.2560
D₅₀= 0.0596 D₃₀= 0.0113 D₁₅=
D₁₀= C_u= C_c=

Classification

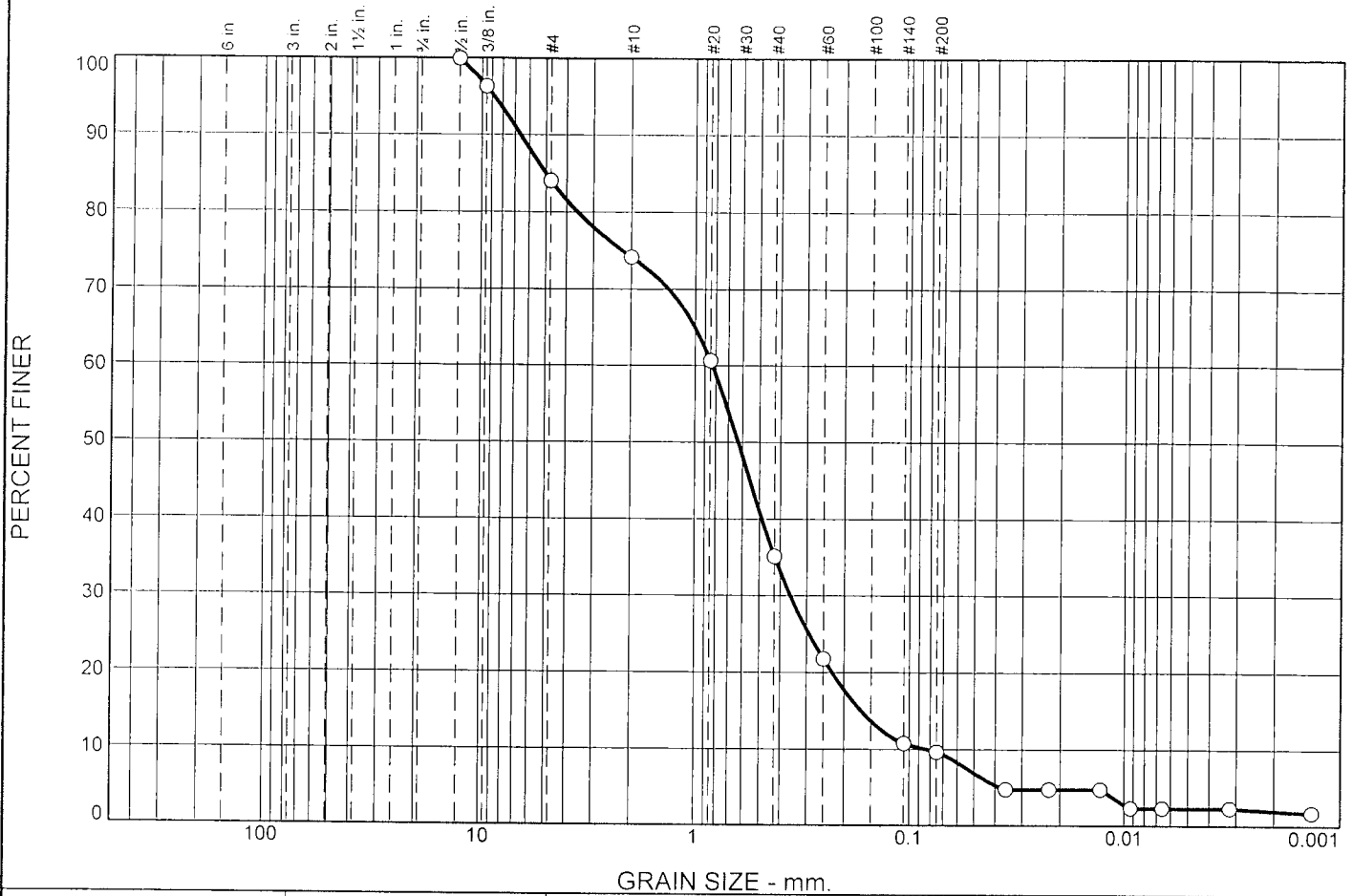
USCS= CL AASHTO= A-6(5)

Remarks

* (no specification provided)

Sample Number: B-114 Depth: 4-6 ft Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	15.9	74.5	7.3	2.3

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
0.5	100.0		
0.375	96.3		
#4	84.1		
#10	74.1		
#20	60.7		
#40	35.1		
#60	21.8		
#140	10.7		
#200	9.6		

Material Description

Sand, some gravel, trace silt and clay, tan

Atterberg Limits

PL= NP LL= NV PI= NP

Coefficients

D₉₀= 6.6005 D₈₅= 5.0148 D₆₀= 0.8318
 D₅₀= 0.6295 D₃₀= 0.3587 D₁₅= 0.1670
 D₁₀= 0.0836 C_u= 9.95 C_c= 1.85

Classification

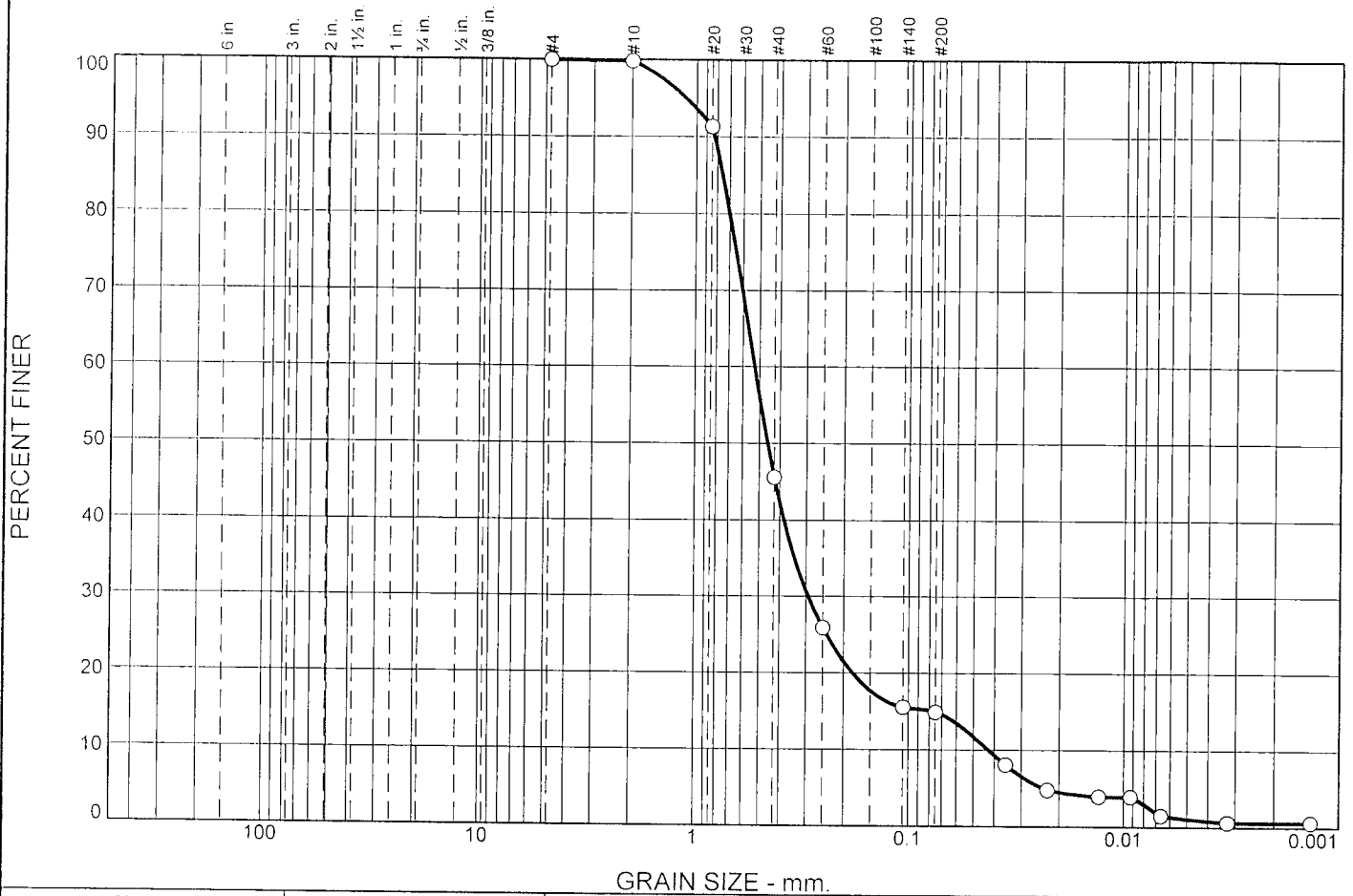
USCS= SW-SM AASHTO= A-1-b

Remarks

* (no specification provided)

Sample Number: B-114 Depth: 6-8 ft Date: 11/6/2020

Particle Size Distribution Report



% +3"	% Gravel	% Sand	% Silt	% Clay
0.0	0.0	85.1	13.8	1.1

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.8		
#20	91.3		
#40	45.5		
#60	25.9		
#140	15.5		
#200	14.9		

* (no specification provided)

Material Description

Sand, some silt, trace clay, green tan

Atterberg Limits

PL= NP LL= NV PI= NP

Coefficients

D₉₀= 0.8268 D₈₅= 0.7554 D₆₀= 0.5283
D₅₀= 0.4570 D₃₀= 0.2933 D₁₅= 0.0775
D₁₀= 0.0427 C_u= 12.38 C_c= 3.82

Classification

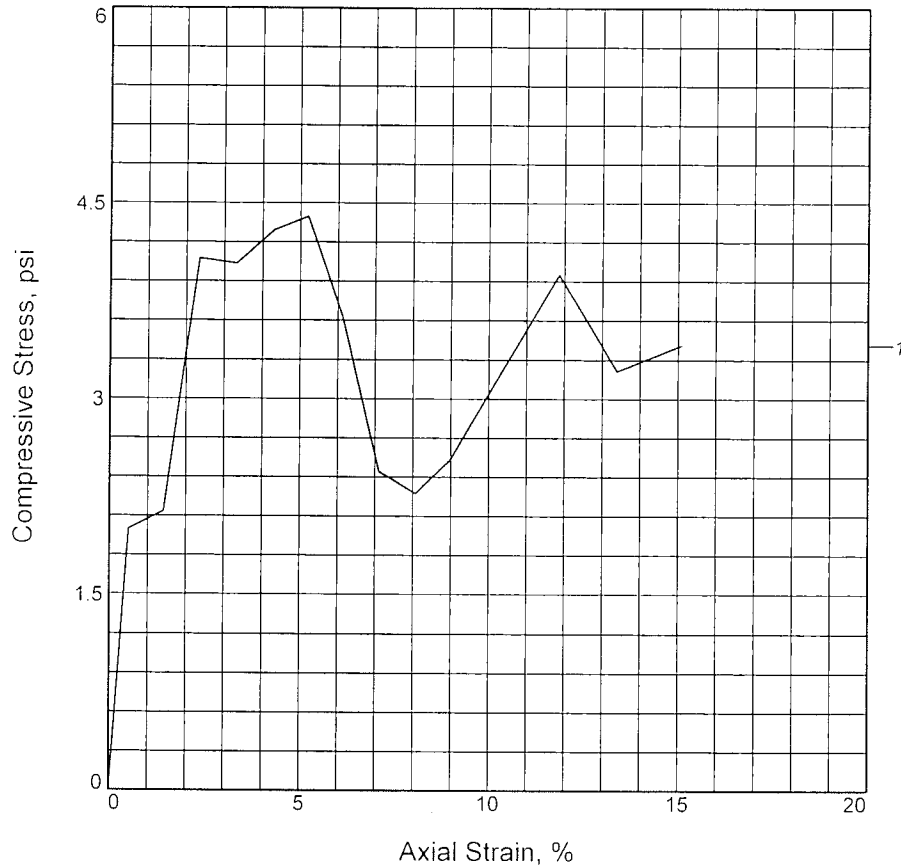
USCS= SM AASHTO= A-1-b

Remarks

Sample Number: B-114 Depth: 8-10 ft

Date: 11/6/2020

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	4.40			
Undrained shear strength, psi	2.20			
Failure strain, %	5.2			
Strain rate, in./min.	0.050			
Water content, %	32.2			
Wet density, pcf	119.1			
Dry density, pcf	90.0			
Saturation, %	99.8			
Void ratio	0.8722			
Specimen diameter, in.	2.87			
Specimen height, in.	5.60			
Height/diameter ratio	1.95			

Description: Sand, some silt and clay, dark tan

LL = 50 **PL = 35** **PI = 15** **GS = 2.7** **Type: Undisturbed**

Project No.: GWINNETT CO PARKS & RECREATION

Date Sampled: 11/6/2020

Remarks:

Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Ruin Parks and Recreation

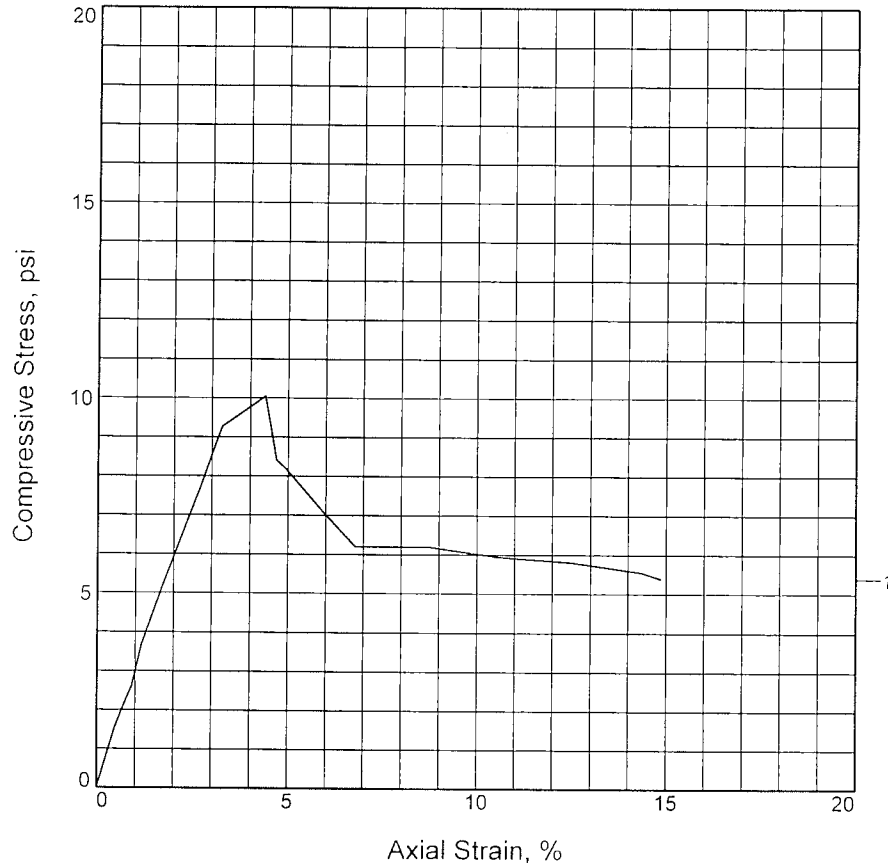
Sample Number: B-109 (Top) **Depth:** 4-6 ft

UNCONFINED COMPRESSION TEST

United Consulting
Norcross, Georgia

Figure _____

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psi	10.05			
Undrained shear strength, psi	5.02			
Failure strain, %	4.4			
Strain rate, in./min.	0.050			
Water content, %	26.1			
Wet density, pcf	128.0			
Dry density, pcf	101.5			
Saturation, %	106.7			
Void ratio	0.6605			
Specimen diameter, in.	2.87			
Specimen height, in.	5.60			
Height/diameter ratio	1.95			

Description: Silt, some sand and clay, dark brown

LL = 49 PL = 30 PI = 19 GS = 2.7 Type: Undisturbed

Project No.: GCP&R206.M0451701

Date Sampled: 11/6/2020

Remarks:

Client: GWINNETT CO PARKS & RECREATION

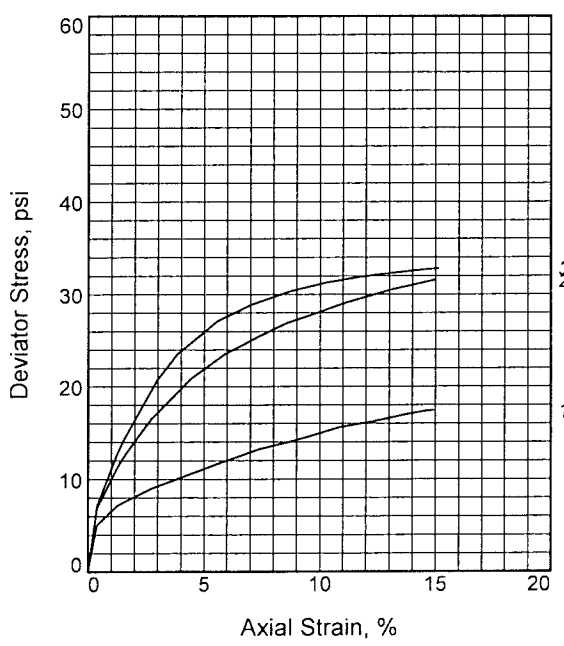
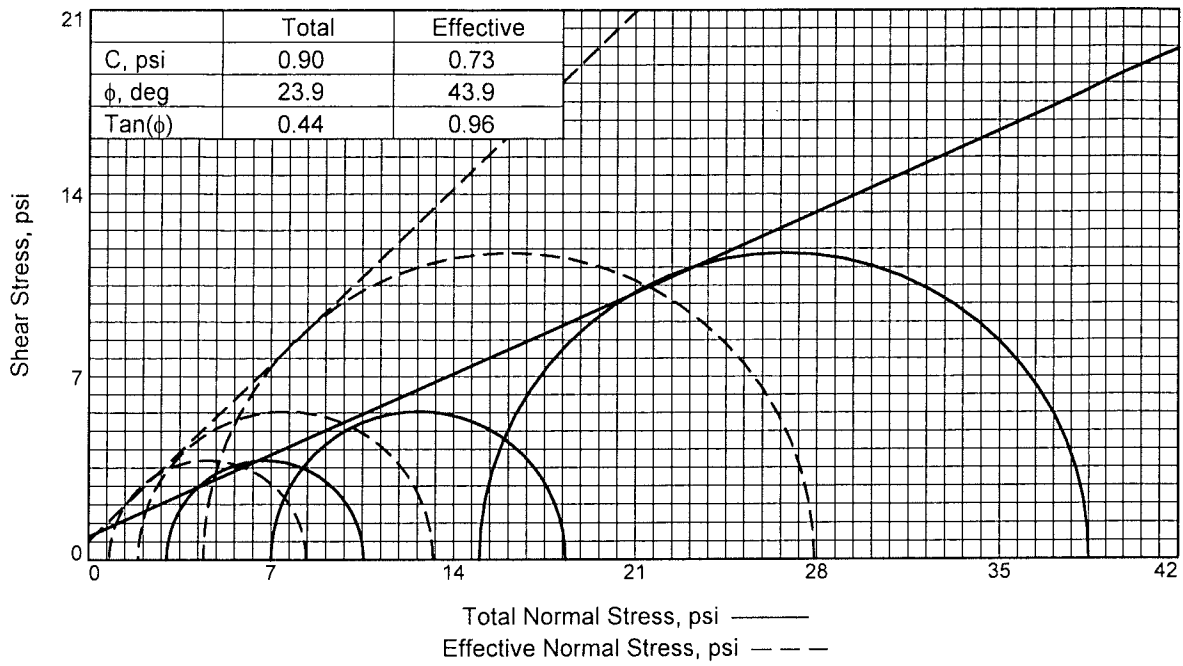
Project: Beaver Ruin Parks and Recreation

Sample Number: B-111 (Middle) **Depth:** 4-6 ft

UNCONFINED COMPRESSION TEST

United Consulting
Norcross, Georgia

Figure _____



Sample No.		1	2	3
Initial	Water Content, %	19.7	17.9	16.8
	Dry Density, pcf	104.0	109.7	112.6
	Saturation, %	85.6	90.0	91.0
	Void Ratio	0.6211	0.5367	0.4974
	Diameter, in.	2.87	2.87	2.87
	Height, in.	5.60	5.60	5.60
At Test	Water Content, %	20.5	17.3	16.7
	Dry Density, pcf	108.6	114.8	116.2
	Saturation, %	100.0	100.0	100.0
	Void Ratio	0.5523	0.4682	0.4504
	Diameter, in.	2.83	2.83	2.84
	Height, in.	5.52	5.52	5.54
Strain rate, in./min.		0.008	0.008	0.008
Back Pressure, psi		75.0	70.0	85.0
Cell Pressure, psi		78.0	77.0	100.0
Fail. Stress, psi		7.6	11.3	23.5
Total Pore Pr., psi		77.2	75.1	95.6
Ult. Stress, psi		17.4	31.5	32.8
Total Pore Pr., psi		73.1	65.2	89.9
$\bar{\sigma}_1$ Failure, psi		8.4	13.2	27.9
$\bar{\sigma}_3$ Failure, psi		0.8	1.9	4.4

Type of Test:
CU with Pore Pressures

Sample Type: Undisturbed

Description: Clay-sandy, some silt, tan and gray

LL= 34 PL= 19 PI= 15

Specific Gravity= 2.7

Remarks:

Figure _____

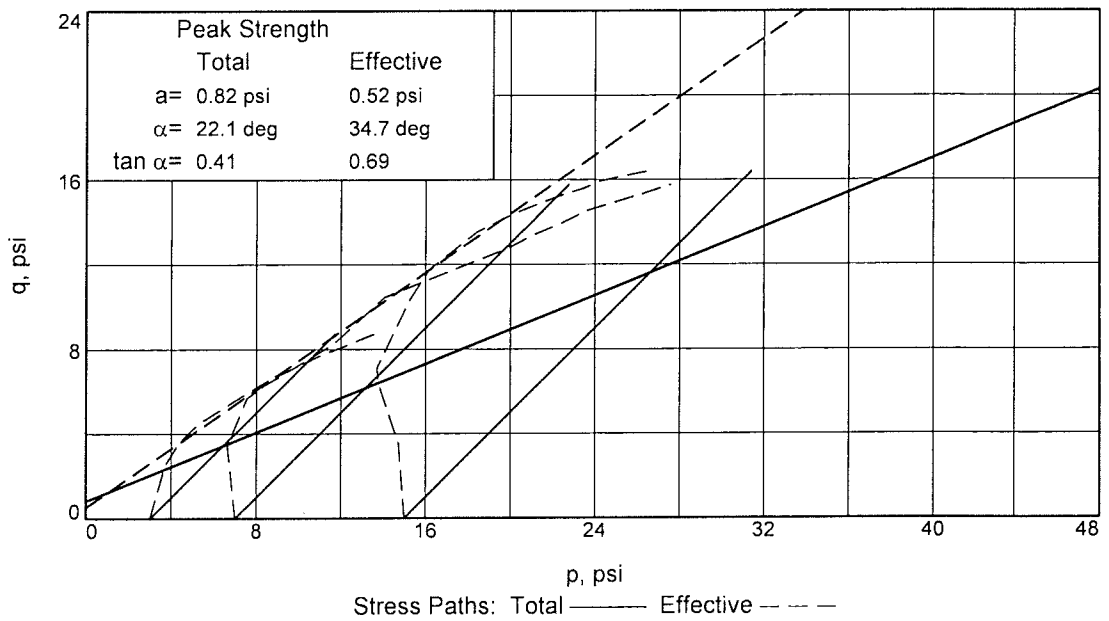
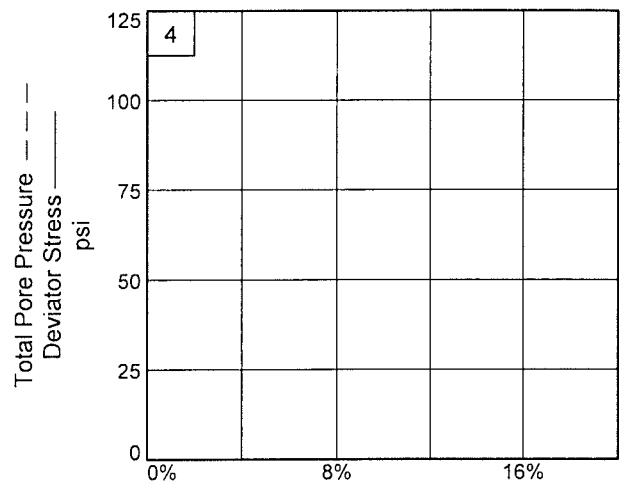
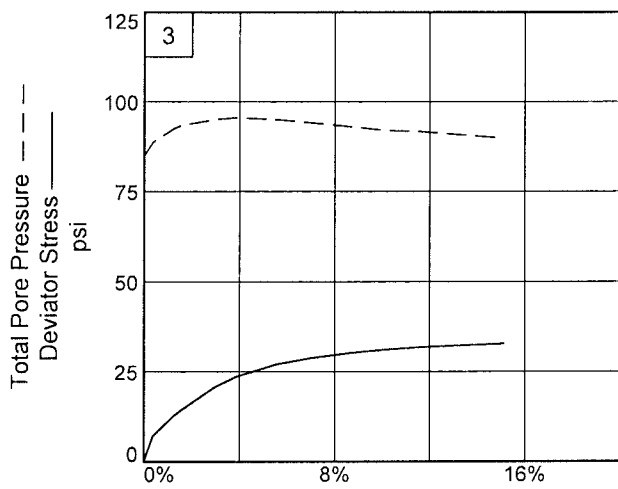
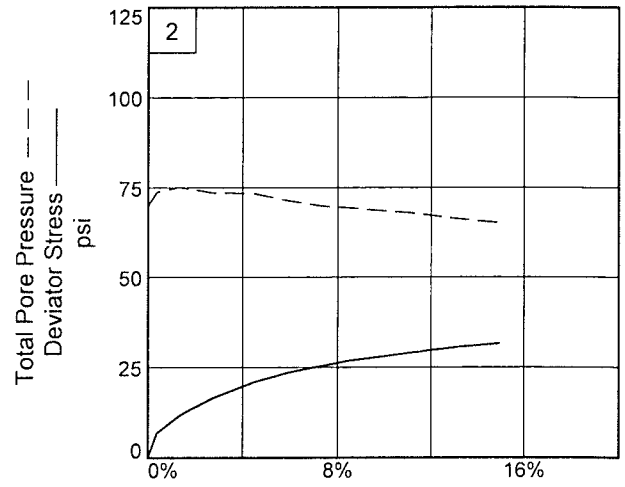
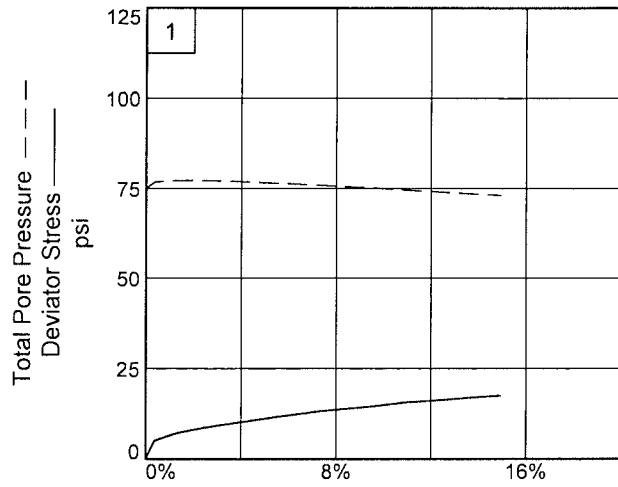
Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Ruin Parks and Recreation

Sample Number: B-114 **Depth:** 4-6 ft

Proj. No.: GCP&R20GA0451701 **Date Sampled:** 11/6/2020

TRIAXIAL SHEAR TEST REPORT
United Consulting
Norcross, Georgia



Client: GWINNETT CO PARKS & RECREATION

Project: Beaver Ruin Parks and Recreation

Depth: 4-6 ft **Sample Number:** B-114

Project No.: GCP&R20GA0451701

Figure _____

United Consulting



ANALYTICAL ENVIRONMENTAL SERVICES, INC.

December 01, 2020

Mahvand Saleki
United Consulting Group Inc.

625 Holcomb Bridge Rd
Norcross GA 30071

RE: Beaver Ruin Parks and Recreation

Dear Mahvand Saleki:

Order No: 2011M92

Analytical Environmental Services, Inc. received 8 samples on 11/19/2020 2:35:00 PM for the analyses presented in following report.

“No problems were encountered during the analyses except as noted in the Case Narrative or by qualifiers in the report or QC Summary. Additionally, all results for the associated Quality Control samples were within EPA and/or AES established limits.

AES’s accreditations are as follows:

-NELAP/State of Florida Laboratory ID E87582 for analysis of Non-Potable Water, Solid & Chemical Materials, Air & Emissions Volatile Organics, and Drinking Water Microbiology & Metals, effective 07/01/20-06/30/21.

State of Georgia, Department of Natural Resources ID #800 for analysis of Drinking Water Metals, effective through 06/30/21 and Total Coliforms/ E. coli, effective 04/20/20-04/24/23.

-AIHA-LAP, LLC Laboratory ID: 100671 for Industrial Hygiene samples (Metals and PCM Asbestos), Environmental Lead (Paint, Soil, Dust Wipes, Air), and Environmental Microbiology (Fungal) Direct Examination, effective until 11/01/21.

These results relate only to the items tested as received. This report may only be reproduced in full.

If you have any questions regarding these test results, please feel free to call.

Sincerely,

Ioana Pacurar
Project Manager

SAMPLE CHAIN-OF-CUSTODY RECORD

2011 M92

UNITED CONSULTING
 625 Holcomb Bridge
 NORCROSS, GEORGIA 30071
 (770) 209-0029 FAX (770) 582-2895
 www.uniteaconsulting.com

PROJECT NAME: Beaver Ruin Parks And Recreation		Project#: GCP&R20GA0451701				ANALYSES (indicate target list)												
TAT or DUE DATE: 11/30/2020		CONTACT: Mahvand Saleki msaleki@unitedconsulting.com		PROJECT MANAGER: Rafael Ospina		Date Shipped	Sample Matrix	Preservative	# / Size of Cont.	pH	Resistivity	Sulphate	Chloride					
PHONE#: (770)582-2843		RECEIVING LAB: AES		PO#:														
SAMPLE NUMBER	SAMPLE DESCRIPTION																	
B-103@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-104@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-106@2-4'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-108@2-4'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-110@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-112@2-4'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-102@2-4'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
B-114@2-3.5'	Soil	11/19/2020	S	ICE	8OZ	X	X	X	X									
SAMPLES RELINQUISHED BY: PHUC VO		DATE/TIME: 11-19-2020 2:34	SAMPLES ACCEPTED BY: <i>[Signature]</i>			DATE/TIME: 11/19/20 2:35 PM	COMMENTS:											

Client: United Consulting Group Inc.
Project: Beaver Ruin Parks and Recreation
Lab ID: 2011M92

Case Narrative

pH Analysis by Method SW9045D:

Samples for pH analysis by Method SW9045D were received and analyzed outside holding time requirement of "immediate or 15 minutes."

Client: United Consulting Group Inc.	Client Sample ID: B-103@2-3.5'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-001	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A					(SW9050)			
Resistivity (@100% Moisture Saturation)	13400	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D					(SW9045D)			
pH	6.41	0.01	H	pH Units	306391	1	11/23/2020 14:00	CB
ION SCAN SW9056A					(SW9056A)			
Chloride	38	12		mg/Kg-dry	306486	1	11/30/2020 14:19	IP
Sulfate	56	12		mg/Kg-dry	306486	1	11/30/2020 14:19	IP
PERCENT MOISTURE D2216								
Percent Moisture	17.9	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-104@2-3.5'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-002	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A		(SW9050)						
Resistivity (@100% Moisture Saturation)	13500	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D		(SW9045D)						
pH	6.04	0.01	H	pH Units	306391	1	11/23/2020 14:02	CB
ION SCAN SW9056A		(SW9056A)						
Chloride	38	11		mg/Kg-dry	306486	1	11/28/2020 17:01	IP
Sulfate	27	11		mg/Kg-dry	306486	1	11/28/2020 17:01	IP
PERCENT MOISTURE D2216								
Percent Moisture	7.62	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-106@2-4'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-003	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	21500	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	5.88	0.01	H	pH Units	306391	1	11/23/2020 15:35	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	45	11		mg/Kg-dry	306486	1	11/25/2020 16:38	IP
Sulfate	130	11		mg/Kg-dry	306486	1	11/25/2020 16:38	IP
PERCENT MOISTURE D2216								
Percent Moisture	13.7	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-108@2-4'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-004	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	6310	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	5.91	0.01	H	pH Units	306391	1	11/23/2020 15:39	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	74	12		mg/Kg-dry	306486	1	11/28/2020 16:45	IP
Sulfate	43	12		mg/Kg-dry	306486	1	11/28/2020 16:45	IP
PERCENT MOISTURE D2216								
Percent Moisture	18.5	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-110@2-3.5'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-005	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A		(SW9050)						
Resistivity (@100% Moisture Saturation)	10600	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D		(SW9045D)						
pH	5.85	0.01	H	pH Units	306391	1	11/23/2020 15:40	CB
ION SCAN SW9056A		(SW9056A)						
Chloride	38	11		mg/Kg-dry	306486	1	11/28/2020 16:29	IP
Sulfate	21	11		mg/Kg-dry	306486	1	11/28/2020 16:29	IP
PERCENT MOISTURE D2216								
Percent Moisture	11.1	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-112@2-4'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-006	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	5580	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	7.33	0.01	H	pH Units	306391	1	11/23/2020 15:43	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	49	12		mg/Kg-dry	306486	1	11/28/2020 17:17	IP
Sulfate	90	12		mg/Kg-dry	306486	1	11/28/2020 17:17	IP
PERCENT MOISTURE D2216								
Percent Moisture	19.3	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-102@2-4'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-007	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A								
					(SW9050)			
Resistivity (@100% Moisture Saturation)	14100	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D								
					(SW9045D)			
pH	6.72	0.01	H	pH Units	306391	1	11/23/2020 15:47	CB
ION SCAN SW9056A								
					(SW9056A)			
Chloride	36	11		mg/Kg-dry	306486	1	11/30/2020 14:03	IP
Sulfate	30	11		mg/Kg-dry	306486	1	11/30/2020 14:03	IP
PERCENT MOISTURE D2216								
Percent Moisture	5.75	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:

- * Value exceeds maximum contaminant level
- BRL Below reporting limit
- H Holding times for preparation or analysis exceeded
- N Analyte not NELAC certified
- B Analyte detected in the associated method blank
- > Greater than Result value

- E Estimated (value above quantitation range)
- S Spike Recovery outside limits due to matrix
- Narr See case narrative
- F Analyzed in the lab which is a deviation from the method
- < Less than Result value
- J Estimated value detected below Reporting Limit

Client: United Consulting Group Inc.	Client Sample ID: B-114@2-3.5'
Project Name: Beaver Ruin Parks and Recreation	Collection Date: 11/19/2020
Lab ID: 2011M92-008	Matrix: Soil

Analyses	Result	Reporting Limit	Qual	Units	BatchID	Dilution Factor	Date Analyzed	Analyst
Soil Resistivity SW9050A		(SW9050)						
Resistivity (@100% Moisture Saturation)	18800	0		ohms*cm	306477	1	11/24/2020 15:18	CB
Laboratory Hydrogen Ion (pH) SW9045D		(SW9045D)						
pH	5.85	0.01	H	pH Units	306391	1	11/23/2020 15:50	CB
ION SCAN SW9056A		(SW9056A)						
Chloride	45	12		mg/Kg-dry	306486	1	11/28/2020 13:37	IP
Sulfate	37	12		mg/Kg-dry	306486	1	11/28/2020 13:37	IP
PERCENT MOISTURE D2216								
Percent Moisture	15.3	0		wt%	R440362	1	11/22/2020 07:00	JW

Qualifiers:	* Value exceeds maximum contaminant level	E Estimated (value above quantitation range)
	BRL Below reporting limit	S Spike Recovery outside limits due to matrix
	H Holding times for preparation or analysis exceeded	Narr See case narrative
	N Analyte not NELAC certified	F Analyzed in the lab which is a deviation from the method
	B Analyte detected in the associated method blank	< Less than Result value
	> Greater than Result value	J Estimated value detected below Reporting Limit

SAMPLE/COOLER RECEIPT CHECKLIST

1. Client Name: United Consulting Group Inc.

AES Work Order Number: 2011M92

2. Carrier: FedEx UPS USPS Client Courier Other _____

	Yes	No	N/A	Details	Comments
3. Shipping container/cooler received in good condition?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	damaged <input type="checkbox"/> leaking <input type="checkbox"/> other <input type="checkbox"/>	
4. Custody seals present on shipping container?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
5. Custody seals intact on shipping container?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
6. Temperature blanks present?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
7. Cooler temperature(s) within limits of 0-6°C? [See item 13 and 14 for temperature recordings.]	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	Cooling initiated for recently collected samples / ice present <input type="checkbox"/>	
8. Chain of Custody (COC) present?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
9. Chain of Custody signed, dated, and timed when relinquished and received?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
10. Sampler name and/or signature on COC?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
11. Were all samples received within holding time?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
12. TAT marked on the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	If no TAT indicated, proceeded with standard TAT per Terms & Conditions. <input type="checkbox"/>	

13. Cooler 1 Temperature 0.1 °C Cooler 2 Temperature _____ °C Cooler 3 Temperature _____ °C Cooler 4 Temperature _____ °C

14. Cooler 5 Temperature _____ °C Cooler 6 Temperature _____ °C Cooler 7 Temperature _____ °C Cooler 8 Temperature _____ °C

15. Comments: _____

I certify that I have completed sections 1-15 (dated initials). BH 11/20/20

	Yes	No	N/A	Details	Comments
16. Were sample containers intact upon receipt?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
17. Custody seals present on sample containers?	<input type="radio"/>	<input checked="" type="radio"/>	<input type="radio"/>		
18. Custody seals intact on sample containers?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
19. Do sample container labels match the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	incomplete info <input type="checkbox"/> illegible <input type="checkbox"/> no label <input type="checkbox"/> other <input type="checkbox"/>	
20. Are analyses requested indicated on the COC?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
21. Were all of the samples listed on the COC received?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>	samples received but not listed on COC <input type="checkbox"/> samples listed on COC not received <input type="checkbox"/>	
22. Was the sample collection date/time noted?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
23. Did we receive sufficient sample volume for indicated analyses?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
24. Were samples received in appropriate containers?	<input checked="" type="radio"/>	<input type="radio"/>	<input type="radio"/>		
25. Were VOA samples received without headspace (< 1/4" bubble)?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
26. Were trip blanks submitted?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>	listed on COC <input type="checkbox"/> not listed on COC <input type="checkbox"/>	

27. Comments: _____

I certify that I have completed sections 16-27 (dated initials). BH 11/20/20

This section only applies to samples where pH can be checked at Sample Receipt

	Yes	No	N/A	Details	Comments
28. Have containers needing chemical preservation been checked? *	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
29. Containers meet preservation guidelines?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		
30. Was pH adjusted at Sample Receipt?	<input type="radio"/>	<input type="radio"/>	<input checked="" type="radio"/>		

* Note: Certain analyses require chemical preservation but must be checked in the laboratory and not upon Sample Receipt such as Coliforms, VOCs and Oil & Grease/TPH.

This also excludes metals by EPA 200.7, 200.8 and 245.1 which will be verified between 16 and 24 hours after preservation.

I certify that I have completed sections 28-30 (dated initials). BH 11/20/20

Client: United Consulting Group Inc.
 Project Name: Beaver Ruin Parks and Recreation
 Lab Order: 2011M92

Dates Report

Lab Sample ID	Client Sample ID	Collection Date	Matrix	Test Name	TCLP Date	Prep Date	Analysis Date
2011M92-001A	B-103@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-001A	B-103@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-001A	B-103@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M92-001A	B-103@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-002A	B-104@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-002A	B-104@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-002A	B-104@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/28/2020
2011M92-002A	B-104@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-003A	B-106@2-4'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-003A	B-106@2-4'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-003A	B-106@2-4'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/25/2020
2011M92-003A	B-106@2-4'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-004A	B-108@2-4'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-004A	B-108@2-4'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-004A	B-108@2-4'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/28/2020
2011M92-004A	B-108@2-4'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-005A	B-110@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-005A	B-110@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-005A	B-110@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/28/2020
2011M92-005A	B-110@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-006A	B-112@2-4'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-006A	B-112@2-4'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-006A	B-112@2-4'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/28/2020
2011M92-006A	B-112@2-4'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-007A	B-102@2-4'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020
2011M92-007A	B-102@2-4'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-007A	B-102@2-4'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/30/2020
2011M92-007A	B-102@2-4'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020
2011M92-008A	B-114@2-3.5'	11/19/2020 12:00:00AM	Soil	Laboratory Hydrogen Ion (pH)		11/23/2020 7:33:00AM	11/23/2020

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Parks and Recreation
Lab Order: 2011M92

Dates Report

Lab Sample ID	Client Sample ID	Collection Date	Matrix	Test Name	TCLP Date	Prep Date	Analysis Date
2011M92-008A	B-114@2-3.5'	11/19/2020 12:00:00AM	Soil	Soil Resistivity		11/23/2020 7:30:00AM	11/24/2020
2011M92-008A	B-114@2-3.5'	11/19/2020 12:00:00AM	Soil	ION SCAN		11/24/2020 5:13:22PM	11/28/2020
2011M92-008A	B-114@2-3.5'	11/19/2020 12:00:00AM	Soil	PERCENT MOISTURE			11/22/2020

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Parks and Recreation
Workorder: 2011M92

ANALYTICAL QC SUMMARY REPORT

BatchID: 306391

Sample ID: LCS-306391	Client ID:	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: LCS	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027582							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 6.990 0.01 7.000 99.9 90 110

Sample ID: 2011M90-001ADUP	Client ID:	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: DUP	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027609							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 5.800 0.01 5.880 1.37 10 H

Sample ID: 2011M91-002ADUP	Client ID:	Units: pH Units	Prep Date: 11/23/2020	Run No: 440415							
SampleType: DUP	TestCode: Laboratory Hydrogen Ion (pH) SW9045D	BatchID: 306391	Analysis Date: 11/23/2020	Seq No: 10027610							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

pH 5.850 0.01 5.940 1.53 10 H

Qualifiers:	> Greater than Result value	< Less than Result value	B Analyte detected in the associated method blank
BRL	Below reporting limit	E Estimated (value above quantitation range)	H Holding times for preparation or analysis exceeded
J	Estimated value detected below Reporting Limit	N Analyte not NELAC certified	R RPD outside limits due to matrix
Rpt Lim	Reporting Limit	S Spike Recovery outside limits due to matrix	

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Parks and Recreation
Workorder: 2011M92

ANALYTICAL QC SUMMARY REPORT

BatchID: 306486

Sample ID: MB-306486	Client ID:	Units: mg/Kg	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MBLK	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036056							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride
Sulfate

BRL 10
BRL 10

Sample ID: LCS-306486	Client ID:	Units: mg/Kg	Prep Date: 11/24/2020	Run No: 440738							
SampleType: LCS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036057							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride
Sulfate

108.4 10 100.0 108 90 110
272.0 10 250.0 109 90 110

Sample ID: 2011M92-003AMS	Client ID: B-106@2-4'	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036061							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride
Sulfate

172.7 11 114.1 44.88 112 80 120
302.7 11 285.2 133.2 59.4 80 120 S

Sample ID: 2011M92-008AMS	Client ID: B-114@2-3.5'	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MS	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/28/2020	Seq No: 10042731							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride
Sulfate

155.9 12 115.7 45.12 95.8 80 120
268.3 12 289.3 36.80 80.0 80 120

Sample ID: 2011M92-003AMSD	Client ID: B-106@2-4'	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738							
SampleType: MSD	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036062							
Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual

Chloride

170.8 12 115.9 44.88 109 80 120 172.7 1.12 20

Qualifiers: > Greater than Result value < Less than Result value B Analyte detected in the associated method blank
 BRL Below reporting limit E Estimated (value above quantitation range) H Holding times for preparation or analysis exceeded
 J Estimated value detected below Reporting Limit N Analyte not NELAC certified R RPD outside limits due to matrix
 Rpt Lim Reporting Limit S Spike Recovery outside limits due to matrix

Client: United Consulting Group Inc.
Project Name: Beaver Ruin Parks and Recreation
Workorder: 2011M92

ANALYTICAL QC SUMMARY REPORT

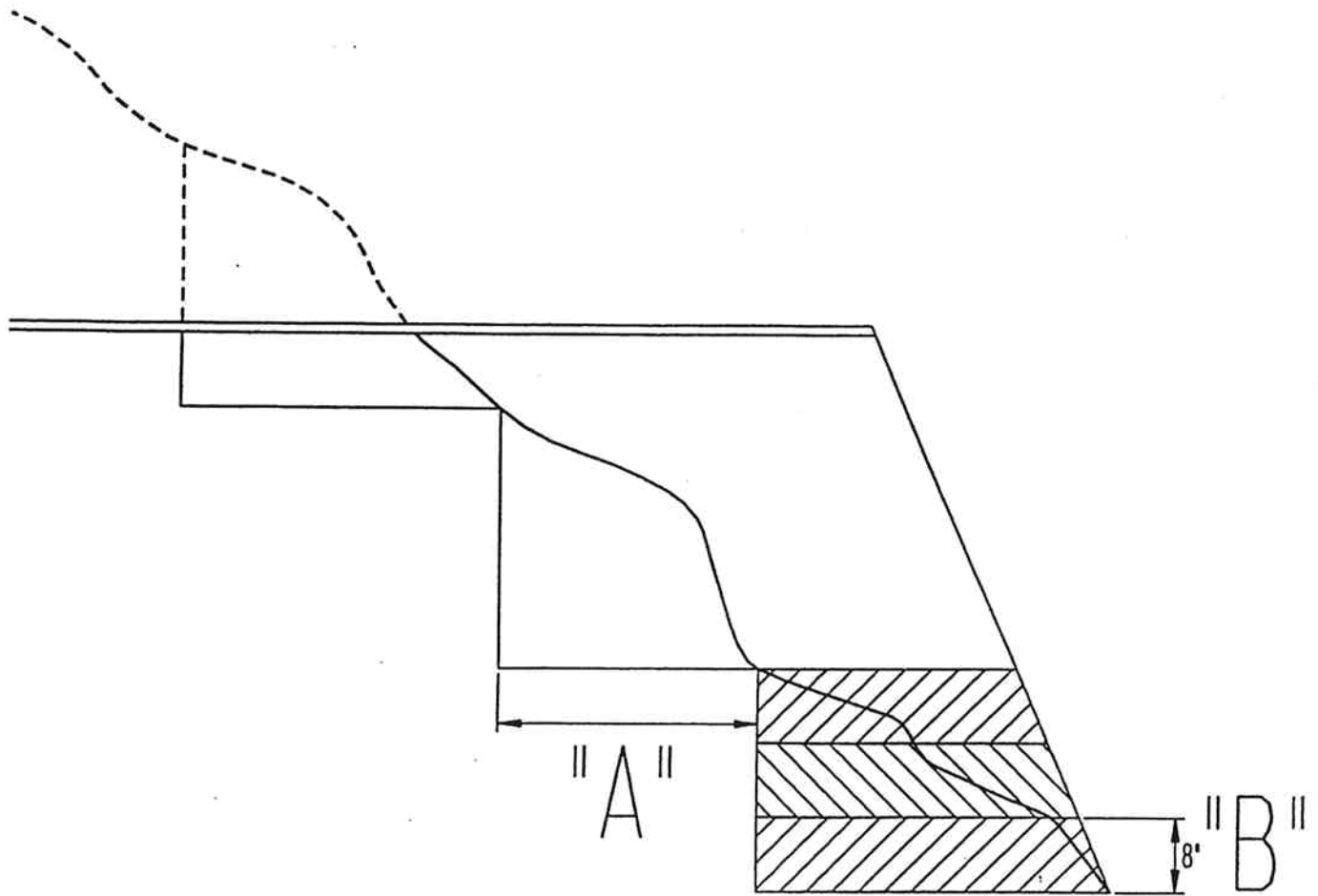
BatchID: 306486

Sample ID: 2011M92-003AMSD	Client ID: B-106@2-4'	Units: mg/Kg-dry	Prep Date: 11/24/2020	Run No: 440738
SampleType: MSD	TestCode: ION SCAN SW9056A	BatchID: 306486	Analysis Date: 11/25/2020	Seq No: 10036062

Analyte	Result	RPT Limit	SPK value	SPK Ref Val	%REC	Low Limit	High Limit	RPD Ref Val	%RPD	RPD Limit	Qual
Sulfate	307.6	12	289.7	133.2	60.2	80	120	302.7	1.61	20	S

Qualifiers:	>	Greater than Result value	<	Less than Result value	B	Analyte detected in the associated method blank
	BRL	Below reporting limit	E	Estimated (value above quantitation range)	H	Holding times for preparation or analysis exceeded
	J	Estimated value detected below Reporting Limit	N	Analyte not NELAC certified	R	RPD outside limits due to matrix
	Rpt Lim	Reporting Limit	S	Spike Recovery outside limits due to matrix		

End of Report



1. THE ABOVE DIAGRAM ILLUSTRATES A TYPICAL BENCHING FOR PLACEMENT OF FILL ON A SLOPING SURFACE.
2. THE DIAGRAM SHOWS THAT BEFORE FILL IS PLACED, THE FIRST STEP IS CUT INTO THE SLOPE A MAXIMUM DISTANCE OF ABOUT 8 FEET 'A' (ABOUT $\frac{3}{4}$ THE WIDTH OF USUAL D-8 BULLDOZER BLADE). SUCCESSIVE LAYERS OF FILL ARE THEN PLACED. BEFORE FINAL LAYER IS PLACED, THE SECOND STEP IS CUT 8 FEET INTO THE SLOPE AND SUCCESSIVE LAYERS ARE AGAIN PLACED.
3. SELECT FILL MATERIAL SHOULD BE PLACED IN 8 INCH LIFTS AND COMPACTED TO THE SPECIFIED DENSITY ('B').

TYPICAL BENCHING DETAIL



UNITED CONSULTING
 625 HOLCOMB BRIDGE ROAD, NORCROSS, GEORGIA 30071
 OFFICE (770)-209-0029 FAX (770)-582-2900

Important Information about This

Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply this report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light-industrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by:* the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmation-dependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.*

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help

others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical-engineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold-prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical-engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; *none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.*

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your GBC-Member geotechnical engineer for more information.



8811 Colesville Road/Suite G106, Silver Spring, MD 20910

Telephone: 301/565-2733 Facsimile: 301/589-2017

e-mail: info@geoprofessional.org www.geoprofessional.org

Copyright 2015 by Geoprofessional Business Association (GBA). Duplication, reproduction, or copying of this document, or its contents, in whole or in part, by any means whatsoever, is strictly prohibited, except with GBA's specific written permission. Excerpting, quoting, or otherwise extracting wording from this document is permitted only with the express written permission of GBA, and only for purposes of scholarly research or book review. Only members of GBA may use this document as a complement to or as an element of a geotechnical-engineering report. Any other firm, individual, or other entity that so uses this document without being a GBA member could be committing negligent or intentional (fraudulent) misrepresentation.



December 31, 2020

Charles E. Crowell, Jr., PE, CPESC, CPSWQ, CFM
Stormwater Section Manager, Engineering and Construction
Gwinnett County, Georgia
Department of Water Resources
684 Winder Highway
Lawrenceville, Georgia 30045

Subject: Beaver Ruin Wetland Enhancement – Boardwalk Foundation Recommendations

Dear Mr. Crowell:

United Consulting has performed a subsurface exploration for the boardwalk project and prepared a report that documents the boring findings and presents recommendations for the boardwalk foundations. Tetra Tech has reviewed their subsurface exploration report and takes no exception to the recommendations presented in the report. A copy of their report is attached to this letter for reference. Pertinent information from our review is presented below.

A total of six borings (B-1 through B-6) were drilled by United Consulting for the proposed boardwalk alignment. The boring depths ranged between 19 and 30 feet. Boring B-5 encountered a couple of feet of fill at the ground surface. Below the fill in boring B-5 and the ground surface in the remaining borings, the borings encountered residual clays and sands that are typical for the area. The upper five to 10 feet was soft or loose. Weathered bedrock, consisting of very dense sand, was encountered in borings B-2 through B-6 at depths of 13.5 feet to 28.5 feet. Boring B-1 did not encounter weathered bedrock to its completion depth of 30 feet. Groundwater was encountered within 8 feet of the ground surface in the six borings at the time the borings were drilled.

It is understood that spread footings were originally considered to support the proposed boardwalk. However, because of the presence of the soft and loose upper soils, shallow foundations are not practical due to the risk of settlement. Consequently, deep foundations, consisting of helical piers, were considered to support the proposed boardwalk.

Based on information from the boardwalk supplier, the proposed boardwalk foundations are subject to both axial and lateral loads. Therefore, battered helical piers will be used to resist the lateral loads. It is anticipated that the helical piers will have to be extended to the dense sands or weathered rock to achieve the desired capacity. The table below presents the preliminary pier capacities at each boring location based on the subsurface conditions encountered in each boring. For additional details regarding the helical pier recommendations, please refer to the attached report.

Boring	Battered Pile Design Compression Service Loads (kips)	Battered Pile Minimum Installation Torque (ft-lb)	Minimum Depth to Bottom Helix (ft)
B-1	30.5	6,108	25
B-2			15
B-3			17
B-4			17
B-5			14
B-6			24

We would also note that there are different suppliers of helical piers, each with different component sizes and helix configurations. Therefore, the final design of the helical pier foundations should be provided by the helical pier supplier based on the anticipated loads from the boardwalk supplier. In addition, the construction documents should require load tests on the installed helical piers to confirm their load capacity.

For the design of earth retention structures, the parameters in the table below may be used. For additional recommendations on retaining wall design for the project, please refer to the attached report.

Earth Pressure Condition	Earth Pressure Coefficient	Recommended Equivalent Fluid Pressure (psf/ft)
Active	$K_a = 0.36$	43
At-Rest	$K_o = 0.53$	64
Passive	$K_p = 2.77$	332

The seismic site classification is impacted by the soft clays and loose soils in the upper 5 to 10 feet of the subsurface profile. Based on the presence of these weaker soils at the site, it is recommended that Site Class E be used for any seismic design.

If you have any questions or require any further information, please do not hesitate to contact us.

Respectfully submitted,

Tetra Tech, Inc.



Frederic (Rick) M. Shmurak, PE
Senior Project Manager